

SEDIMENTOLOGY OF A FRESHWATER TIDAL SYSTEM,  
PITT RIVER - PITT LAKE, BRITISH COLUMBIA

*by*

GAIL MOWRY ASHLEY

B.Sc., University of Massachusetts, 1963

M.Sc., University of Massachusetts, 1972

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Department of Geological Sciences

The University of British Columbia  
2075 Wesbrook Place  
Vancouver, Canada  
V6T 1W5

Date July 14, 1977

ABSTRACT

Pitt River, 30 km inland from Vancouver, British Columbia at the southern margin of the Coast Mountains, links Fraser River estuary and Pitt Lake. Salt water seldom extends to within 10 km of Fraser - Pitt confluence; nevertheless, tides modulate Fraser flow and cause Pitt River to fluctuate 2 m and Pitt Lake as much as 1.2 m. There is an upstream movement of sediment in Pitt River from Fraser River, evidenced by identical mineralogy of Pitt River and Fraser River sediments; a decrease in grain size from the Fraser to Pitt Lake, and a predominance of flood-oriented bedforms in the river channel. A delta of 12 km<sup>2</sup> area has accumulated at the lower (draining) end of the lake.

The purposes of the study were to: (1) examine aspects of the hydrodynamics of Pitt River and Pitt Lake as a tidal system; (2) evaluate the effect of bidirectional flow on river and delta morphology; (3) determine processes of sediment movement in the river and of sediment dispersal on the delta; and (4) estimate present sedimentation rate on the delta.

Water Survey of Canada stage data from 3 locations in the system, used in conjunction with velocity measurements

(profiles and tethered meter), revealed large seasonal and tidal variations in discharge. Calculations indicate that flood basal shear stress peaks early in the flow, whereas ebb currents have a lower basal shear stress which peaks late in the flow. Thus, sediment moves farther forward on a flood flow than it moves back on the succeeding ebb.

Studies of the river channel using hydrographic charts revealed regular meanders ( $\lambda_M = 6100$  m) and evenly spaced riffles and pools which are scaled to the strongest flow (winter flood current,  $Q_e$ ). Meander point bars are accreting on the "upstream" side indicating deposition by the flood-oriented flow. The three dimensional geometry of the large-scale bedforms which cover the sandy thalweg of both river and delta channel was determined by echo sounding and side-scan sonar. Three distinct sizes (height/spacing = 0.8 m/10-15m; 1.5 m/25-30 m; 3 m/50-60 m) of large-scale bedforms (sand waves) were found; their linear relationship of height vs. spacing ( $\lambda_B$ ) on log-log plot suggests a common genesis. The size appears to be related to channel geometry, not to depth of flow. Largest forms are found in reaches which shallow in the direction of water movement and smallest forms occur on relatively flat topography. The following tentative relationship is suggested for sandy meandering rivers:  $\lambda_M/\lambda_B \propto Q_e$ .

Pitt delta morphology was studied with aerial photos and depth soundings. Its shape is considered an excellent

example of sediment diffusion and deposition from a simple jet into a low energy lacustrine environment. Analysis of 190 sediment samples from river, delta, and lake bottom shows the sediment to be polymodal. Graphical partitioning of the cumulative probability plots reveals that sediments are composed of up to 4 log-normal distributions. Each distribution is interpreted as a population related to a process of sediment transport. Five subenvironments in the Pitt system are characterized by unique combinations of these "process" populations.

Cores in the delta topsets and lake bottom sediments reveal silt and clay rhythmites, interpreted as varves. The coarse layers are deposited during winter when discharge of Fraser River is low and tidally induced discharge in Pitt system is high. The fine layers are deposited during spring run-off when additional fines are added to the lake from the Pitt basin.  $^{137}\text{Cs}$  dating of sediments shows that as much as 1.8 cm/yr are accumulating in the active portions of the delta with an estimated  $150 \pm 20 \times 10^3$  tonnes deposited annually.

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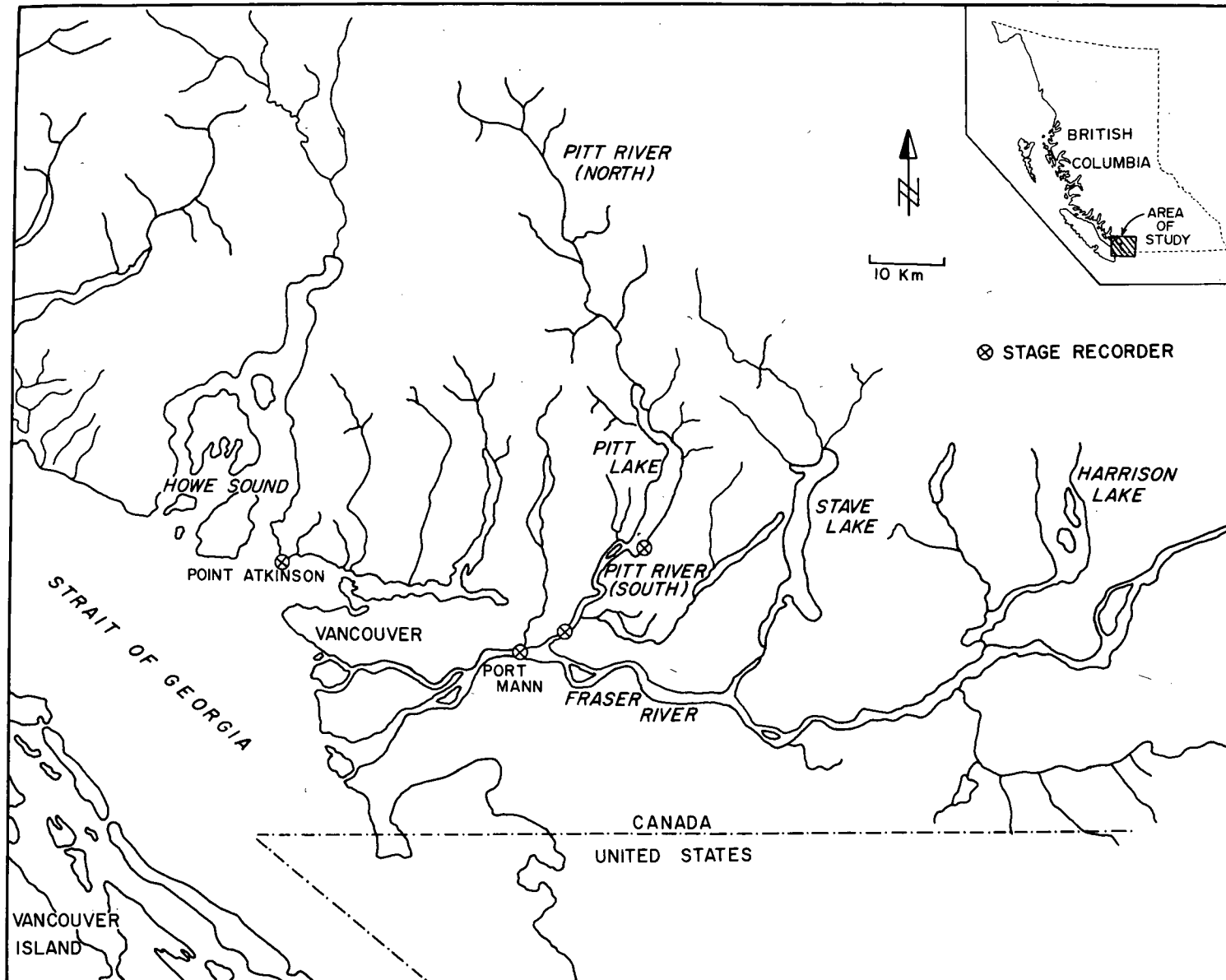
## PART ONE:

## INTRODUCTION

Pitt River (North) - Pitt Lake - Pitt River (South) system is situated in a glacially scoured valley within the Coast Mountains, British Columbia, approximately 30 km inland from the port of Vancouver (Fig. 1). The valley of the Pitt, 70 km in length, opens abruptly into the Fraser lowland. Pitt River (North) drains 816 km<sup>2</sup> including several mountain glaciers and provides a mean discharge of 80 cu m/sec to the lake. Pitt River (North) is not included in this study and the term Pitt River will hereafter refer to Pitt River (South) which joins Pitt Lake to the Fraser River.

Pitt River and Pitt Lake are tidal, being connected to the ocean (Strait of Georgia) by lower Fraser River. Although water levels in the Pitt system respond to the tides, salt water seldom extends closer than 10 km downstream of the Fraser-Pitt confluence. Rising water (flood tide) in the Strait, retards flow of the Fraser and raises its elevation, or stage level, progressively eastward until the water level at the Fraser-Pitt confluence is higher than in Pitt River. Flow in the Pitt then reverses and water diverted from the Fraser flows northward up Pitt River into Pitt Lake.

FIGURE 1. Location map of Pitt River -  
Pitt Lake system.



As the water elevation falls (ebb tide) in the Strait, Fraser River flow is accelerated. The surface elevation is lowered progressively eastward until the level at the Fraser-Pitt confluence is lower than that of the Pitt River. Flow then reverses in the Pitt system and drains toward the sea. Hereafter, flow northward away from the ocean and toward Pitt Lake is referred to as flood; flow returning to the Fraser River and ocean is ebb.

The Fraser River estuary, Pitt River, and Pitt Lake all exhibit a time-stage asymmetry. That is, water elevations rise more quickly during flood tide than levels fall on the ebb. This produces a velocity inequality such that the flood usually has the highest average peak velocities.

Although Pitt River is subjected to continually reversing flow it has few estuarine characteristics. Shallow estuaries often have a branching system of tidal channels whose numbers increase in an up-estuary direction. Also they commonly have separate channels for flood and ebb flow (Pritchard, 1967). The Pitt has only a single channel for both flow directions. At least two aspects of the Pitt system may account for the distinct lack of estuarine characteristics. (1) A shallow estuary whose depth would normally decrease up estuary has been replaced by a conduit (Pitt River) and a reservoir (Pitt Lake). This reservoir

with large storage capacity allows flood tide water to flow through Pitt River with no more impedance than in a normal river channel. (2) Pitt basin drainage contributes a discharge which varies from 5% to 50% of the total volume of water moving through the system and thus is not always dominated by tidal flow. Pitt River is a tidal channel that can be thought of as a simple water course subjected to two different unidirectional flows with the stronger flow (flood) having the greater effect in shaping its morphology.

There is an apparent upstream movement of sediment in Pitt River from Fraser River to Pitt Lake. This is evidenced by a predominance of flood-oriented bedforms in the river channel and a decrease in grain size from the Fraser to the lake. A large area of sediment ( $12 \text{ km}^2$ ) is accumulating at the lower end of the lake. The purposes of this study are to examine the hydrodynamics of the Pitt as a tidal river and to evaluate the effect of bi-directional flow on both sediment movement and the development of the present day channel morphology.

## GEOLOGIC HISTORY

During the Pleistocene Epoch, repeated glaciations aided by pre- and inter-glacial stream activity, have deeply eroded valleys oriented along a north-west and north-east oriented joint pattern occurring in the Coast Mountains (Peacock, 1935). Following the most recent deglaciation (15,000 - 11,000 B.P.) the melting ice left numerous elongate lakes in interior valleys and a coastline dominated by fiords. However, in early postglacial times the location of the shore fluctuated as a result of complex interaction of eustatic sealevel changes and crustal rebound (Mathews et al., 1970). During this period of instability, ocean waters flooded past the mouth of Pitt Valley, as evidenced by marine shells (12,690  $\pm$  190 B.P.; I5959, Mathewes, 1973) collected at an elevation of 107 m on the east side of Pitt valley. Glaciomarine sediment (up to 275 meters thick) was deposited in the valley during this post-glacial period. Isostatic uplift began around 13,000 B.P. and was essentially complete by 8,000 B.P. (Mathews, et al., 1970). Fraser River, supplied by abundant glacial sediment, rapidly constructed a delta westward and by 8,290  $\pm$  140 B.P. (G.S.C. 229, Dyck et al., 1965) "Pitt Fiord" was sealed off at its southern end by this delta. It is likely that a short tidal channel maintained a connection between the

fiord and Fraser estuary. Tidal currents flowing through this channel must have carried sediment from Fraser River into the fiord, building a flood tidal delta which continued to grow northward as the Fraser delta progressed westward. By  $4,645 \pm 95$  B.P. (I7047; Mathews, 1976, pers. comm.) the leading edge of the Pitt delta stood at least 20 km north of Fraser River near the present outlet of Pitt Lake (Fig. 1). At some time during this period "Pitt Fiord" was flushed of saline water and became Pitt Lake. No salt water remains in the lake; not even in deepest basin (150 m). As the sea-land relationship has been much the same as at present since 5,500 B.P. (Mathews et al., 1970), it is probable that Pitt Lake has been in existence for at least six thousand years. During the last 4,700 years, Pitt tidal delta has advanced up to 6 km farther into Pitt Lake at an average rate of  $1.28 \text{ m.yr.}^{-1}$ . However, this sedimentation rate has most likely decreased exponentially, starting at meters per year and tapering off to the present rate of approximately a centimeter per year (Ashley, 1977).

Pitt River presently flows along the western edge of the valley and there is no geomorphic evidence on the floodplain to suggest that the channel has migrated extensively during its development. Dikes built along 85% of the river shoreline during the last 50 years are for flood prevention rather than to prevent bank erosion and



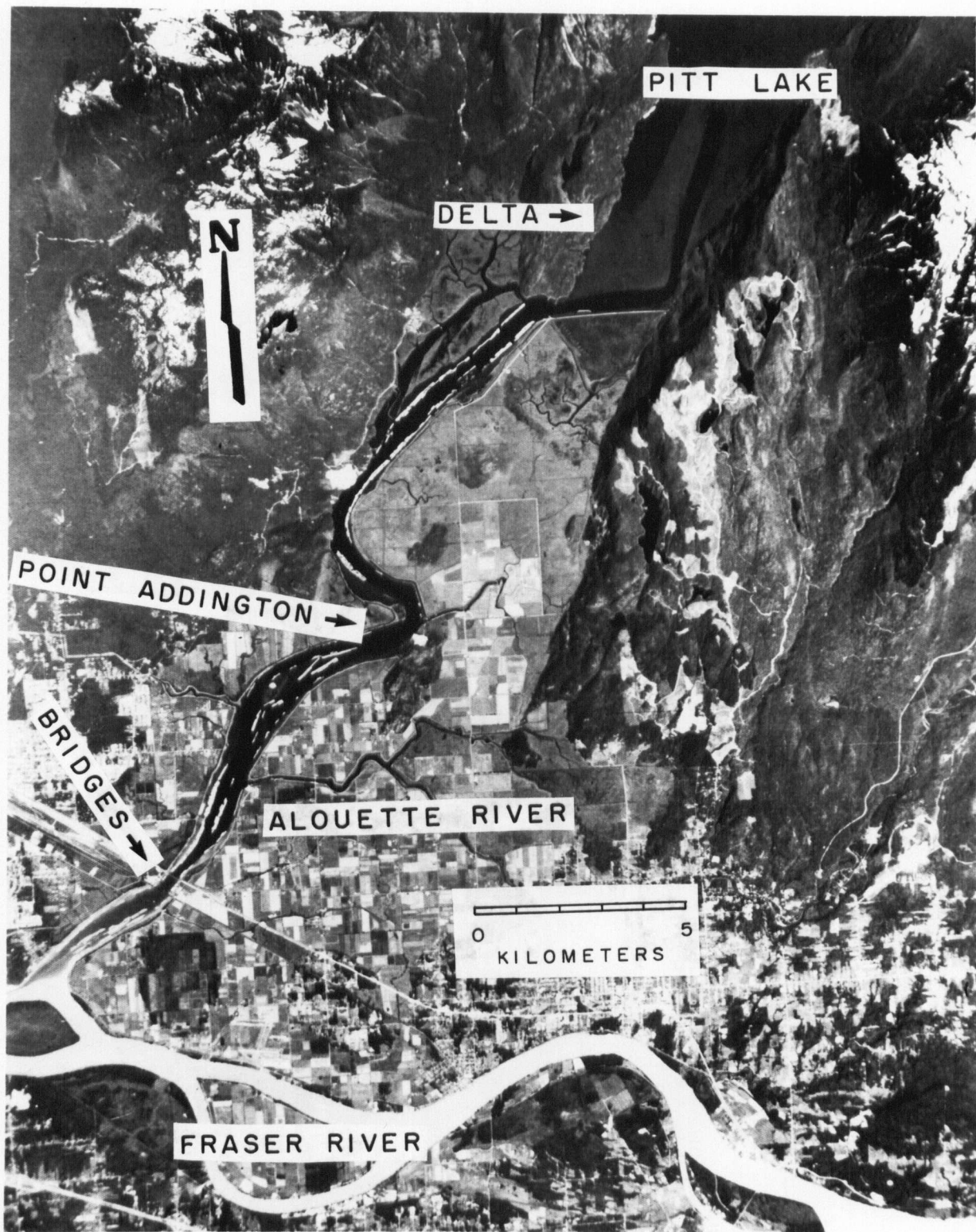
appear to have no effect on controlling river processes. On the other hand two bridges, and the log storage areas constructed along most of the river banks, islands, and mid-channel shoals locally effect erosion and sedimentation.

## GEOMORPHOLOGY

The Pitt River floodplain occupies the complete width (ranging from 5-10 km) of the lower Pitt Valley and 17.2 km of its length from the banks of Fraser River to the outlet of Pitt Lake (Fig.2). The Pitt River channel (20.7 km) is only slightly longer than its floodplain, resulting in a low sinuosity (Schumm, 1963) of 1.2. The floodplain surface is of low relief, less than 3 meters above mean sea level (M.S.L.), and appears to be graded to the Fraser River floodplain located to the south and west. Bedrock knobs protrude through the plain, indicating that the bedrock surface is one of moderately high relief. Boreholes (Geol. Survey of Canada, unpublished data) through the Pitt sediments reveal a monotonous sequence (up to 275 m thick) of silt and clay with occasional thin units of sand. Salt water is commonly found below 25 m. The upper portion of the silts was likely deposited in Fraser delta and "Pitt Fiord" delta in their early stages. These sediments grade up into more recent Pitt River floodplain deposits which probably contain minor amounts of Fraser overbank material.

The detailed study of the Pitt channel geomorphology was based on large-scale bathymetric charts (Dept. Public Works, 1966, unpublished data) which were verified in the

FIGURE 2. Aerial photo of lower Pitt Lake and  
Pitt River floodplain.



PITT LAKE

DELTA →

N

POINT ADDINGTON →

BRIDGES →

ALOUETTE RIVER

0 5  
KILOMETERS

FRASER RIVER

no page 12

field by depth soundings (Raytheon, model #DE-1190; Furuno, model #F-850 Mark II series) and sidescan sonar recordings (Klein, model #400). Aerial photographs (scale, 1:15,840 and 1:31,680) were used for interpretation of planimetric features of both channel and floodplain.

The morphology of Pitt River channel consists of several slightly curved reaches and one major s-shaped bend (Fig. 3). The location and shape of this bend appears to be mainly due to bedrock control but may be aided by tributaries entering the river at the points of maximum curvature. Bankful channel width ( $W$ ) varies from 250 m to 900 m with an overall average of 600 m. The longitudinal profile (Fig. 4) shows great variability in depth with the deepest sections at the bridges and meander bends. Consequently cross-sectional area is also variable, ranging from 2390 m<sup>2</sup> to 4831 m<sup>2</sup> with a mean of 3251 m<sup>2</sup>. Depth ( $d$ ) varies from 8 m to 24.4 m, and mean depth is 12.1 m giving Pitt River a fairly low width/depth ratio of 50. Fisk (1951) and Schumm (1960) noted that rivers with fine grained bank materials would be expected to be narrow and deep, as well as slow to migrate.

The floodplain geomorphology reveals no evidence of extensive river channel migration from its present site on the west side of Pitt Valley. Since the Fraser Delta was prograding westward and ultimate base level for the

FIGURE 3A. Flow pattern of flood oriented currents.  
Flow lines drawn perpendicular to crests  
of large scale two-dimensional bed  
configurations (15 - 60 m in spacing,  
1 - 3 m in height).

FIGURE 3B. Mean grain size (in mm) distribution map  
and location of current measurement sites.

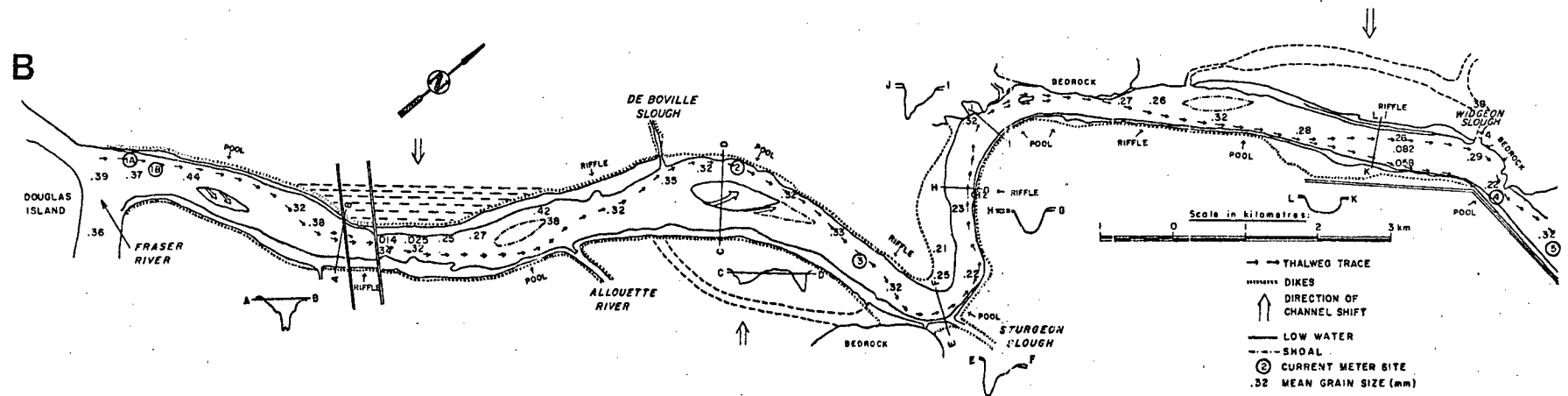
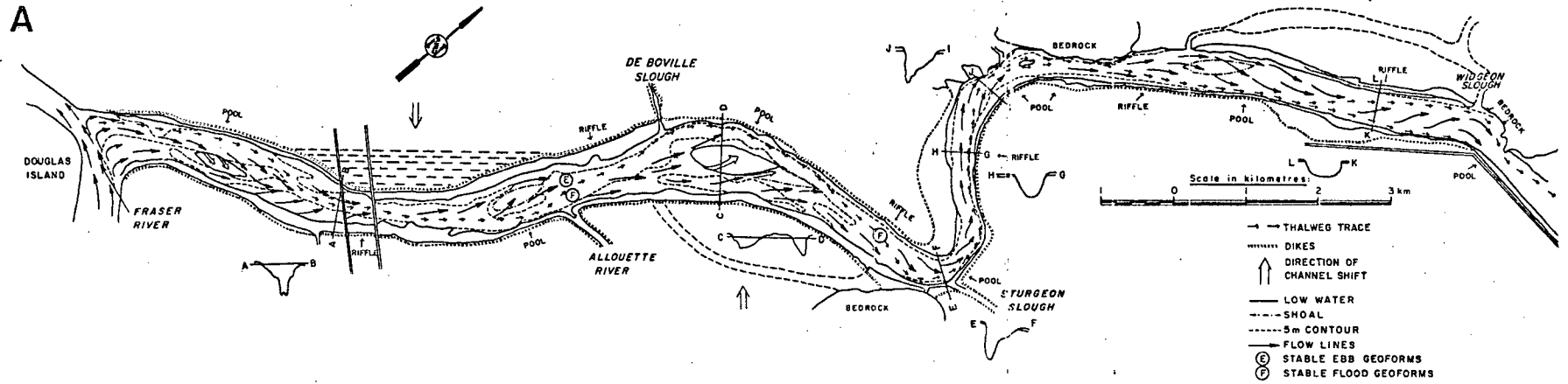
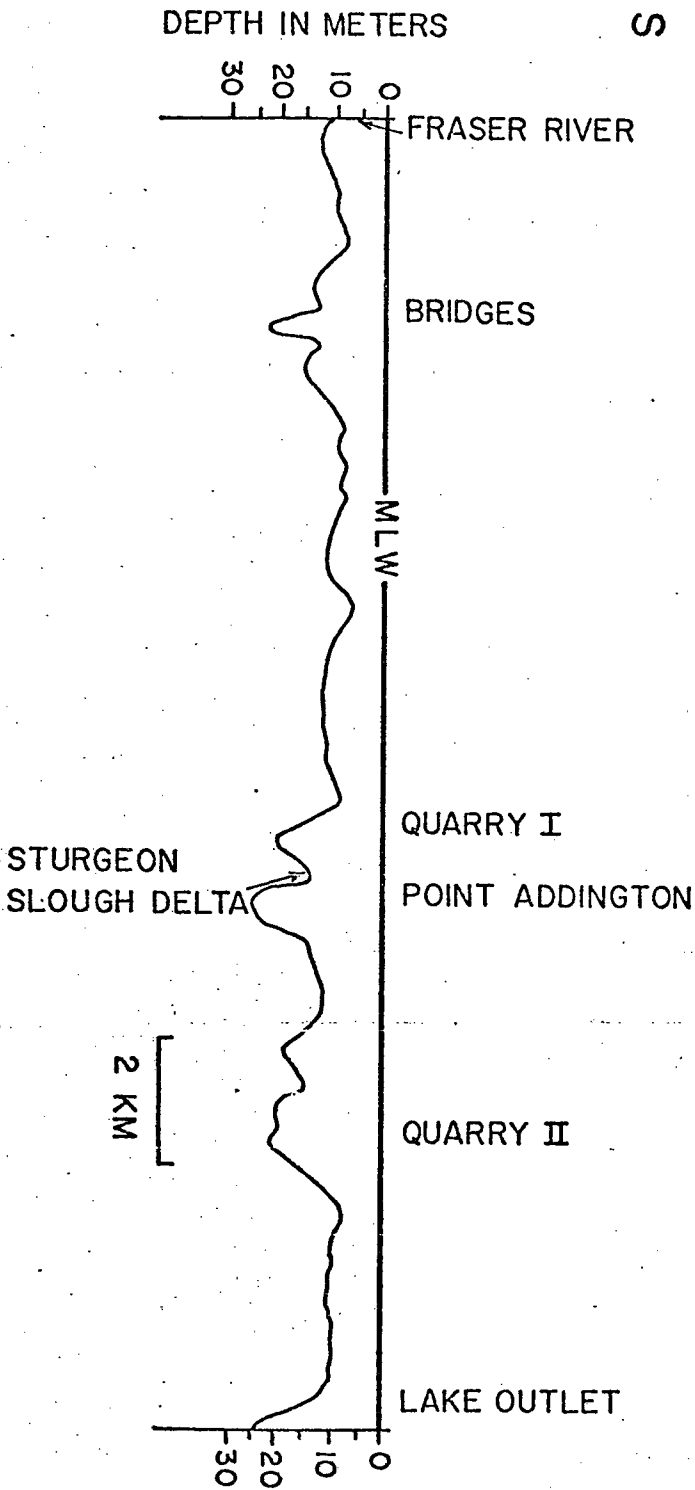




FIGURE 4. Longitudinal profile along thalweg  
of Pitt River.

PITT RIVER  
LONGITUDINAL PROFILE  
THALWEG TRACE  
VERT. Ex 80x



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former "Pitt Fiord" (the ocean) was also to the west, the early tidal channel was likely positioned on the valley's west side. As sediment gradually filled in the fiord and the channel lengthened it would tend to remain on the west. In addition, Alouette River (Fig. 2), the main tributary of Pitt River, flows westward and would reinforce this tendency. Not only has the general location of the Pitt channel apparently been stable, but even locally there have been few major channel changes. Fig. 3 shows three displacements which in total have not had an appreciable effect in changing channel length. The two northern ones appear to have a similar origin. It is proposed that the shifts occurred by bifurcation of the channel with the growth of a mid-channel bar. The less-used channel on the inside of the bend was subsequently abandoned and another mid-channel bar would grow, again bifurcating the channel (Fig. 5). The three channel shifts occur in opposing directions so that the middle one counteracts the direction of shift of the other two. The southernmost channel displacement at the bridges appears to have occurred in small increments with no bar development. Borehole information (Peters, 1973) shows that the river is constrained here in its eastward movement by a deposit of organic-rich clayey silts (Fig. 6). Thus the bridges are located at the narrowest section of river where the channel is being forced against resistant bank material.

FIGURE 5. Aerial photo near Addington Point. Note meander scar and diverging flow pattern across island. Point bar is accreting on upstream side of meander.

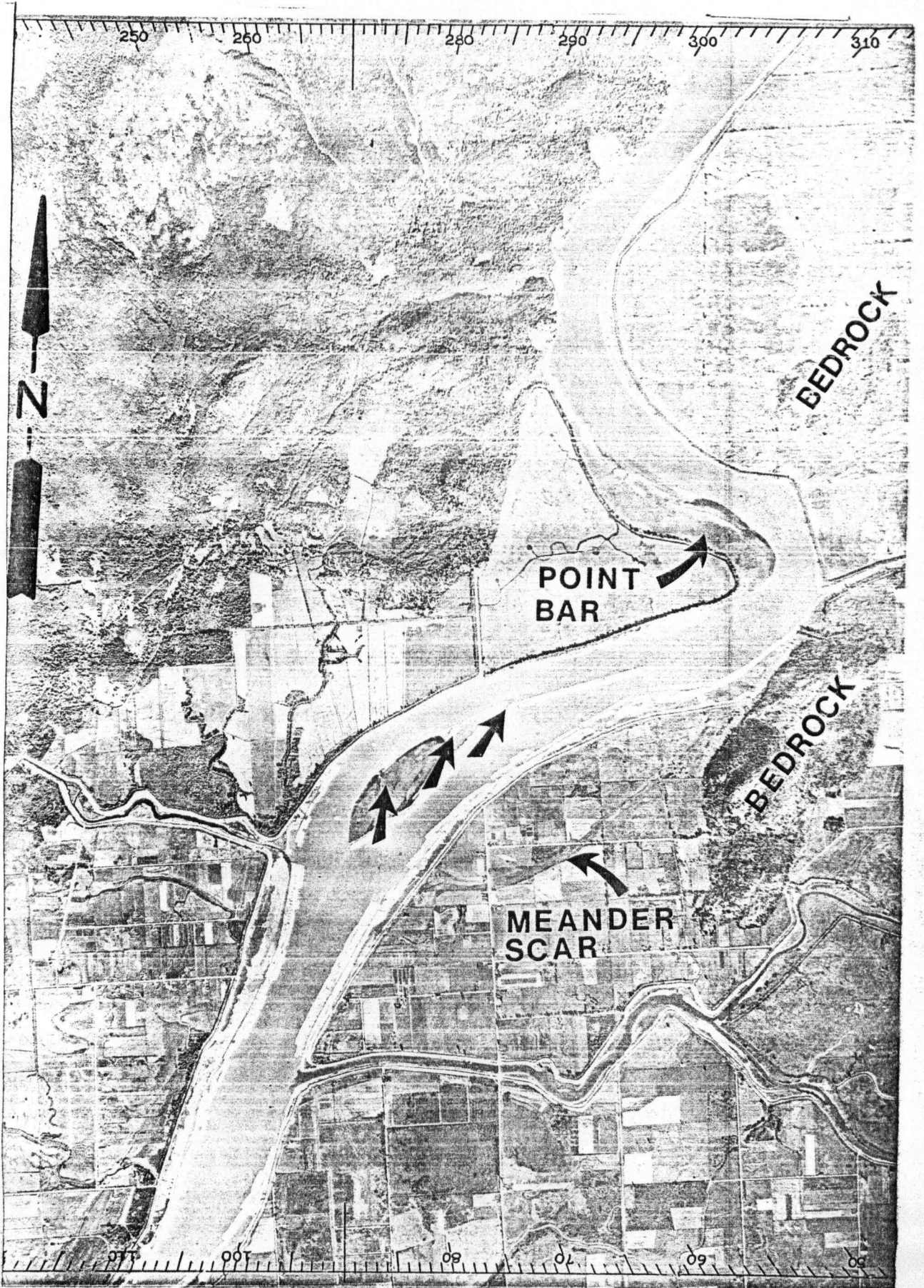
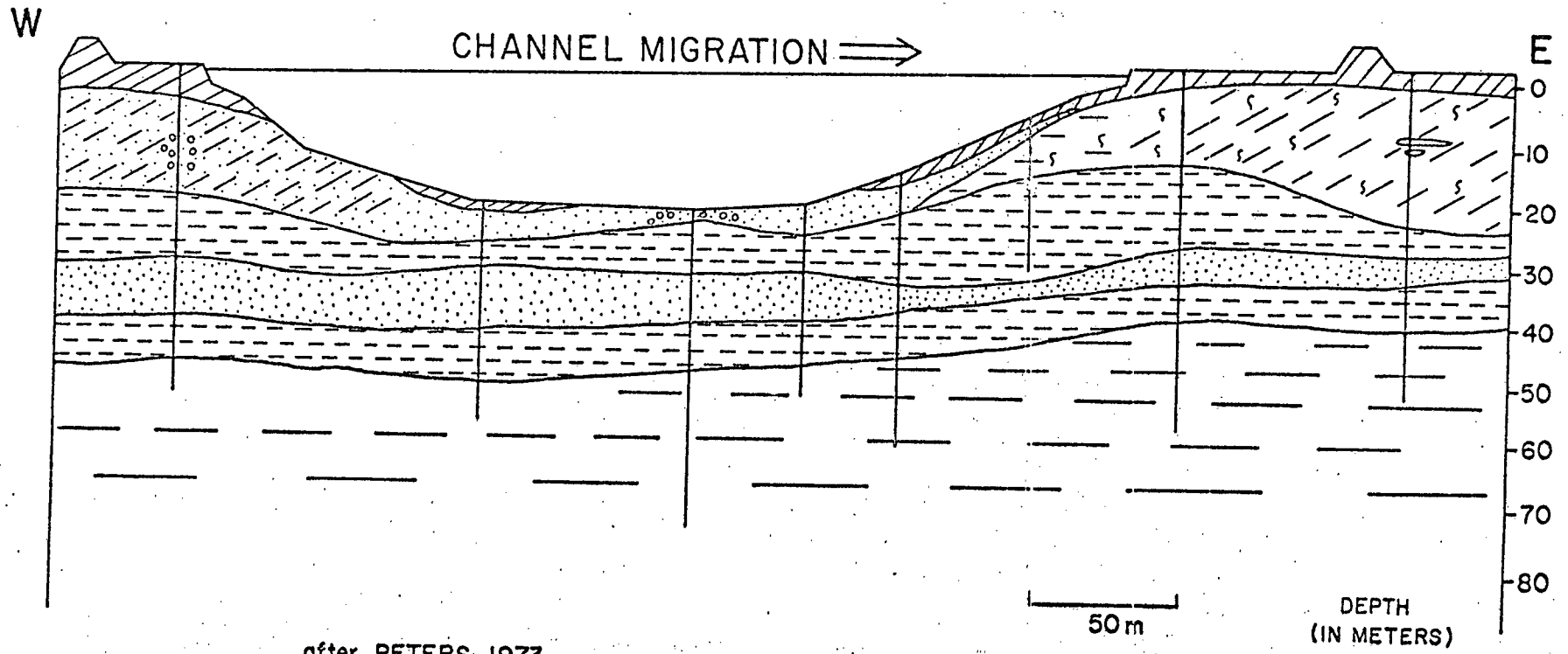
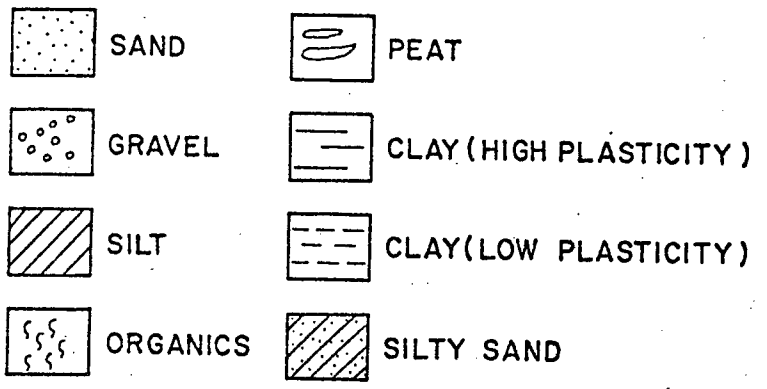


FIGURE 6. Stratigraphic cross section at the bridges.



after, PETERS, 1973



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It is apparent from Figure 3A that the meandering pattern of the river channel is directly related to the meandering pattern of the thalweg trace. Both have an average wavelength ( $\lambda_M$ ) of 6100 m and an average radius of curvature ( $r_M$ ) of 1675 m (excluding the bedrock controlled meander, Fig. 5). Pools located at meander bends and riffles at cross-over locations of the thalweg are both spaced approximately 3000 m apart or five times channel width. A cross section at a pool shows a deep asymmetric channel (Fig. 3A-EF) whereas riffles (Fig. 3A-LK) are shallower and usually more symmetric. A section at the bridges (Fig. 3A-AB) shows a deep symmetric channel which results from the confined flow and scour around bridge pilings.

Leopold and Wolman (1960) stressed the concept that meanders form to lengthen the channel in order to minimize the time rate of energy expenditure. Also that a well developed pool and riffle sequence allows approximately equal expenditure of energy along succeeding reaches of a river. More specifically they found that there is a definite relationship in rivers between discharge, width, and radius of curvature. Figure 7 illustrates a good agreement between their findings and characteristics of the Pitt River.

Figure 8 summarizes the planform geometry of Pitt River. Several prominent bedrock outcrops, in addition to

FIGURE 7. Location of Pitt hydraulic parameter values on Leopold and Wolman's (1960) plot of  $\lambda_M$  vs.  $W$  and  $\lambda_M$  vs.  $r_M$ .  $\lambda_M$  values ranged from 4300 to 8000 m.  $\lambda_M$  values (excluding the bedrock-controlled meander) ranged from 1400 - 2100 m.

LEOPOLD and WOLMAN (1960)

PITT RIVER

$\lambda = 10.9 w^{1.01}$

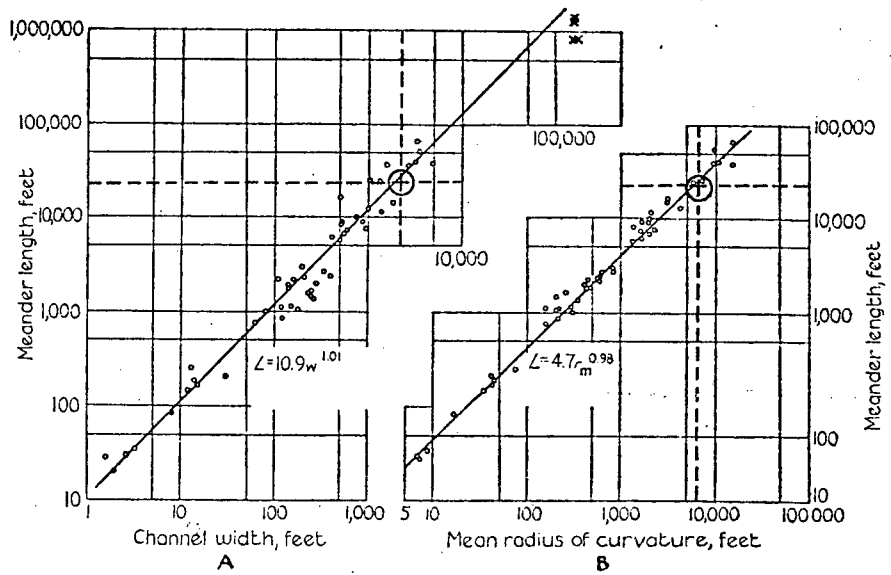
$\lambda = 9.3 w^{1.01}$

$\lambda = 4.7 r_m^{0.98}$

$\lambda = 4.3 r_m^{0.98}$

$r_m/w = 2-3$

$r_m/w = 2.75$



- Meanders of rivers and in flumes
- × Meanders of Gulf Stream
- Meanders on glacier ice

the fine-grained bank material, present physical constraints to channel migration. Either point bars, mid-channel shoals, or mid-channel bars (islands) have developed on the inside of each meander bend. A study was undertaken of the side-scan sonar and depth soundings recorded in all areas of the river to determine the pattern of flow in the channel and the origin of the mid-channel bars. Although details of this study will be covered in the section on bed configuration, results of some aspects are shown in Figure 3A. For this diagram the orientation of large scale two-dimensional bed configurations (15 - 60 m in spacing, 1 - 3 m in height) were noted and flow lines drawn perpendicular to crests. Using this information along with the topography of channel bottom the flow pattern was constructed. In general it appears to fit the converging-diverging flow model of de Leliavsky (1894) taking into consideration the effect of the bridges and bedrock outcrops on flow pattern. The pattern is drawn for the flood direction because the majority of the information available is for flood-oriented flow. Over 65% of the bed configurations on sounding records taken during all seasons and during both flood and ebb flows were flood oriented. The small amount of available information indicates that ebb flow pattern meanders with approximately the same wavelength as the flood and that it crosses the channel at the same locations

(riffles). However, the position of maximum curvature of the ebb flow opposes the position of maximum curvature of the flood (i.e., occurs on the opposite side of river).

In general each mid-channel bar (island or shoal) extends from the riffle area to the point opposite (and usually beyond) the deepest portion of the thalweg at the meander bend. The bars appear to be related to riffle formation. It is interpreted that they form by deposition during diverging flow (Fig. 5) and thus seem to be a physical extension of the riffle. However, since they form on the inside of the meander bend they also occupy the position of the point bar even though they are separated from the inside bank. Thus, at each bend in the thalweg there is either a point bar or a mid-channel bar (Fig. 8). It was not determined in this study why point bars are found at some bends and mid-channel bars at others. It should be noted, however, that point bars occur at bends of maximum curvature. In a normal river point bar deposits accrete on the downstream side of the bar and the deepest area of pools occurs on the downstream end of meander bends. Based on this premise, one may deduce that Point Addington (Fig. 5) is being constructed by flood-dominated flows and channel topography indicates that the flood-oriented current is the channel-forming flow with little modification occurring on the ebb.

FIGURE 8. Diagrammatic sketch of hydraulic geometry of Pitt River.

$A = 3250 \text{ sq. m}$

$W = 610 \text{ m}$

$d = R = 12.1 \text{ m}$

$\lambda = 6100 \text{ m}$

$W/d = 50$

CHANNEL  
LENGTH - 19.8 Km

SINUOSITY 1.20

Q WINTER-FLOOD = 2400 cu.m/sec. (85,000 cu.ft./sec.)

Q WINTER-EBB = 2080 cu.m/sec. (73,500 cu.ft./sec.)

Q FRESHET-FLOOD = 1800 cu.m/sec. (64,500 cu.ft./sec.)

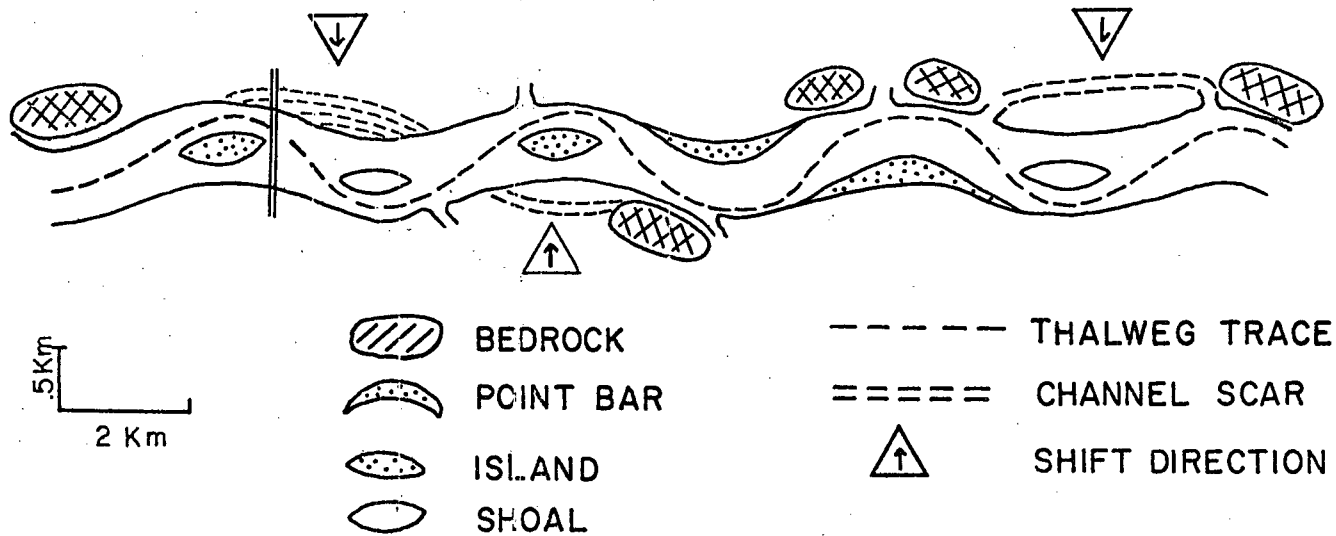
Q FRESHET-EBB = 950 cu.m/sec. (33,500 cu.ft./sec.)

S WINTER FLOOD = +.000053

S WINTER EBB = -.000032

S FRESHET FLOOD = +.000018

S FRESHET EBB = -.000016





The interrelationship of hydraulic variables such as discharge (Q), velocity (V), depth (d), bankful width (W), resistance (n), and water slope ( $S_W$ ) has long been recognized. However, the nature (dependent or independent) of the variables depends upon the hydraulic setting and the time scale under consideration. In the Pitt tidal system, Q and  $S_W$  are independent on both a short- and long-term basis while V, d, W, and n are dependent under both time scales. Q,  $S_W$ , d, W and V can all be measured and total resistance can be determined from a Manning-type equation ( $n = \frac{d_*^{2/3} S^{1/2}}{V^2}$ ;  $d_*$  (mean flow depth) =  $\frac{A}{W}$ ). Leopold and Maddock (1953) specified all five variables as power functions of discharge.

In Pitt River both water slope and discharge reverse direction regularly and vary between opposite maxima. Although, during the freshet when Pitt basin discharge is high, occasionally tidally induced backwater occurs without reversal in flow direction. Because of variable slope and discharge, it is problematic which values should be used to represent the Pitt as a hydraulic system. Both flood and ebb slopes within the Pitt can be calculated from simultaneous stage elevations as a mean over the distance between the stage recording stations (Fig. 1). Maximum possible slope on any flood or ebb of a tidal cycle would be determined by the difference in elevation between the recording stations

(Fig. 9). Discharge on any tidal cycle is determined from a product of velocity at .4 depth (measured from the bed) times an average cross sectional area (A). The actual values were probably slightly less, as the data point on Fraser River is 4 km downstream from the Fraser-Pitt confluence. Also, the maximum (or minimum) elevations in Pitt Lake and Fraser River did not occur simultaneously. The flow is non-uniform and at any point in time the water slope is variable along the system. Flow is also unsteady and the water slope varies with time at any point. To avoid this problem of variable slope, maximum slope values are chosen to characterize each flow direction and be used as a base for comparing flood and ebb flows.

The maximum water slope values for both freshet and winter measured during this study are plotted on Leopold and Wolman's (1957) slope-discharge diagram (Fig. 10). These authors intended the diagram only as a means of separating braided and meandering streams, but it can be used to illustrate the range of slope-discharge values that are found in a sampling of rivers. The Pitt data falls within the meandering regime; however, it is the maximum slope-discharge for the winter ( $2400 \text{ m}^3 \cdot \text{sec}^{-1}$ ) that is closest to the general scatter of river points. This implies that it is the winter discharge not the freshet ( $2080 \text{ m}^3 \cdot \text{sec}^{-1}$ ) which is most effective in defining the channel geometry.

FIGURE 9. Tidal range in Strait of Georgia, Fraser River, Pitt River, and Pitt Lake on four representative days in Dec., Mar., June, and Sept. Maximum mean water slope (ebb or flood) possible on a given day was calculated from the difference in elevation between Fraser River and Pitt Lake.

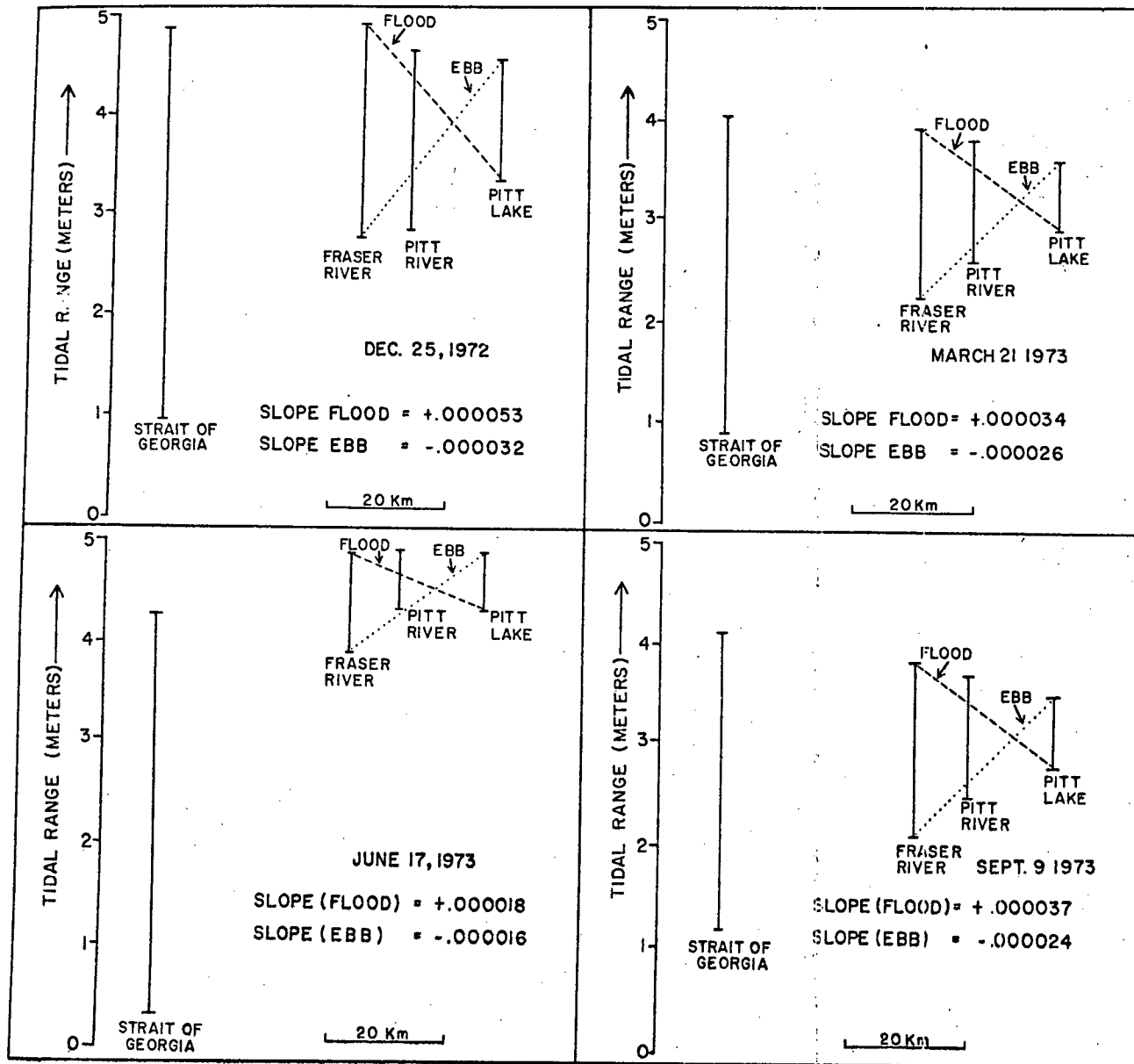


FIGURE 10. Pitt parameters plotted on Leopold and Wolman's (1957) slope-discharge diagram. Pitt values plot with other meandering rivers, but winter values occur closest to the general scatter of points. This implies the winter flow is the channel-forming discharge.



It is important to note that flood water slopes are higher than corresponding ebb water slopes (Fig. 9), and that winter water slopes are significantly higher than those of the freshet. As water slope is the most important driving force in a hydraulic system, it is interpreted that the Pitt system is dominated by winter flood flows.

Although the flow in Pitt River is similar to that in an estuary (bidirectional), the physical setting is significantly different from that of most estuaries. Pitt River is a conduit carrying water between the Fraser River and a reservoir (Pitt Lake) of large capacity. Because the reservoir provides a very large storage capacity, flow through the river is similar to other open channel flows. Energy is dissipated fairly evenly along the channel as evidence by the regular meanders and well developed pool and riffle sequence. However, other characteristics of the Pitt are definitely estuarine; for example, slope and discharge are determined by a complex interaction of the tidal range in the Strait of Georgia, discharge of the Fraser River, and discharge from the Pitt drainage system.

In conclusion, despite its bidirectional flow the geomorphology of the Pitt River has mainly riverine characteristics, rather than estuarine. The effective discharge ( $Q_e$ ) or channel-forming discharge (bankful discharge) appears to be the winter peak flood flow. The

regular meanders, the well developed pool and riffle sequence, and history of channel stability all imply that the processes acting in the river are in "quasi-equilibrium" with its reversing flow and continually changing discharge. The following observation made by Keller and Melhorn (1973) originally intended for unidirectional rivers, applies equally well to tidal Pitt River: "it appears that it is neither processes in alluvial stream channels which entirely control channel form, nor form which entirely controls process. Rather form and process evolve together in harmony as feedback mechanisms inherent to open systems approaching dynamic equilibrium".



## SEDIMENTS

Channel bottom sediments of the Pitt River were sampled and analyzed for grain size distribution and mineralogy in order to compare them to Fraser River sediments and ascertain that the Fraser was their source. Mean grain size of bottom sediments in the Fraser near Pitt River was determined to be 0.42 mm (1.25  $\phi$ ) (Tywoniuk and Stichling, 1973) with a range from 1.41 mm (-0.5  $\phi$ ) to 0.044 mm (4.5  $\phi$ ). This study found a mean grain size of 0.35 mm (1.35  $\phi$ ) in bed material directly off Pitt River mouth.

Cores drilled at the bridges (Fig. 6) and other cores taken by the D.P.W. at kilometers 2 and 8 (Fig. 3A) indicate that the channel is incised into silt and clay (probably older Fraser and Pitt River flood plain deposits). The channel is floored with a relatively thin blanket (5 - 15 m) of sand.

A total of 38 Pitt River samples were collected with a Dietz-Lafond grab sampler. Sandy samples from the thalweg were analyzed in a R.S.A. (Rapid Sediment Analyzer) settling tube of 12.7 cm diameter. Silty samples were sized by a combination of sieve (0.5  $\phi$  interval - following the method of Folk, 1968) and Sedigraph (model 5000, Olivier et al., 1970/71) techniques. A fairly simple pattern of grain

size distribution emerged from the study.

A steady decrease in mean grain size of sediments occurs in the thalweg from 0.37 mm (1.43  $\phi$ ) at Pitt-Fraser confluence to 0.25 mm (2  $\phi$ ) at the entrance to the Lake (Fig. 3B). A disruption of this trend occurs off the mouth of Widgeon Slough where slightly coarser material (mean grain size = 0.34 mm (1.42  $\phi$ )) is debouched into the finer grained sediments of Pitt River, 0.26 mm (1.94  $\phi$ ), resulting in an intermediate size of 0.29 mm (1.78  $\phi$ ). In addition to the longitudinal decrease in size there is a lateral decrease from thalweg to river banks. For example at kilometer 19 mean grain size in the thalweg is 0.26 mm (1.96  $\phi$ ) and decreases to 0.086 mm (3.6  $\phi$ ) and 0.0625 mm (4.0  $\phi$ ) at the inside of the meander. Areas of consistently low velocity such as the location upstream and landward of the bridge abutment have comparatively fine sediments (0.031 mm (5  $\phi$ ) - 0.0156 mm (6  $\phi$ )).

In general sediments are well sorted, with 90% of a given sample occurring within 2  $\phi$  intervals. However, settling tube sizing techniques are insensitive to the small concentrations that occur in distribution tails thus samples may not actually be quite as well sorted as the analyses indicate.

The mineralogy of Fraser River has been examined by MacKintosh and Gardner, (1966); Garrison et al., (1969); and Pharo, (1972). The source material is heterogeneous

(mostly Pleistocene deposits occupying the Fraser drainage basin). A comparison of Fraser River mineralogy with the Pitt system is shown in Table I. Mineralogies and proportions of minerals in the two rivers are essentially identical with a few minor exceptions. Proportion of volcanic rock fragments decrease while proportion of fresh hornblende and plagioclase increase from Fraser River to Pitt Lake.

Widgeon slough has similar mineralogy to Fraser and Pitt Rivers but different proportions: quartz (45%) with no quartzite or chert, feldspar (37%; 30% plagioclase and 7% K-spar), higher pyroxene (7%) and lower rock fragments (2%). Amphibole is mainly green hornblende and generally fresh. Thus, Widgeon Slough possesses a distinct mineralogy characterized by abundant fresh plagioclase, fresh green hornblende and no chert. Because the volume of material contributed by the slough is small in comparison with that contributed by Pitt River, Widgeon Slough minerals soon become diluted. Attempts to trace the direction of sediment movement from Widgeon Slough were unsuccessful.

In conclusion, Fraser River sediments are confirmed as source material for the Pitt River based on (1) essentially identical mineralogies, and (2) a gradual decrease in grain size (within the thalweg) from the Pitt-Fraser confluence up Pitt River to Pitt Lake.

TABLE I Summary of mineralogy of Fraser River, Pitt River, Pitt Lake, and Widgeon Slough.

LOCATION	GRAIN SIZE				
	> 2 $\mu$				< 2 $\mu$
	this study	Garrison et al(1969)	Pharo(1973)	Pharo(1973)	
FRASER RIVER	quartz 10% chert 35% met.rock frag. 15% volc.rock frag. 20% feldspar 11% others 07% hornblende 02%	quartzite, quartz, chert 40% feldspar 11% rock fragments 45% other 04%	quartz feldspar amphibole mica garnet	chlorite montmorillonite illite quartz, feldspar, amphibole	
	Pitt River	Widgeon Slough		Pitt Lake (Pharo, pers.comm)	
PITT SYSTEM  this study	quartz 20% chert 30% met.rock frag. 20% volc.rock frag. 06% feldspar 13% hornblende 04% opaque 04% mica 03%	quartz 45% plagioclase 30% K-spar 07% hornblende 07% mica(biotite) 05% others 06%	chlorite montmorillonite illite quartz, feldspar, amphibole, cuprite (trace)		

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## FLOW AND SEDIMENT TRANSPORT

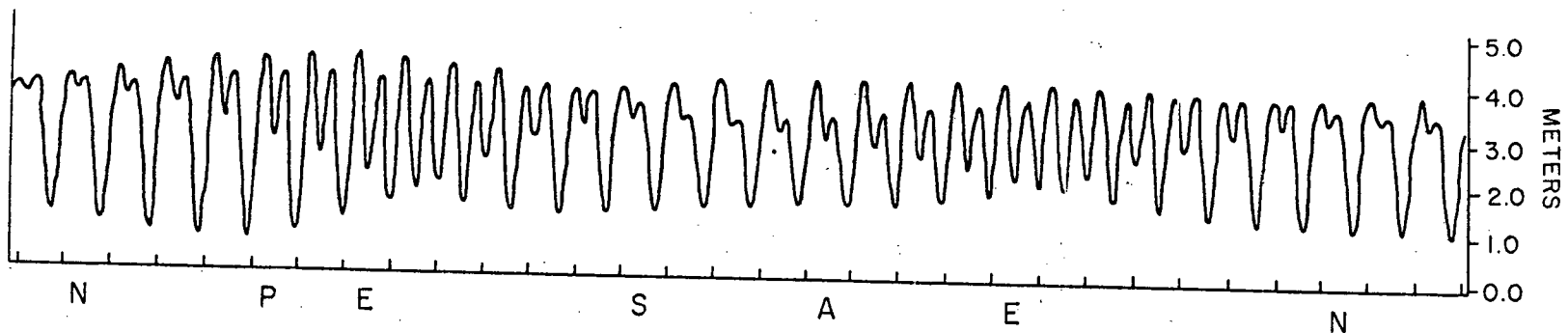
Tides

The tide in the Strait of Georgia is the main driving force behind the hydrodynamics of the Pitt system. The tide is mixed, mainly diurnal, with a range of 3 - 5 meters. In addition to the mixed nature (diurnal inequality) of the tide, lunar cyclic variations also occur (Fig. 11). The difference in height (H) between successive high waters is usually less than the height difference between successive low waters.

In theory (Bowditch, 1962), tides can be thought of as a symmetric water wave with a long wavelength (20,000 km) and short amplitude (30 cm). In a deep ocean this wave form (Fig. 12) would travel from east to west as the earth spins on its axis. The wave form (crest to crest) takes 12 hours and 25 minutes to pass a stationary reference point; i.e., one high tide to the next. Although the wave form moves forward the water motion is up and down. In shallowing water approaching land, frictional drag translates this vertical motion into horizontal motion; i.e., a progressive wave. Drag retards flow in the lower portion of the wave and, as the water level rises, faster moving water near the wave crest begins to overtake the

FIGURE 11. A representative tidal curve (month) for  
Strait of Georgia.

# POINT ATKINSON, BRITISH COLUMBIA



○  
SPRING  
TIDE

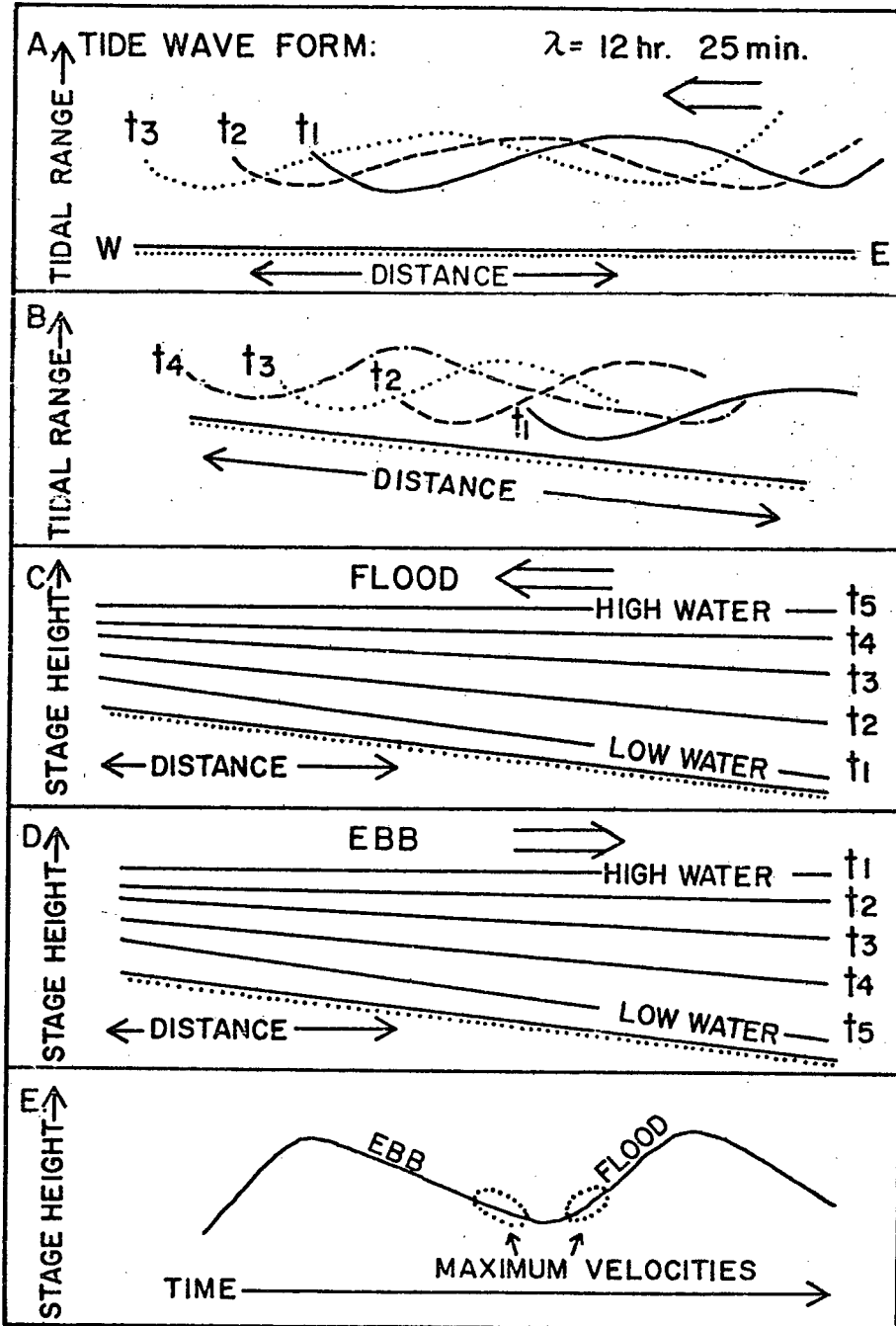


●  
NEAP  
TIDE





FIGURE 12. Tidal theory: (A) Wave form over infinitely deep ocean; (B) Wave form with bottom friction; (C)  $dH/dT$  is highest at beginning of flood, but slows down near high water; (D)  $dH/dT$  is lowest at beginning of ebb and increases toward low water; (E) Maximum velocities occur at end of ebb and beginning of flood.

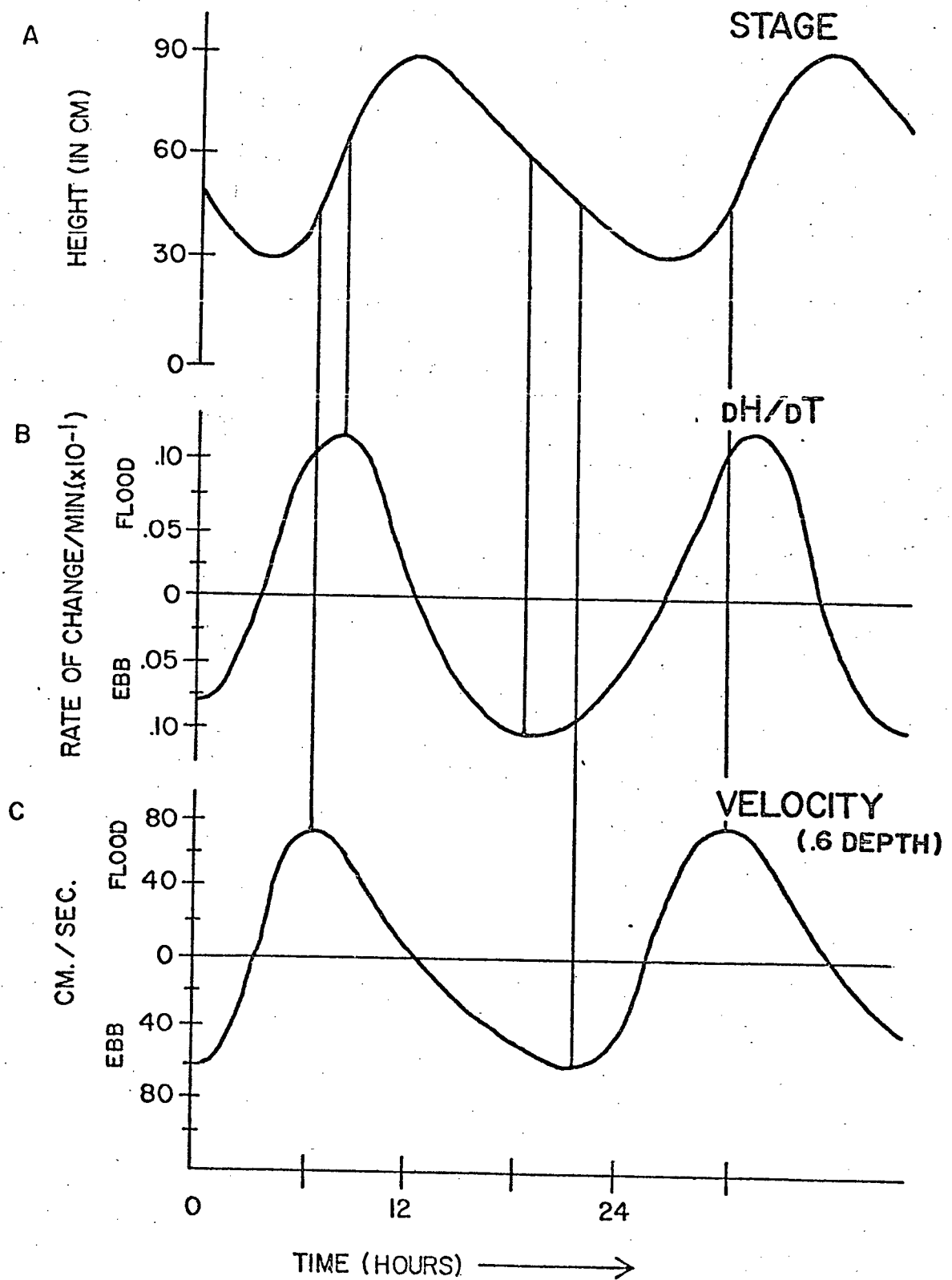


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more slowly moving water at the wave front. An asymmetric wave form is thus developed (Fig. 12B). The asymmetry is accentuated within the confines of the estuarine channel by increased drag caused by boundary (wall) effects. Cross sectional area available for water transfer is reduced, thus altering form of progressive wave. Ignoring tidal backwater effects, stage-time asymmetry increases while magnitude of stage fluctuations, as well as proportion of time devoted to flood decreases (Ippen and Harleman, 1966). Slope ( $dH/dT$ ) of the flood tide wave front is graphically shown with time lines ( $t_1 - t_5$ ) in Figure 12C. On the ebb, water levels drop slowly at first but become faster with time as the water slope becomes greater (Fig. 12D). A stationary observer would see the entire passing tidal wave as a rapidly rising, then slowly falling water level. An idealized  $dH/dT$  plot of Pitt River is shown in Figure 12E where periods of fastest flow (which correspond to times of steepest water slope) are encircled. The relationship in time between stage level, water slope, and velocity (.4 depth measured from base of flow) is illustrated in Figure 13.

The tidal wave form is dampened as it progresses inland from the Strait of Georgia up Fraser and Pitt Rivers and into Pitt Lake. The tidal range is decreased and the shape of the stage level curve is modified. Other things being equal, the greater the magnitude of the tide

FIGURE 13. Stage,  $dH/dT$ , and velocity are asymmetric waves but slightly out of phase.



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in the Strait, the greater the water level fluctuations in the Pitt system. Figure 14 depicts 24-hour  $dH/dT$  curves for the Strait of Georgia (Point Atkinson), Fraser River (Port Mann Bridge), Pitt River (at the bridges), and Pitt Lake (southern end). The four sites are locations of continuously recording stage meters (Fig. 1) (unpublished data, Water Survey of Canada). Both the semi-diurnal (Fig. 14A) and mixed, mainly diurnal (Fig. 14B) tidal curves in the Strait are closely mimicked at the other three locations, but with a considerable time lag (approximately 5 hr and 15 min) between high water in the Strait and high water in Pitt Lake. It takes even longer (6 hr and 20 min) for the low water impulse to progress from the Strait to the lake. The approximate time lags that can be expected for the three inland stations are summarized in Table II.

In addition to the tidally induced oscillations in water level of Fraser estuary and Pitt systems, the absolute level of these oscillations changes seasonally with a maximum during Fraser River freshet run-off (May, June, and July) and a minimum during the winter (Dec., Jan., and Feb.). Discharge contributed to Pitt system from Pitt River (North) and small streams surrounding the lake varies from  $210 \text{ m}^3/\text{sec}$  (freshet) to  $30 \text{ m}^3/\text{sec}$  (winter). The result is that during the freshet more than 50% of water moving through the Pitt system is contributed by



FIGURE 14. Relationship of stage vs. time for four locations (Strait of Georgia, Fraser River, Pitt River, and Pitt Lake) for three representative days in (A) fall (B) winter (C) freshet (spring run-off).

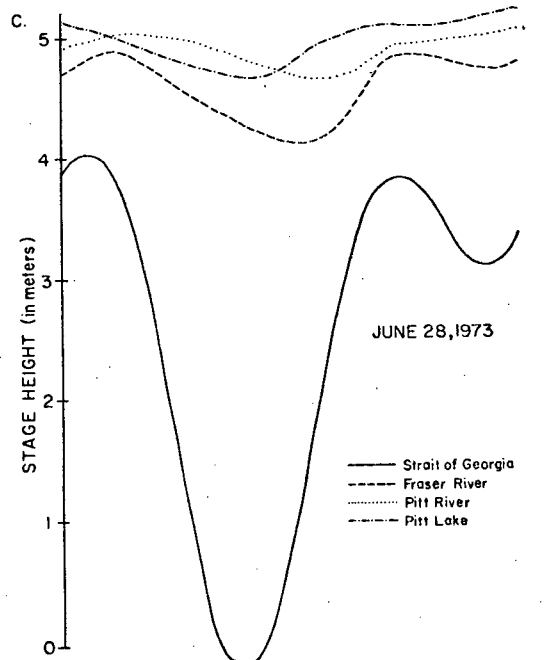
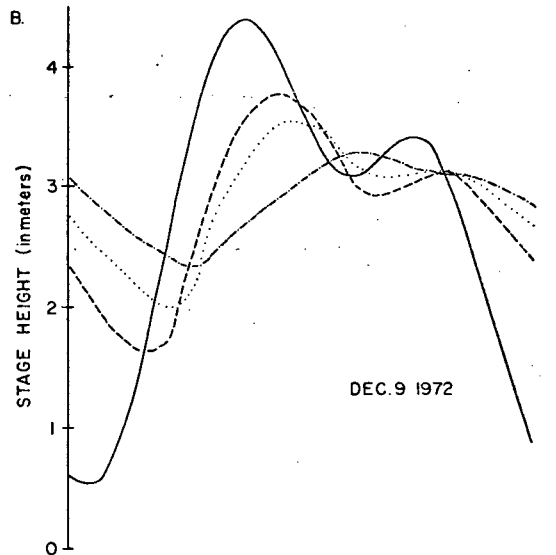
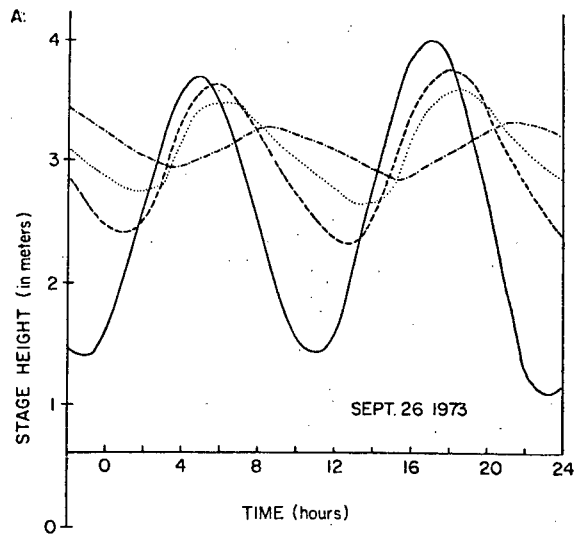


TABLE II Estimations of the delay for low-low water and high-high water to progress from Strait of Georgia to locations within the study area.

STAGE		STRAIT OF GEORGIA	PORT MANN BRIDGE FRASER R.	PITT RIVER	PITT LAKE
High-high Water (Flood Peak)	Freshet	0	2 hr	3 hr 15 m	15 hr 30 m
	Winter	0	1 hr 10 m	2 hr 30 m	5 h 15 m
Low-low Water (Ebb Peak)	Freshet	0	3 hr	4 hr 30 m	15 hr 30 m
	Winter	0	3 hr	4 hr 15 m	6 h 20 m

basin drainage contrasting with only 5% during the winter. Thus, there is an order of magnitude difference between winter and freshet conditions. In the winter (Fig. 14B) when discharge of Fraser and Pitt systems is low, the tidal effect is great. In contrast during freshet when runoff is high, tidal effect is minor (Fig. 14C). Stage fluctuations in Fraser and Pitt are irregular and out-of-phase. On this particular day (June 28, 1973) flow did not reverse in Pitt system.

The progressive nature of the tidal wave form in the Pitt system is reflected by the filling and emptying of the reservoir (Pitt Lake). This can be demonstrated by showing that the volume of water moving through the river during a tidal cycle is approximately equal to the volume lost or gained by the lake. The total volume moved through the river was calculated as the area under the time-discharge curve. Discharge curve for a tidal cycle was determined from a product of mean velocity measured at lake outlet and cross-sectional area ( $4100 \text{ m}^2$ ) at outlet. Total volume moved through river compares favorably with the volume actually added to the lake calculated from the relation: (lake stage height change,  $\Delta H$ ) X (lake area,  $A$ ) + (volume contributed from drainage area during flood flow,  $Q_B$ ) (Table III). The same was true for ebb flows. Total discharge passing through the river is comparable to the

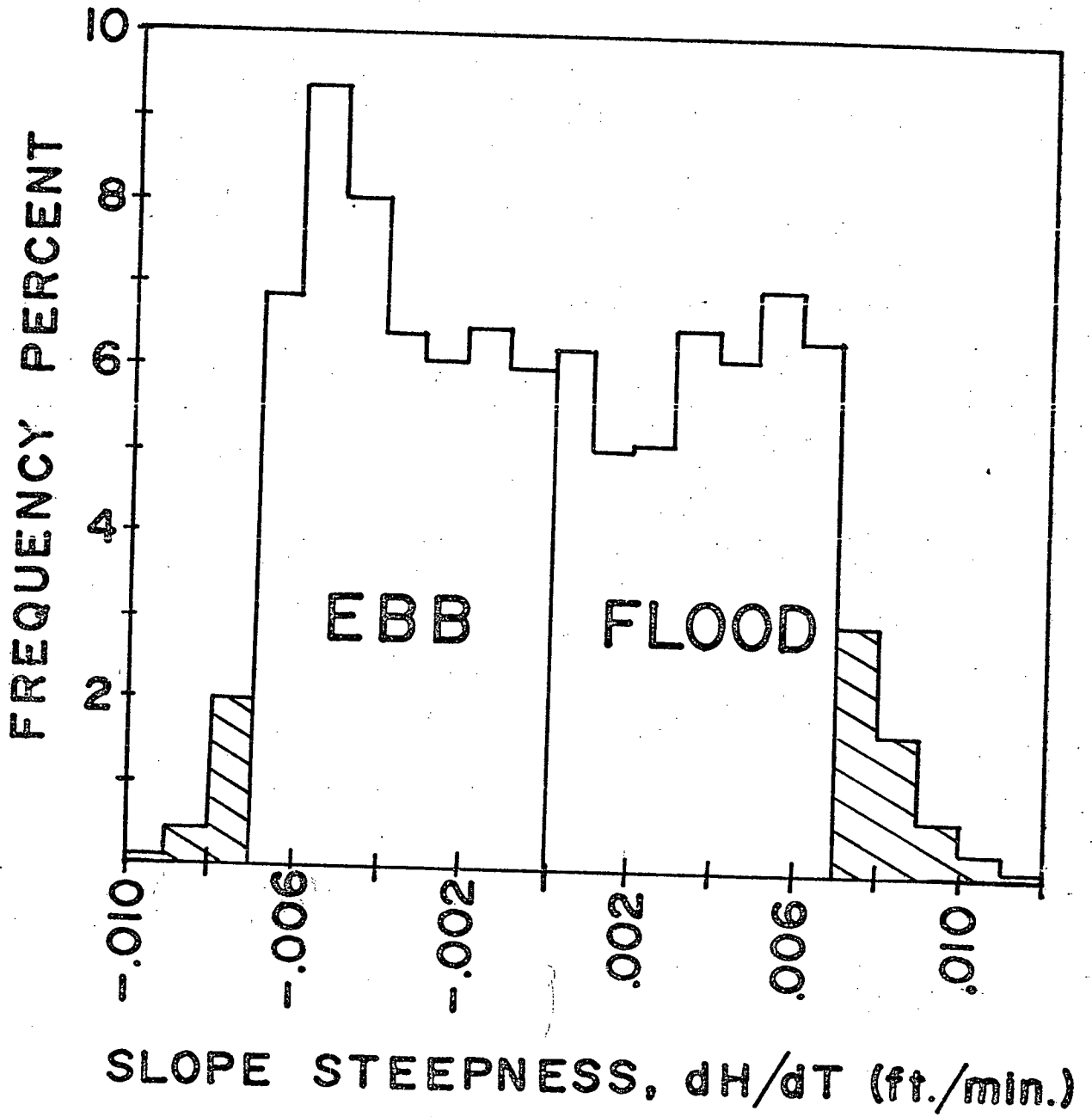
TABLE III Calculations demonstrating total discharge passing through the river is approximately equal to volume added or subtracted from the lake.

FLOOD	EBB
August 13, 1975 - Site (4)	May 9, 1975 - Site (2)
$A = 4100 \text{ m}^2$	$A = 2875 \text{ m}^2$
Flow Duration = 4.5 hrs.	Flow Duration = 8.5 hrs.
(Lake Basin) $Q_B = 113 \text{ m}^3 \cdot \text{sec}^{-1}$	(Lake Basin) $Q_B = 184 \text{ m}^3 \cdot \text{sec}^{-1}$
<u>Lake</u>	<u>Lake</u>
$A_L = 55 \times 10^6 \text{ m}^2$	$A_L = 55 \times 10^6 \text{ m}^2$
$X\Delta H = +.22 \text{ m}$	$X\Delta H = -.63 \text{ m}$
<hr/>	<hr/>
$\text{VOL} = 12.2 \times 10^6 \text{ m}^3$	$\text{VOL} = -34.3 \times 10^6 \text{ m}^3$
<u>River</u>	<u>River</u>
total $Q = 11.4 \times 10^6 \text{ m}^3$	total $Q = -40 \times 10^6 \text{ m}^3$
+ $Q_B = 1.6 \times 10^6 \text{ m}^3$	- $Q_B = -4.3 \times 10^6 \text{ m}^3$
<hr/>	<hr/>
$\text{VOL} = 13.0 \times 10^6 \text{ m}^3$	$\text{VOL} = -35.8 \times 10^6 \text{ m}^3$

volume ( $\Delta HA$ ) that left the lake plus volume supplied by the drainage basin during the time of ebb flow.

Visually, all curves appear asymmetric with steepest slopes occurring on flood tide, implying that discharge and thus velocity is higher on flood. A statistical analysis was undertaken on the frequency of  $dH/dT$  values of Pitt Lake for winter months (Nov. 24, 1972 - April 30, 1973) when tidal effect is greatest. A slight adjustment was made to account for the effect of water volume contributed to the lake by the Pitt watershed. Watershed discharge would be dammed during flood flow increasing apparent rate of lake stage rise. Its continuous flow into the lake during ebb flow would reduce apparent rate of lake stage fall. However, watershed discharge is small, (5%) compared to tidally induced discharge contributed by Pitt River, and its effect is considered minor. It can be seen from the bar graph (Fig. 15) that the bulk of values for both flood and ebb lie below a  $dH/dT$  of .007 ft/min (.213 cm/min). Note that 5.7% of flood values are above this slope compared with 2.5% of ebb values. Thus over a 5-month period flood flows reach higher  $dH/dT$  values indicating higher peak velocities than ebb flows. This flood-dominated trend is confirmed by the velocity measurements presented in the following section.

FIGURE 15. Bargraph illustrating frequency percent of  $dH/dT$  values of Pitt Lake (reflecting rate of infilling) over a 6-month period. Highest  $dH/dT$  values occur on flood flows indicating a higher velocity than on the ebb.





## Streamflow

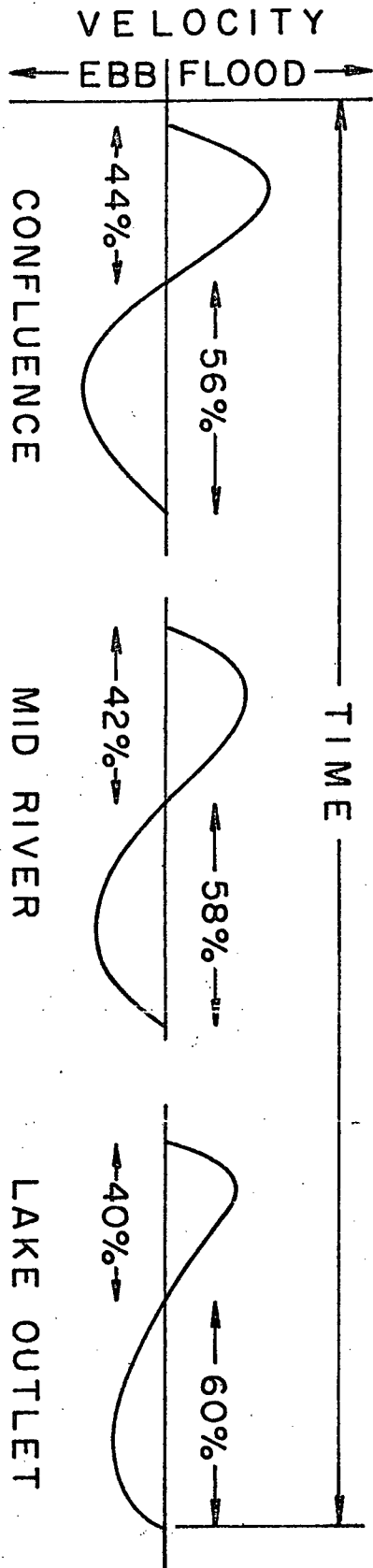
Velocity is one of the more important parameters used to characterize flow and a necessary variable for any sediment transport prediction. Unfortunately, velocity in the Pitt River is variable in direction and magnitude, both daily and seasonally. It was considered important to determine the range of velocities that could be expected to occur during any year, in particular, the maximum velocities and their duration. Two different methods of current measurements were used: (1) readings taken at 7.5-minute intervals, one meter from bottom, for 36 days; (2) current profiles taken at 30-minute intervals for flood or ebb cycles. Portions of 50 days of velocity data in both river and lake channel were taken in hopes of obtaining a representative sampling of the broad spectrum of flow conditions existing in the Pitt system.

Peak mean velocities measured at four sites (Fig. 3B) are summarized in Table IV and show that flood flows are, in general, stronger than ebb. This is true, in particular, when the hydrodynamic control conditions (tidal range in the Strait and Fraser discharge) are the same for the flood and ebb flows being compared. Estuaries with dominant flood velocities are common (Wright *et al.*, 1973; Visher and Howard, 1974; Boggs and Jones, 1976) and, in fact, may be considered the rule for estuaries with low fresh water discharge (Meade, 1969). In all cases total

TABLE IV Summary of peak mean velocities determined from profile measurements; mean is at .4d, measured from bed.

Date	Site	Flood	Ebb	Date	Site	Flood	Ebb
March 11, 1975	(3)	52	40	August 6, 1975	(4)		57
March 13, 1975	(3)	64	42	August 11, 1975	(1B)	59	44
May 9, 1975	(2)		56	August 13, 1975	(4)	34	
May 21, 1975	(2)	40		Sept. 4, 1975	(1B)		62
June 12, 1975	(4)	50		Oct. 8, 1975	(2)	64	38
June 24, 1975	(4)	47		Feb. 20, 1976	(2)	70	
July 9, 1975	(4)		33				

FIGURE 16. Magnitude of velocity and the ratio of flood to ebb duration decreases from confluence to lake.



discharge is greater on ebb than flood because of the volume added by the river. In reconciling this apparent contradiction Visher and Howard (1974) noted higher flood velocities at base of flow and higher ebb velocities at surface, whereas Meade (1969), Wright et al. (1973), and this study have found that flood currents have a higher velocity, but flow for a shorter period of time than the corresponding ebb. In the Pitt system, the proportion of time devoted to flood and ebb flows changes progressively from river confluence to the lake (Fig. 16) with more and more time being devoted to ebb and less to flood.

Current profiles\* were made from a boat anchored at one position in the thalweg during ebb and flood flows and under freshet (May - July) and "winter" (August - April) conditions. Each profile consisted of 8 points (10 cm from bottom, 30 cm from bottom, one meter from bottom, 0.2d, 0.4d (mean), 0.6d, 0.8d, and surface). The measurements (both magnitude and direction) at each depth were based on readings averaged over a two-minute period, thus each profile spans 15 to 20 minutes. A digital counter integrating electrical pulses over a 10-second period was used to average velocity fluctuations caused by micro- and macroturbulence (Matthes, 1947).

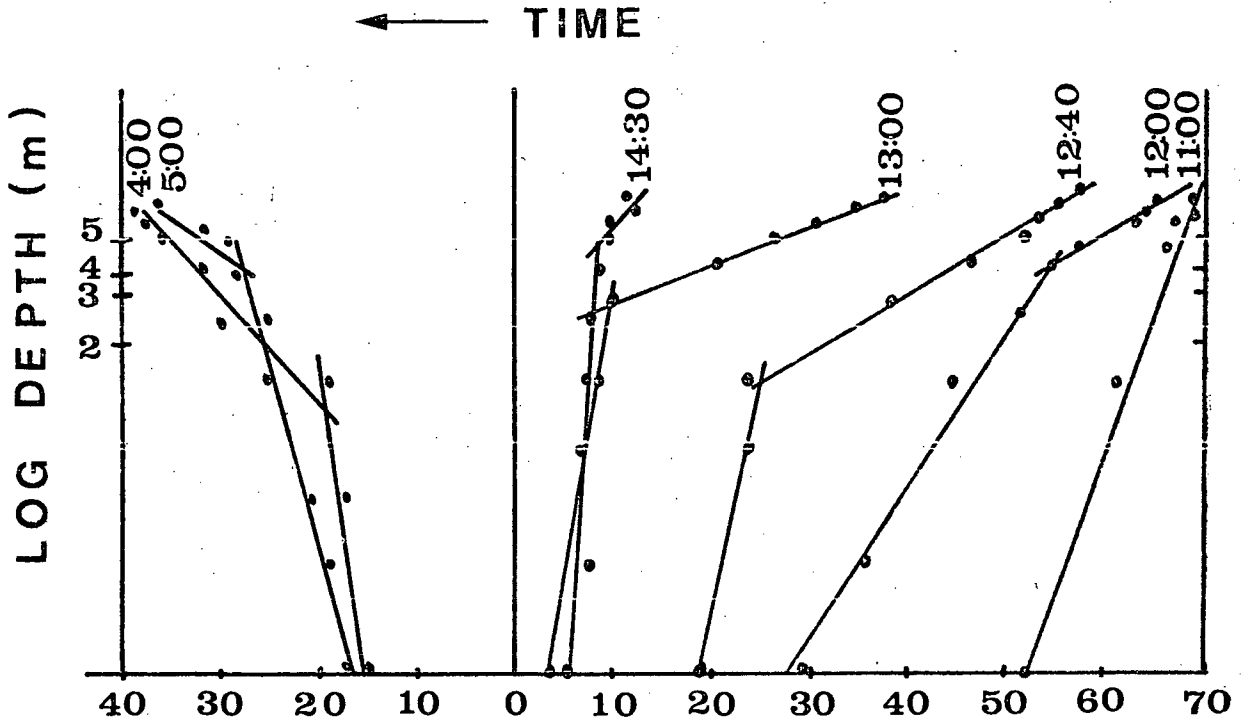
\*Hydro Products, Savonius Rotor with a direct readout for current speed (model #460A) and direction (model #465A).

Profiles reveal that current direction changes gradually from surface to base of flow. The change in flow direction is dominantly to the left and in the order of  $30^\circ$ . Ludwick's (1974) data shows a similar trend, but he makes no comment as to the cause. Unfortunately, the current measurement sites in the Pitt were too few in number to evaluate properly whether this deflection was due to the effect of local channel morphology or some other factor.

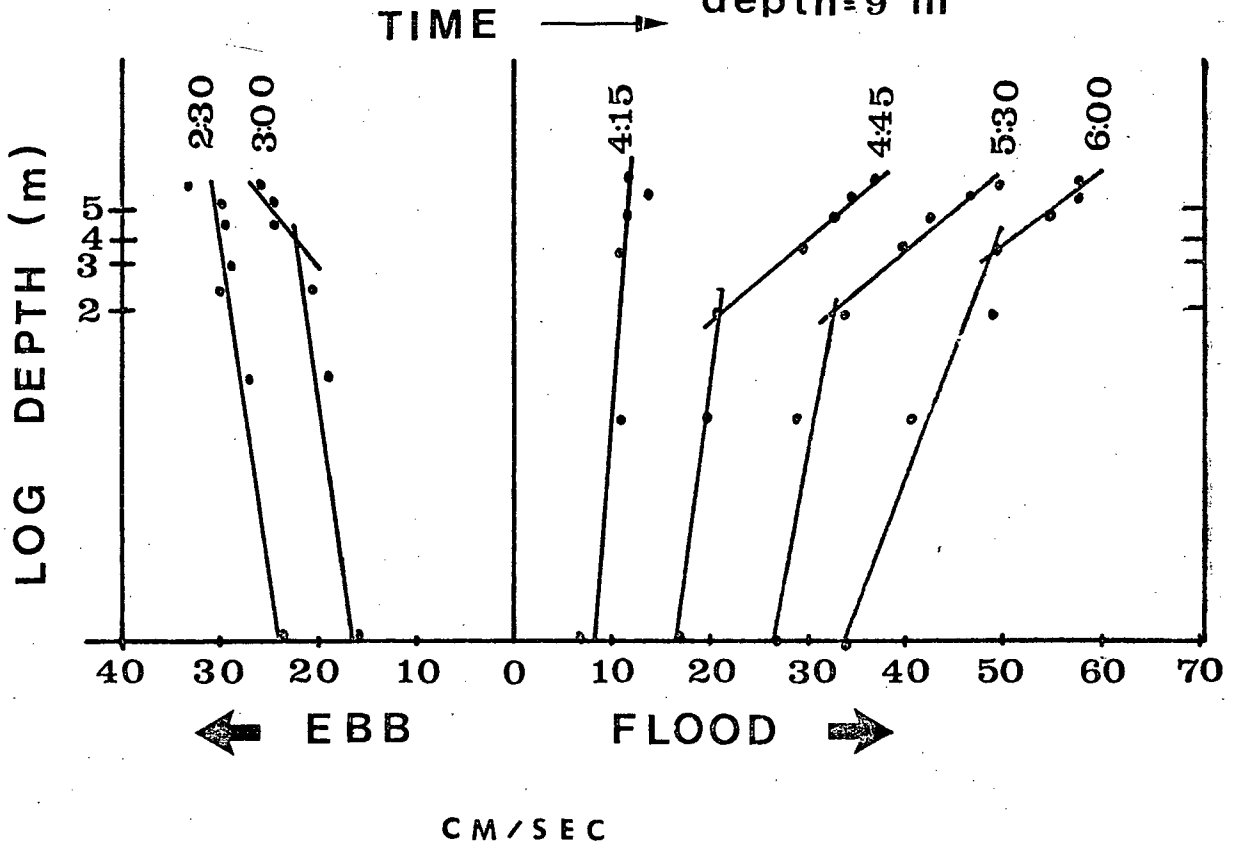
Semi-log plots of velocity data for entire flow depth (boundary layer) reveal that most profiles are composed of two distinct zones. The break between the zones occurs between 2 m and 4 m above the bottom (Fig. 17). Within each zone the profile generally shows a logarithmic variation of velocity with depth ( $d$ , distance above the bed), however the slope ( $d \cdot V / d \log d$ ) is higher in upper zone. The slope steepness changes during acceleration and deceleration of both flood and ebb oriented flows. Large-scale bedforms (1 - 3 m in height) cover the channel bottom and it is possible that their presence is instrumental in the development of the two zones. Considerably more data is needed to determine how flow structure changes during a tidal cycle and to ascertain the relationship between bedforms and the presence of flow zones.

FIGURE 17. Velocity profiles taken at A. Site 2 B. Site 3.  
Flow is divided into two distinct zones.  
Velocity varies logarithmically with depth,  
but at different rates in each zone. Division  
between the zones is at 2 - 4 m from bed.  
Flow structure may be related to bedforms  
(1 - 3 m in height) present on channel bottom.

OCT. 8, 1975  
depth = 12.2 m



MARCH 11, 1975  
depth = 9 m





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Arithmetic depth-velocity plots indicate that the shape of "typical" flood and ebb curves are distinctly different for a given mean velocity (Fig. 18A). The shape of a velocity-depth plot depends mainly on extent of drag imposed on the flow. For a given depth, the greater the drag the greater the turbulence, which in turn produces a more gradual velocity profile toward the bed. Bedforms on channel bottom are predominantly flood oriented and the form resistance (drag coefficient) would be expected to change between flood and ebb. The slope angle of the exposed bedform surface (stoss side) presented to ebb flow is greater than slope angle of the surface (lee side) opposing flood-oriented flows (Fig. 19). Thus, it is interpreted that more drag occurs on the ebb resulting in a more gradual velocity profile toward the bed. Although Znamenskaya (1967) has attempted to relate bedform geometry and flow resistance, few quantitative data are available for the types of large-scale bedforms found in the Pitt River.

Velocity measurements taken near the Pitt-Fraser confluence (Fig. 3, site 1B) (Fig. 18B) are considered typical of most profiles measured. These time-velocity curves were drawn by eye to average scatter which presumably is due to low-frequency velocity fluctuations. Plots of mean velocity, velocity one meter from bottom and

FIGURE 18A. Diagrammatic comparison of "typical" flood and ebb current profiles.

FIGURE 18B. Velocity vs. time plot of data taken August 11, 1975 at current measurement site 1B (Fig. 3B). Line drawn at 32 cm/sec illustrates amount of flood time above critical velocity is greater than that of ebb. Bottom actually is 10 cm from bottom.

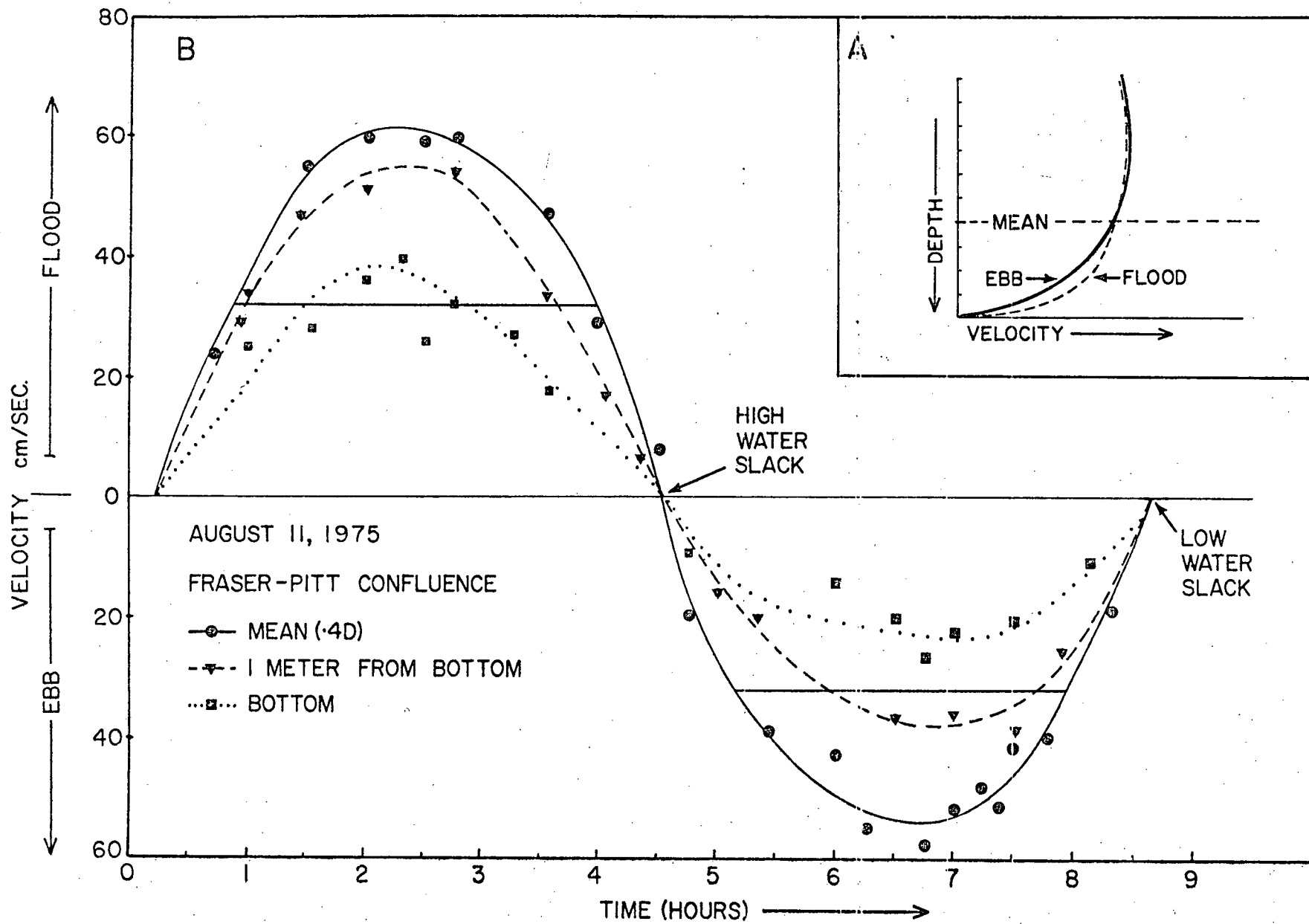
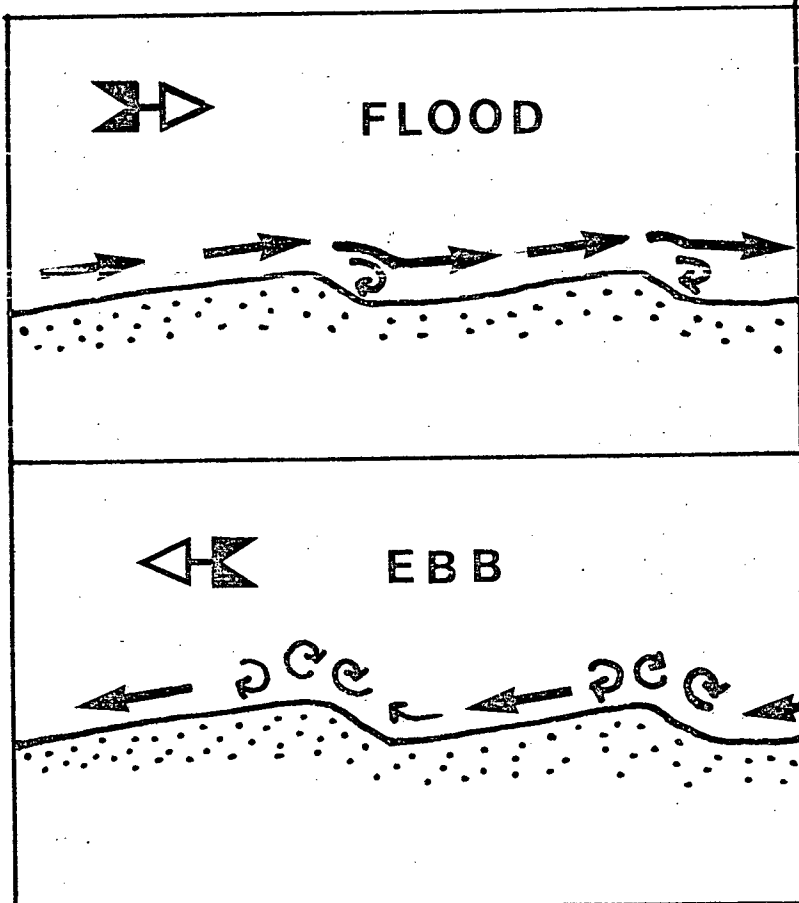


FIGURE 19. Diagrammatic comparison between flood and ebb flows of turbulence created by the flood-oriented flows.



10 cm from bottom all exhibit similar shapes. The difference between flood and ebb mean velocity peaks is 7 cm/sec, however, the difference at one meter from bottom is substantially greater (17 cm/sec). Visher and Howard (1974) noted a 20 cm/sec difference at one meter in Altamaha Estuary, whereas, Klein (1970) found only 6 cm/sec difference at one meter from bottom in the portion of the Midas Basin characterized by flood-oriented sand waves. It should be noted that, in the Pitt, if an ebb or flood flow were of equal strength (equal mean velocities) the velocity near the base and thus basal shear stress and sediment entrainment potential would be greater for the flood. This is a consequence of the basic difference between the flood and ebb profiles (Fig. 18A). At first glance this interpretation may appear to contradict theory which assumes that turbulence intensity and shear increase together. However, the portion of total flow resistance borne by form resistance or that utilized on the grains differs between ebb and flood. On ebb, a greater portion of the resistance is borne by form resistance (Einstein and Barbarossa, 1952) because of increased drag (Fig. 19). The opposite is true of the flood where a greater portion of resistance is available for shear at grain level. It is only that portion of total resistance imparted on the grain which may lead to sediment entrainment.

The continuously recorded velocity measurements were taken by a positively buoyant meter (General Oceanics, Inc. film recording current meter (model #2010)), which was anchored to the channel bottom (Fig. 3B, site 1A) but free to sway with changing currents. The meter recorded on movie film instantaneous readings of magnitude and direction of flow (one meter off bottom) at 7.5-minute intervals. The meter was placed at sites 1A through 5 on a total of 7 occasions. Due to equipment failure only two readable records were obtained: a 17-day record in the river of site 1A (March, 1976) and a 19-day record at site 5 in the lake channel (Ashley, 1977). Portions of the river record are shown in Figure 20 and Table V gives a comparison of the proportion of time devoted to ebb and flood flow. Not only was a longer period of total time (56%) devoted to ebb flow than to flood (44%), but more time was devoted to ebb at any given velocity level. Since all other aspects of this study and others (Johnston, 1922; Morton, 1949; Ages and Wollard, 1976) point to a flood-dominated system these apparent anomalous data require examination.

The area of the Fraser-Pitt confluence is likely to be dominated by the hydrodynamics of the Fraser rather than the Pitt. Milliman (1977) has noted that ebb velocities in Fraser River are related to tidal range. Thus, analysis was made of data from site 1A and Pitt Lake channel



(site 5) to determine if a similar relationship existed. A strong correlation ( $r = 0.866$ ) was found in 1A data between tidal range in the Strait of Georgia and peak ebb velocity (Fig. 20, Table VI) and a poor ( $r = 0.064$ ) correlation between peak flood velocity and tidal range. Peak velocities were based on an average of highest velocities over a 30-minute period. On the other hand, the lake channel data show a moderately good correlation ( $r = 0.631$ ) between peak flood velocity and a poor one ( $r = 0.266$ ) for peak ebb velocity. A negative correlation exists between Fraser River discharge and peak velocities at both sites under both flood and ebb flows. Thus, it is concluded that data from site 1A are strongly influenced by Fraser River conditions. To reinforce this conclusion a similar but more detailed comparison was made of site 1B (100 m upstream from site 1A) and site 5 against site 1A all under approximately equal tidal ranges (Table VII). Sites 1B and 5 both show a slight flood dominance interpreted as representing Pitt conditions while site 1A demonstrates a strong ebb dominance considered typical of the Fraser River.

An additional factor concerning site 1A data is that the meter site may have biased measurements taken such that most of the ebb discharge was recorded, but only a portion of the flood. Position of flow lines with respect to the current meter, determined by velocity measurements with the

TABLE V Summary of "continuous" velocity data (March 16 - 31, 1976);  
770 total hours of measurement at site 1A.

Time greater than;	EBB			FLOOD		
	Hours	Hrs(cum)	Cum. %	Hours	Hrs(cum)	Cum. %
80 cm/sec	15	15	2.0	1	1	0.0
70 cm/sec	20	36	4.6	2	3	.35
60 cm/sec	21	57	7.3	11	14	1.7
50 cm/sec	76	133	17.2	55	68	8.8
40 cm/sec	109	242	31.4	79	147	19.0
30 cm/sec	72	314	40.8	92	239	31.0
20 cm/sec	43	357	46.0	34	273	35.0
10 cm/sec	40	397	51.0	39	312	40.5
0 cm/sec	35	432	56.0	26	338	44.0

FIGURE 20A. Computer plot of velocity data from site 1A (Fig. 3B). Each data point represents an instantaneous recording of velocity taken at 7.5-minute intervals, one meter off bottom. March 17 - 18, 1976; mixed, mainly diurnal tides.

FIGURE 20B. A strong correlation exists between the tidal range in Strait of Georgia and maximum ebb velocity in current measurements taken at site 1A (March 16 - 31, 1976) (Fig. 3B). This implies data represents Fraser River hydraulics and not Pitt River.

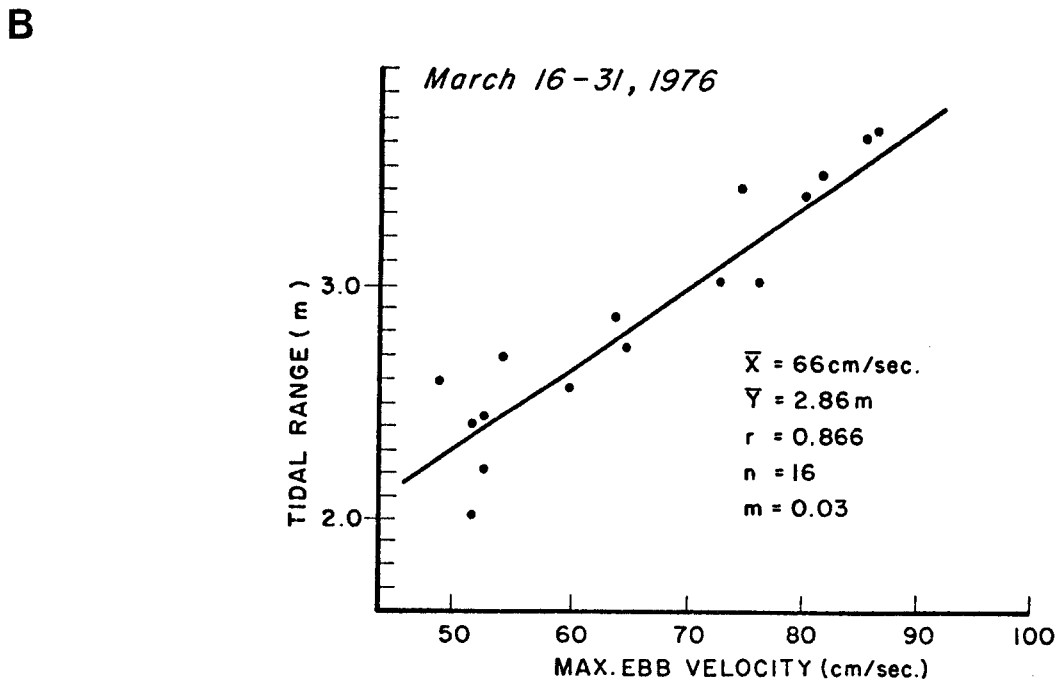
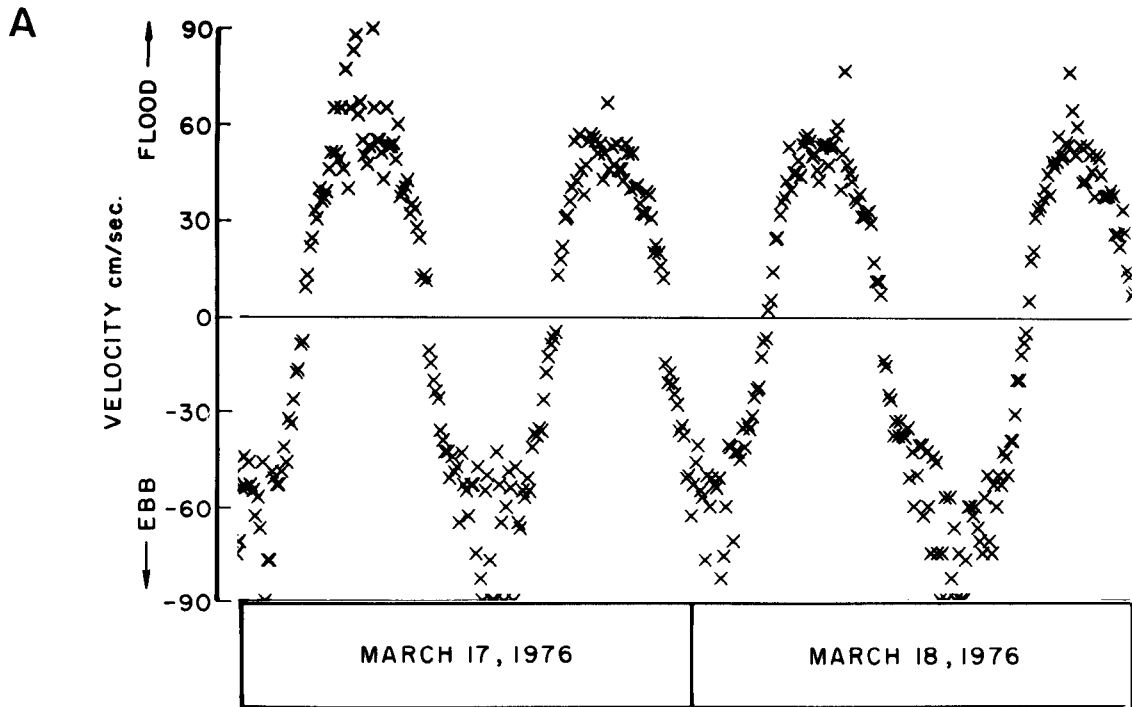


TABLE VI Relationship between tidal range (Strait) and peak velocities attained in Pitt system; Fraser discharge and velocities attained in Pitt system.

Site	Date	Tidal range (Strait) vs. peak vel.		Fraser Q vs. peak vel.	
		Ebb	Flood	Ebb	Flood
1A	3/16/76- 4/1/76	+0.866	+0.064	-0.116	-0.59
5	4/16/76- 5/4/76	+0.266	+0.631	-0.38	-0.165

TABLE VII Comparison of maximum mean velocities reached in Pitt system under similar tidal ranges but differing Fraser discharge.

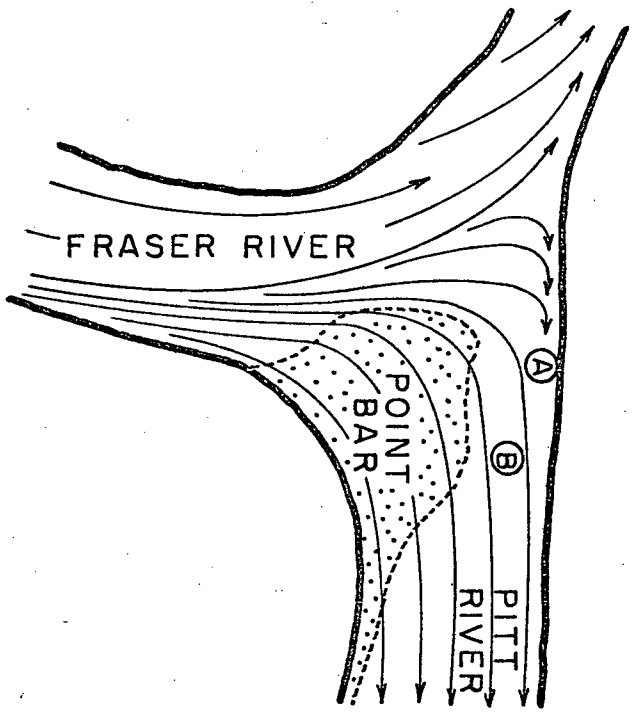
Meter site	Date	Tidal range (in Strait)	Fraser discharge	Max. mean flood vel.	Max. mean ebb vel.	Reference
1A	3/24/76	2.8 m	1020 cu m/sec	62 cm/sec	82	Fig. 17
1B	8/11/75	2.9 m	3285 cu m/sec	62 cm/sec	56	Fig. 18
5	4/28/76	2.8 m	3060 cu m/sec	54 cm/sec	38	Ashley, (1977)

Savonius rotor current meter and drogue observations are significantly different for ebb (Fig. 21A) and flood (Fig. 21B). Flood currents diverge and spread out across the Pitt River entrance while ebb currents converge and are concentrated near the west bank directly over meter site. Thus, it is concluded that the flow pattern can be more complex locally than the simple one presented in Figure 3A. In addition no one site by itself should be expected to exhibit average flow conditions for the entire river.

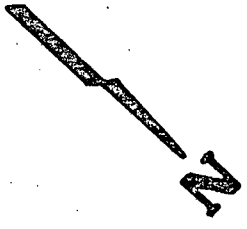
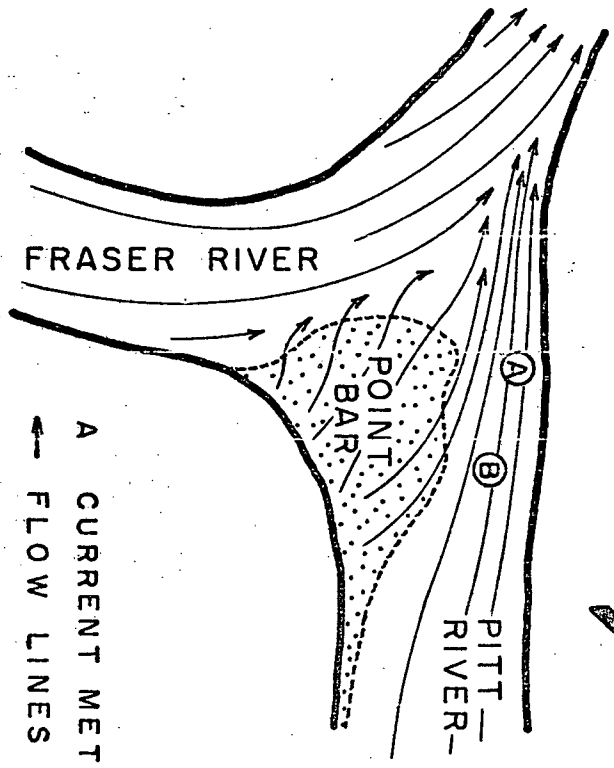
Both flood and ebb time-velocity plots are asymmetric. The asymmetry becomes more pronounced from confluence to lake in conjunction with a gradual decrease in the magnitude of peak velocities (Fig. 16). Peak velocities occur early in flood and late in ebb (Fig. 12E; Fig. 13) with reasons for this illustrated in Figure 12. The net result of the timing of peak flows is that the time before and after "low water slack" contains periods of high velocities on both flood and ebb. In contrast, time near "high water slack" has periods of relatively low velocities. This phenomenon is fairly common in estuaries (Postma, 1967) but not necessarily characteristic of all. The fact that stage and velocity cycles are out of phase plays an important part in the mechanism of sediment transport up the Pitt River. This mechanism will be outlined in the following section on sediment transport.

FIGURE 21. Flow pattern of flood (A) and ebb (B) at Pitt-Fraser confluence.

A) FLOOD



B) EBB



A CURRENT METER  
— FLOW LINES

500 m



In summary, velocity data collected in this study indicates that flood flows generally exhibit higher mean velocities but for shorter durations than ebb flows. The superiority of flood currents results from the asymmetry of the tidal cycle: i.e., the flood stage rises faster than the ebb stage falls. Thus, the unequal flow is a control imposed upon the system. However, sediment is introduced at the downstream end and is transported upstream as flood-oriented bedforms. The geometry of the forms alters the velocity of ebb currents and apparently reduces their capability of entraining sediment in comparison to flood currents. It is inferred then, that the flood-dominated nature of the Pitt River is maintained by a type of feedback mechanism.

#### Sediment transport

The study of mobile bed hydraulics, has advanced mainly by laboratory flume studies based on well established fluid mechanics principles. Unfortunately, applications of small-scale laboratory models to the large-scale reality of sediment transport in rivers has had only limited success. One of the major problems is that the equilibrium state of the river is difficult to determine on both a short and long-term basis. Thus, in examining behavior of natural streams it is important to differentiate between short-term (hourly) and long-term (yearly) interaction of

channel and discharge. This is particularly important in Pitt River, where bidirectional, unsteady, and seasonal flow variations are the norm. The following section investigates the short-term (tidal cycle) interaction of water and sediment by examining conditions of sediment entrainment and long-term (seasonal) interaction by estimating total volume of sediment moved through the system in a year.

#### Bed load

The most challenging question related to the tidal Pitt system is how net water flow can be out of Pitt Lake while net sediment movement is in the opposite direction. Meade (1969); Wright et al., (1972); and Wright et al., (1973) have all noted a similar landward transport of sediment in other estuaries, explaining it in terms of salt wedges. The Pitt freshwater system clearly requires a model which is not based on the density difference between fresh and salt water. The steeper water slopes and higher velocities generated on the flood tide have been documented in previous sections and appear to provide a driving force for landward sediment transport. Sediment is continuously supplied to the lower Pitt River by its source (Fraser River). At the same time the gradational change in the hydrodynamics of the Pitt from the Fraser confluence to Pitt Lake (Fig. 16) may explain the systematic

decrease observed in mean grain size up the river. To evaluate quantitatively these effects calculations have been carried out on the shear velocities necessary to entrain sediments.

Critical shear stress necessary for sediment entrainment, under various temperatures, was determined from Shields' diagram as modified by Briggs and Middleton (1965). The largest grains found near Pitt-Fraser confluence (and also in entire river) are 0.59 mm (0.76  $\phi$ ), with mean grain size being 0.37 mm (1.43  $\phi$ ), 0.28 mm (1.83  $\phi$ ), and 0.25 mm (2.0  $\phi$ ) at confluence, mid-river, and lake outlet, respectively. Table VIII summarizes shear stress, calculated for winter (5°C), spring and autumn (10°C), and summer (15°C) conditions.  $\lambda_0$  necessary to move the largest grains in winter is 3.14 dyne-cm/sec or a shear velocity  $V_*$  of 1.77 cm/sec., whereas  $V_*$  of 1.36 cm/sec will move mean grain size (0.25 mm) at lake outlet.

To estimate the extent of sediment transport on the flood and ebb it is necessary to determine flow conditions under which the critical shear velocity is reached and their duration. Charnock (1959), Sternberg (1966), and Nece and Smith (1970) have all measured current velocity profiles within 2 meters of the bottom in areas of fully turbulent tidal currents and verified that the profile near an hydraulically rough bed can be represented by the logarithmic flow law. Sternberg (1968) found 85% of his tidal

TABLE VIII Critical shear stress values determined from Shields' (1936) graph.

Grain Size mm	Temperature °C	Dynes-cm/sec $\tau_0$	$V_*$ cm/sec
.59	5	3.14	1.77
	10	3.10	1.76
	15	3.05	1.74
.37	5	3.51	1.58
	10	2.33	1.52
	15	2.15	1.46
.28	5	2.26	1.50
	10	2.08	1.44
	15	1.94	1.39
.25	5	2.18	1.47
	10	2.06	1.43
	15	1.85	1.36

channels had logarithmic velocity profiles. This suggests the validity of applying the von Karman-Prandtl law of the wall:

$$\frac{V}{V_*} = \frac{2.3}{K} \log \left( \frac{d+z_0}{z_0} \right) \quad (2)$$

where  $K$  is von Karman's constant, assumed to be 0.4,  $V$  is velocity at depth,  $d$  (measured from bed), and  $z_0$  is some measure of height of roughness elements at the boundary (i.e., grain size). Knowing  $z_0$  to be small in comparison to  $d$ , the equation can be rewritten:

$$\frac{V}{V_*} = 5.75 \frac{\log d}{\log z_0} \quad (3)$$

Because it is a straight line

$$V_* = \frac{\frac{d}{d} \frac{V}{\log d}}{5.75} + \log z_0 \quad (4)$$

where 1. slope of line =  $\frac{d}{d} \frac{V}{\log d}$

2. intercept =  $z_0$

$$3. V_* = \sqrt{\frac{\tau_0}{\rho}}$$

Total depth of flow ranged from 9 m in the river to 42 m at the lake outlet, however only the bottom (2 - 4) meters plotted consistently as a straight line on a semi-log plot of velocity vs. log depth (Fig. 17). Basal shear velocity,  $V_*$ , was determined using equation (4) on the bottom 4 meters of each velocity profile for a total of 130 profiles on the 14 different days listed in Table IV. Measurements used were usually 10 cm, 30 cm, 100 cm, 200 cm, and 400 cm above bottom..

Unfortunately, velocity profile measurements were taken sequentially with one meter and not with an array of several. Thus, resulting shear stress calculations are only an approximation of conditions at bed. For more precise measurements a current meter array or Preston Tube (device for measuring Reynolds Stress directly) should be used. Nece and Smith (1970) have demonstrated that both methods produce comparable results. An additional problem is revealed by Dyer (1972) who found that the relationship of bed configuration and position of profile is important. He found that friction velocity can differ by as much as a factor of two depending upon location of the profiles relative to bedform morphology. Highest shear stress occurs near the bedform crest, lowest in the trough. However, it is important to note that the bedforms in Dyer's study had a wavelength of 200 m and a height of 7 m compared with the 15 - 60 m and 1 - 3 m in the

Pitt. Thus, the uncertainty in the location of current profiles relative to bedforms may be less critical in Pitt River than Dyer's data suggest. Despite these problems, the consistency of the data and the qualitative agreement in the relation between  $\tau_o$  and  $\bar{V}$  with both Ludwick's (1974) and Gordon's (1975) studies support the validity of the data.

$V_*$ ,  $\tau_o$ , and  $\tau_o \bar{V}$  (stream power) calculations for one day's data (Fig. 18) are summarized in Table IX. It is important to note that shear stress changes proportionally with increase in mean velocity. This is not true with decelerating flow, as  $\tau_o$  remains high then drops off rapidly. More specifically, shear stress is usually higher for the same mean velocity on decelerating flow than for accelerating flow. Shear stress was not seen to increase after peak mean velocity. McCave (1973) and Gordon (1975) have both noted a similar "hysteresis" in the relationship of shear stress and mean velocity. Kachel and Sternberg (1971) noticed an increase in bed load transport as ripples during decelerating flow. Gordon (1975) suggested that the increase of shear on decelerating flow occurs when longitudinal pressure gradient changes from favorable to adverse with change of stage. Because of the hysteretic relationship found in Pitt River, predictions of sediment entrainment using mean velocity as an indication of friction velocity will be minima.

TABLE IX  $V_*$ ,  $\tau_o$ , and  $\bar{V}_{\tau_o}$  calculations for August 11, 1975 at Pitt-Fraser confluence.

Time	$dV/d\log d$	$V_* \frac{cm}{sec}$	$\bar{V}$ cm/sec	$\tau_o$	$\bar{V}_{\tau_o}$	$\bar{V}_{\tau_o}$ ave. time-weighted	
FLOOD							
9:30	13.73	2.38	34	1.54	52.4	88.7	
10:00	18.28	3.17	55	1.78	97.9		
10:30	16.00	2.78	61	1.66	101.7		
11:00	26.59	4.62	57	2.15	122.0		
11:15	16.07	2.79	59	1.67	98.5		
12:00	15.86	2.75	44	1.65	72.9		
-----							
1:00	6.61	1.15	05	1.07	5.4		
-----							
EBB							
1:15	10.72	1.86	25	1.36	34.0	76.8	
2:30	27.59	4.79	40	2.19	87.5		
3:00	24.44	4.25	54	2.06	111.0		
3:30	21.20	3.68	47	1.91	90.0		
4:00	21.89	3.80	42	1.94	81.8		
4:30	15.65	2.72	35	1.65	57.7		

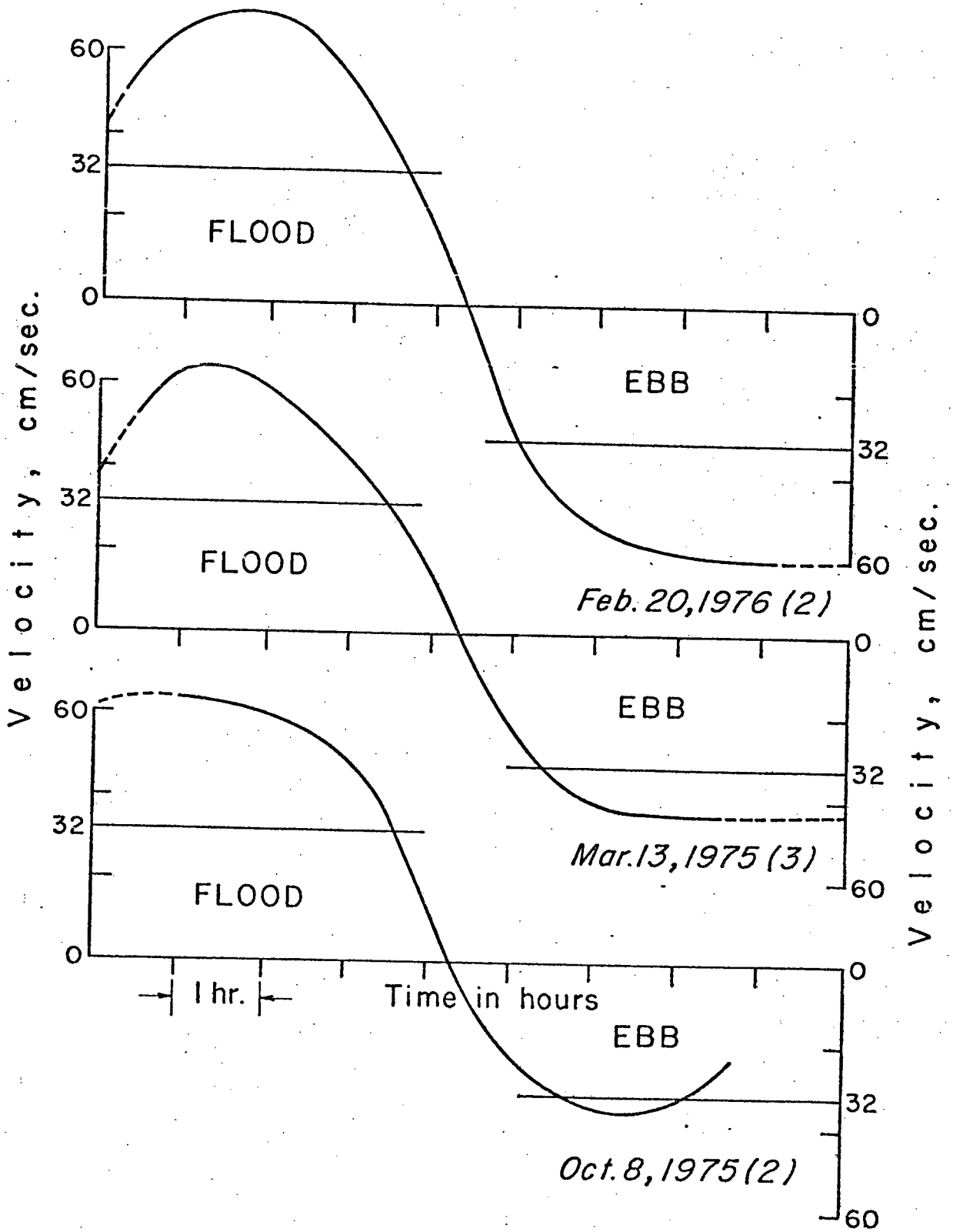


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Due to the nonlinear relationship between mean velocity and shear stress, their product stream power ( $\lambda_0 \bar{V}$ ) follows an intermediate trend. Stream power is considered a better indication of the ability of the flow to move sediment than either of the factors individually (Simons et al., 1965; Bagnold, 1963). Note in Table IX (for Aug. 11, 1975 data) that stream power values for flood averaged (time-weighted)  $88.7 \text{ dynes}-(\text{cm}/\text{sec})^2$  while ebb averaged  $76.8 \text{ dynes}-(\text{cm}/\text{sec})^2$  indicating a flood dominance.

Using the logarithmic velocity law it was determined that a mean velocity (.4d) of at least 32 cm/sec (i.e.  $dV/d\log d=10$ ) was needed to create the  $V_* = 1.77 \text{ cm}/\text{sec}$  necessary to move the largest Pitt sediment (0.59 mm). Even though highest mean velocities occur on the flood critical velocity (32 cm/sec) is maintained for a longer period of time during the ebb (Fig. 22A,B). As all other aspects of the Pitt indicate a flood-dominated system, it is concluded that the difference in peak flow velocities rather than actual time above critical velocity is the more important factor in determining direction of net sediment transport. It is suspected that the contrast between peak velocities occurring on flood and ebb would be even more accentuated during winter months (Dec. - Mar.). The highest values of  $V_*$  determined in this study, over 6.0 cm/sec, were recorded on March 13, 1975 and February 20, 1976. No  $V_*$

FIGURE 22. Comparison of time duration of flood and ebb currents above the predicted critical velocity (32 cm/sec) for Pitt River.



over 3.0 cm/sec was determined from freshet profiles and most were less than the needed critical friction velocity of 1.77 cm/sec. Figure 16 shows a decrease in maximum velocities from confluence to lake. Since magnitude of shear stress varies with mean velocity it is interpreted that shear stress or sediment entrainment potential would also decrease. This contention is supported by the decrease in mean grain size of channel bottom material from the Fraser to Pitt Lake.

On the basis of <sup>137</sup>Cs dating of sediment cores from Pitt Lake (Ashley, 1977) it has been estimated that  $150 \pm 20 \times 10^3$  tonnes of sediment (1% of Fraser's total load) are accumulating annually in the lower half of the lake. Grain size analysis of this sediment reveals that approximately 50% of this material (75,000 tonnes per year) is greater than 0.31 mm (5  $\phi$ ) and thus probably moves as bed load (Einstein et al., 1950). An attempt was made to calculate bedload transport in Pitt River using the following simple form of Einstein's (1950) analytical equation:

$$\phi = f(\psi), \quad \psi = \frac{\rho_s - \rho}{\rho} \frac{d}{S_w R_n}, \quad \phi = \frac{g_s}{r_s} \frac{\rho}{\rho_s - \rho} - \frac{1}{gD^3} \quad (5)$$

The more complex form of this equation is based on the probability of grains moving under given hydraulic conditions and has been substantiated reasonably well by laboratory and field studies (Toffaletti, 1969; Kachel and Sternberg,

1971; Garg et. al., 1971; Einstein and Abdel-Aal, 1972).

Calculations were done at three cross sections along river (confluence, mid-river, and near lake outlet). The calculations were intended only as an approximation of bedload movement and the results are probably correct to within an order of magnitude of the actual values. A representative grain size ( $D_{65}$  bed material) was used and no correction was made for form resistance.

Calculations for the tidal Pitt River also necessitate comparing transport rates upriver under flood and downstream under ebb. At any cross section, the only parameter varying between ebb and flood is water slope. Since slope varies both with time and distance, seasonally and during both flood and ebb, a maximum value was determined for various seasons and flow directions (Fig. 9). A maximum value is consistent and serves as the means of objective comparison of the varied sets of conditions. In addition maximum transport would be expected to occur near times of maximum slope. Resulting calculations (Appendix) show a net flood-oriented transport with volumes of the order of magnitude (75,000 tonnes) predicted from accumulating lake sediments.

In conclusion, bedload estimations tend to support the velocity data; i.e., that flood flows have a greater transport capacity. However more field data, in particular direct bedload measurements, are needed to substantiate this unequivocally.

Even though the system appears to be flood dominated, ebb flow can still entrain and move sediment in the opposite direction. But because of the out-of-phase relationship between stage and velocity of flow (Fig. 13) and the fact that a lower velocity is required to transport a grain than entrain it, movement in the flood direction is favored. Figure 23 incorporates the hydraulic and sediment entrainment findings of this study into a model for net upriver movement.

Critical shear stress (i.e., mean velocity of 32 cm/sec) is reached early in a flood cycle because of velocity curve asymmetry and its temporal relationship with stage changes.  $\bar{V}$  increases rapidly and declines slowly until high water is reached. In contrast, on the ebb,  $\bar{V}$  increases slowly until it reaches a peak late in the cycle, and then decreases quickly to low water. Once a grain is entrained it can be carried along by a current lower than the critical velocity. Because critical velocity occurs early in flood and late in ebb there is more time following critical flow in flood than in ebb. Thus the likelihood of additional transport under flood flow is increased. Although the proportion of total flood time that is above critical velocity appears to be less than the proportion of ebb time, higher velocities are reached during the flood. Grains move farther during a given time period on flood than they do in the

opposite direction on the ebb. The result of the oscillating sediment movement results in a net upriver movement (after Postma, 1967).

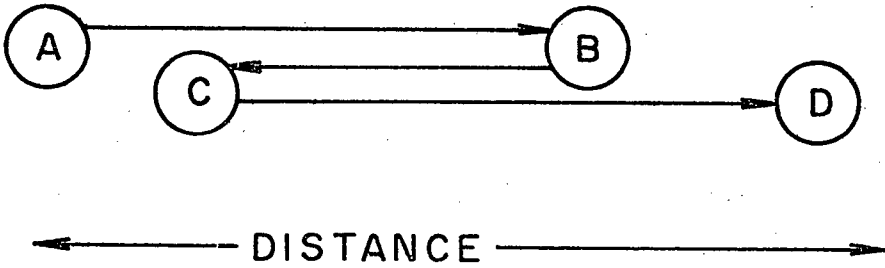
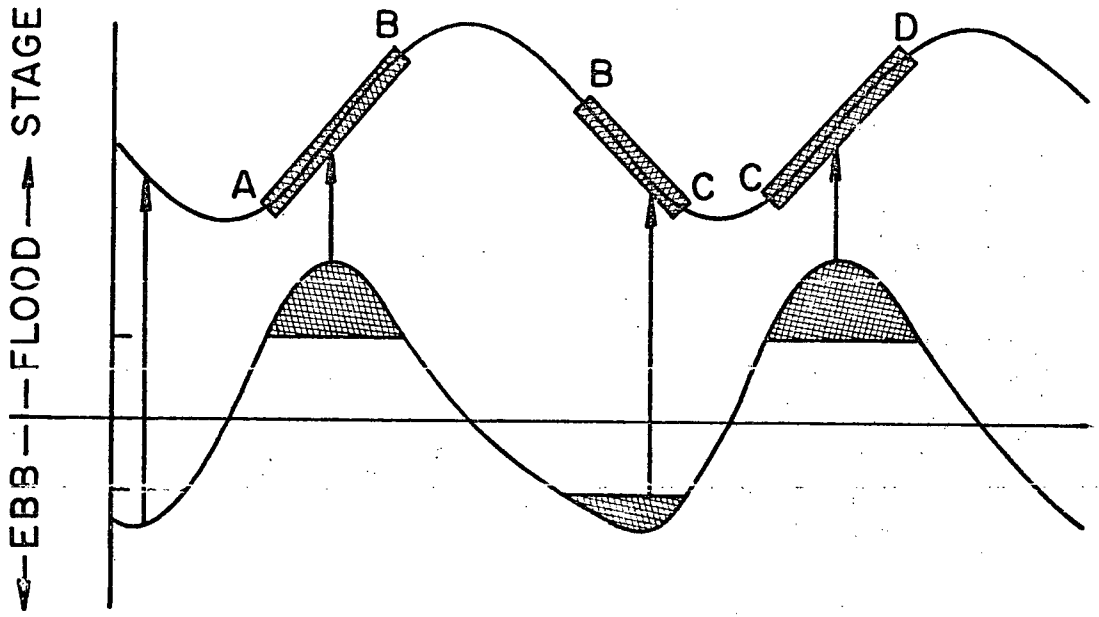
### Suspended Sediment

The suspended sediment content of Fraser River water fluctuates seasonally and ranges from an average of 62 mg/l during winter (lows are 1 mg/l) to a mean over 320 mg/l during freshet (Johnston, 1922). Water Survey of Canada for 1967-1969 at Port Mann Bridge found annual means 93, 105 and 73 mg/l respectively, ranging from a winter low of 18 mg/l to freshet high of 286 mg/l. Milliman (1977) measured a yearly mean of 135 mg/l at Port Mann Bridge 4 km seaward of Pitt River. Near bottom variations from 10 to 1500 mg/l occurred and Milliman observed that this fluctuation is due to an increase in sand content associated with increase in discharge and variations in tidal flow and that the silt and clay content remains essentially constant year round. By comparison, Pitt River water has very low suspended sediment (5 mg/l) as it drains only Pitt Lake and a few sluggish streams.

When part of the Fraser River is diverted into the Pitt system during flood tides the turbid waters first appear to move as a coherent body with a sharp line dividing muddy Fraser from relatively clear Pitt water.



FIGURE 23. Model for movement of sediment up Pitt River  
(after Postma, 1959).



Within half an hour mixing becomes obvious in the surface water and the contact becomes progressively more diffuse with time. The progression of the Fraser plume can be followed up the Pitt River visually by observing surface water or by repeated suspended sediment sampling. Table X tabulates results of surface and near bottom sediment sampling (at 2 km spacing) during a 4-hour period. Suspended sediment moved at 1.6 km/hr or 44 cm/sec or approximately the average velocity of the flow itself. However, since the river is 20.7 km long it would take over 12 hours for Fraser River water to reach the lake. Flood flows are seldom longer than 8 hours; thus, suspended sediment probably never reaches the lake on one tidal cycle, but would move in small increments over several tidal cycles. Areas of low velocity near log storage booms which line the river banks and mid-channel islands might provide a settling site for some of the suspended load, but it is suspected that the bulk of it returns to the Fraser on the ebb flow. Taking the yearly mean of 100 mg/l, 22,000 tonnes of suspended sediment enters Pitt River on the flood. However, less than 0.5% of this is required to remain in Pitt River after each flood and eventually reach the lake to account for the estimated 75,000 tonnes of suspended material (<0.31 mm) accumulating yearly in the lake.

TABLE X Pitt River suspended sediment measurements.  
Stations (1) - (5) at 2-km intervals.

TIME	FRASER RIVER	PITT RIVER				
	(1)	(2)	(3)	(4)	(5)	(6)
0-.75 HR	31.06	15.29	8.29	7.94	9.64	
	36.25	15.23	13.98	13.21		
1.25- 2.0 HR		32.85	33.82	17.54	12.90	
		38.59	31.23	14.13		
3.25- 3.75 HR		24.87	24.70	27.25	8.76	3.86
		29.27	36.93	34.98		
INTERFACE ADVANCES 1.6 KM/HR (44 CM/SEC)						

## BED CONFIGURATIONS

Observations

All observations of the configuration of the channel bottom were made remotely by depth sounders and a side-scan sonar. The precision of the depth sounding records is within 30 cm (vertical) and approximately 15 m (horizontal). The records have a vertical exaggeration of between 1:10 and 1:15. Side-scan sonar records can be read to within 1 m vertically and 15 m horizontally. Vertical exaggeration of side-scan records is 1:3. A distortion of the true bedform shape occurs on some depth sounding records due to orientation of slopes of varying steepness relative to direction of boat motion. However, as only the gross form (length and height) and proportion of length of stoss and lee sides of the bedforms were being examined from the depth soundings the distortion was not considered important.

The depth sounding program was initiated as part of the investigation of bedload transport. Repeated soundings were taken along all reaches of the river, concentrating in the thalweg. Most runs were carried out between the months of May and September with a lesser number in the winter to detect seasonal changes. Because a bewildering variety of bedform shapes and sizes was revealed during the 18-month survey, the side-scan sonar was used for a two-day

period (June 1,2, 1975) to aid in the interpretation of the forms by determining their 3-dimensional geometry.

The large range of sizes and shapes of bedforms found in the channel presented a problem of bedform terminology. The classification of large-scale alluvial bedforms is in a state of confusion reflecting a general lack of understanding of their genesis. The most recent review of bedform terminology (Task Force, 1966) is based on an attempt to extrapolate bedform-hydraulic relationships developed in flume studies such as that of Simons et al., (1965) to the natural environment. Unfortunately, the range of conditions found in rivers is not easily reproduced in flumes. In addition, the large-scale, low-amplitude bedforms found in shallow marine, estuarine, and riverine environments have no equivalent forms in the flume results of Simons et al., (1965). These large bedforms have been termed giant ripples, sand ridges, dunes, sand waves, super ripples, transverse bars, sand dunes, and large scale ripples by various authors. Clearly, for the present, a viable bedform classification should be independent of genetic assumptions and based only on descriptive morphology.

A detailed study of the 3-dimensional geometry of bedforms in Pitt channel was made from the sounding records. Using plan geometry, form height and spacing, and form orientation with respect to flood or ebb flow direction, a

classification of bedform shapes found in Pitt River was developed (Figure 24). On the basis of height/spacing proportions two major groups of forms can be discerned: small forms (spacing 5 m, ht/spacing ratio = 1/10) equivalent to "dunes" of Simons et al., (1965), and large forms (spacing 10 - 60 m, ht/spacing ratio = 1/20) equivalent to "sand waves" of Harms et al. (1975). Spacings in the large forms do not represent a continuum but occur in discrete groups (10 - 15 m, 25 - 30m, 50 - 60m) with few bedforms of 15 - 25 m and 30 - 50 m observed. The dominant form is 25 - 30 m in length, composing 70% of the total. The smaller forms (10 - 15 m) make up 25% and the large forms (50 - 60 m) about 5%.

Dunes (height/spacing = 0.3m/2 - 3m) are 3-dimensional with sinuous crests and are found on the backs of the large 2-dimensional straight-crested sandwaves. Sandwaves occur in two basic shapes. Type one, characterized by a rounded stoss side (usually covered with dunes) and fairly steep lee slope (Fig. 24A,C) occurs in trains at only a few sites (E and F of Fig. 3A). This form referred to as a "hump-back" sand wave (Fig. 25D, flood forms; Fig. 25F, ebb forms) is identical to ones found in Fraser River (Fig. 24B; Fig. 25A) developed under unidirectional flow. The second type (Fig. 24D-H) has uniformly sloping stoss and lee sides. However, the angle of slope and proportion of length of sides varies continuously from flood-oriented forms (60%

of total) through ebb-modified flood forms and fairly symmetrical shapes (25%) of ebb-oriented types (15%).

Bedforms occur along the entire sandy thalweg from Fraser River (Fig. 25A) to the lake outlet (Fig. 25G). The thalweg is approximately 100 - 150 m wide and bedforms usually cover the entire area. Sand wave crests are perpendicular to the orientation of the thalweg and the superimposed dunes have crests parallel to the sand wave crests. Dunes also occur in sandy channel areas off the thalweg and on sandy shoals surrounding the islands. In contrast, side-scan records and visual observation indicate that ripples are typical of finer grained (silty) areas.

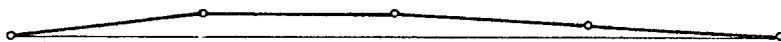
A general relationship between both bedform size and type and topography was found in the Pitt River. The largest forms are found at the base of ramps (areas of rapid shoaling, with slopes  $\leq 1^\circ$ ) and the smallest forms are found on relatively flat topography. For example, sand waves (4.5 m/60m) occur on the ramp at the constricted area near a bedrock outcrop at km 15 (Fig. 3A). The channel shallows from 21 m toward the shoal to 10 m at the north end of the wave train. The reach north of Addington Point (Fig. 2) is deep (24 m) but relatively flat. Sand waves here are 1 m/30 m), identical with the average size found in other parts of the river at only 5 m depth. Several trains of small sandwaves (.8 m/10-15m) occur on flat shoals



FIGURE 24. Bedform shapes found in Pitt River drawn to true scale.

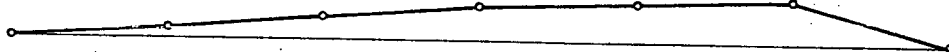
FLOOD →

A



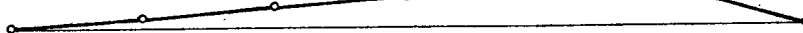
EBB HUMPBACK

B



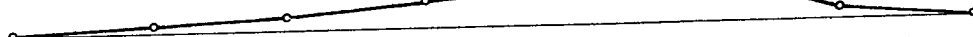
EBB HUMPBACK  
(Fraser River)

C



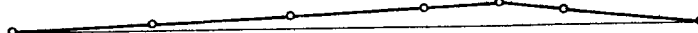
FLOOD HUMPBACK

D



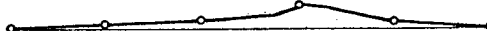
LARGE FLOOD

E



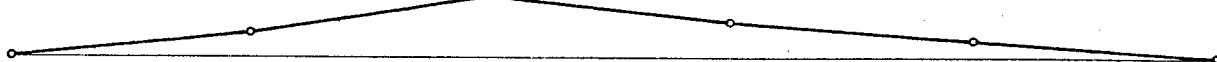
SMALL FLOOD

F



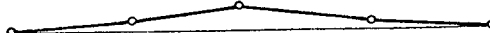
EBB MODIFIED FLOOD

G



LARGE SYMMETRIC

H



SMALL SYMMETRIC

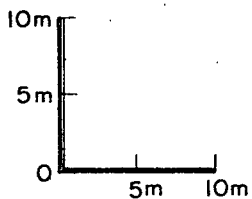
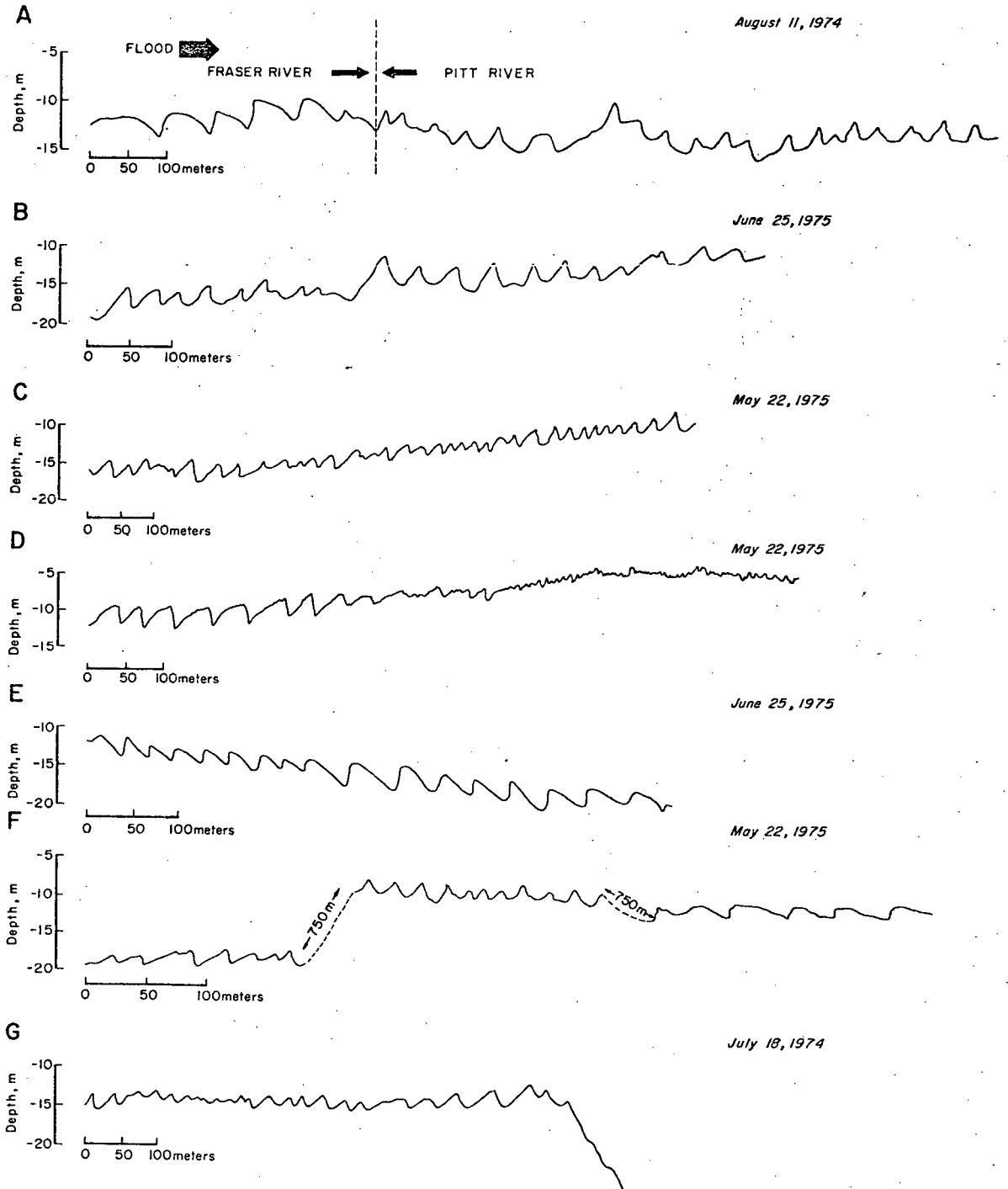


FIGURE 25. Depth sounding profiles:

- (A) Fraser-Pitt confluence; Fraser has ebb forms, Pitt floodforms.
- (B) Flood-oriented sandwaves with some ebb modified crests (km 3).
- (C) Flood-oriented small scale sandwaves (10 - 15 m spacing) (km 8).
- (D) Flood "humpback" forms and dunes on flat topography (km 9).
- (E) Ebb "humpback" forms south of Point Addington (E on Fig. 3A).
- (F) Flood-oriented, symmetric and ebb-modified, and ebb-oriented sand waves that occur on large mounds in channel.
- (G) Bedforms at Pitt Lake outlet.



surrounding the islands.

In most reaches large longitudinal "mounds" occur with a wavelength of 3 km (one half the meander wavelength,  $\lambda_M$ ) and are thus presumably related to the meander sequence. Elevation difference from crest to trough of the mounds is 7 - 8 m. These major channel features are located on inside bends of midchannel islands or at riffles and present a ramp of shallowing channel to both flood and ebb oriented currents. Flood-oriented sand waves are found on the downstream side of these ramps, symmetrical forms on the shallow top, and ebb-oriented forms on the upstream side (Fig. 25F).

Repeated soundings over a period of months indicated a reorganization of different scales of sand waves. For example, it appeared that several (10 - 15m) forms merged to create a 30 m or 60 m bedform or, inversely, a large form would be replaced by smaller ones. Similar jumps in scale of bedforms have been noted in other rivers by Pretious and Blench (1951) in Fraser River, Znamenskaya (1963) in Polometi River (U.S.S.R.) and Neill (1969) in Red Deer River (Alberta, Canada). The nature of the transformation is not clear; however, intermediate size forms are transient if they exist at all. Although the exact flow conditions which might have caused "regrouping" in the Pitt could not be determined, the changes occurred mainly within the flood-oriented forms during winter flows and on the downstream side of the "mounds" (2 km, 6 km and

and 12 km: Fig. 3).

Repeated depth soundings over a tidal cycle provided evidence of bedform modification. Flood-oriented forms developed ebb-modified crests (Fig. 24F; Fig. 25F) during strong ebb flows (mean velocity of 50 - 60 cm/sec). A complete change from flood-oriented to ebb-oriented form or from ebb-to-flood was not observed..

## Interpretation

### Bedform Scaling

Because Pitt River has bidirectional flow, the state of equilibrium of the bedforms becomes an important factor. Unidirectional rivers commonly experience an annual high discharge event (spring flood) lasting several days or weeks. Bedforms have been observed to have a delayed response to the increasing or decreasing discharge, and this delay has been termed "lag". In tidal flows the discharge fluctuations have a time scale of hours, apparently insufficient for one event to have a significant effect on large bedforms (Ludwick, 1974). Thus a lag phenomenon would be difficult to measure in the tidal environment. In the Pitt, geometry of each bedform represents the summation of the modifications of both flow directions. Since soundings over an 18-month period determined that the majority of bedform types (Fig. 24) remained constant throughout the year, the forms are

interpreted to be in quasi-equilibrium with the bidirectional flow. Thus, bedform shape maintains the imprint of the dominant flow conditions at that site. The humpback forms (Fig. 24A,C) are found in fairly protected areas of the channel. As they appear to be affected by only one current direction humpback forms are considered to be an equilibrium form. In general, the size and shape of the sand waves appears to be related to channel geometry and not to depth as was suggested by Allen (1968); Yalin (1974), and Jackson (1976B). Coleman (1969, Brahmaputra River) and Whetten and Fullam (1967, Columbia River) both found no correlation between scale of bedforms and depth, in agreement with the data from the Pitt.

Bed configurations in the Pitt are difficult to interpret because of the multiplicity of forms and the fact that they appear to reflect the average hydraulic conditions. Most research on sand waves has been done in shallow marine and estuarine environments. Characteristics of flow in these infinitely wide areas are distinctly different from those in channelized flow where lateral-boundary conditions are important. Although the Pitt River is tidal, it is clearly similar to unidirectional rivers in both channel morphology and bed configuration. Significantly, analysis reveals systematic relationships between the various bedform groups and channel parameters.

Plotting the average height and spacing of sand waves on a logarithmic scale results in a linear relationship. As these sand waves form at least 3 distinct groups, this linear relationship appears significant and suggests a common mode of genesis. A similar plot of estuarine sand-waves (Boothroyd and Hubbard, 1975; Fig. 3) shows a scatter of values but does suggest a distinction between subtidal, or deeper water forms, and intertidal, or more shallow water forms. The Pitt values fall within the field of the deep water sand waves on Boothroyd and Hubbard's plot. Dunes from the Pitt plot in the middle of the megaripple field on the same diagram and are assumed to be the same form.

Theoretical models for the genesis of dunes and sand-waves are in a state of flux. Dune formation is thought by some to be related to large scale turbulence (Velikonov and Mikhailova, 1950; Znamenskaya, 1963). The regular spacing of dunes appears to be a direct function of the scale of the largest turbulent eddies (Znamenskaya, 1963; Grishanin, 1972; Jackson, 1975). Flow separation and associated slipface development provide alternating areas of erosion and deposition critical to sediment entrainment and transport. A detailed model of dune genesis has been presented by Costello (1974).

Although considerable progress has been made in understanding the mechanics of dune formation, none of the theo-



retical models proposed (Kennedy, 1969; Smith, 1970) predict the existence of sand waves.

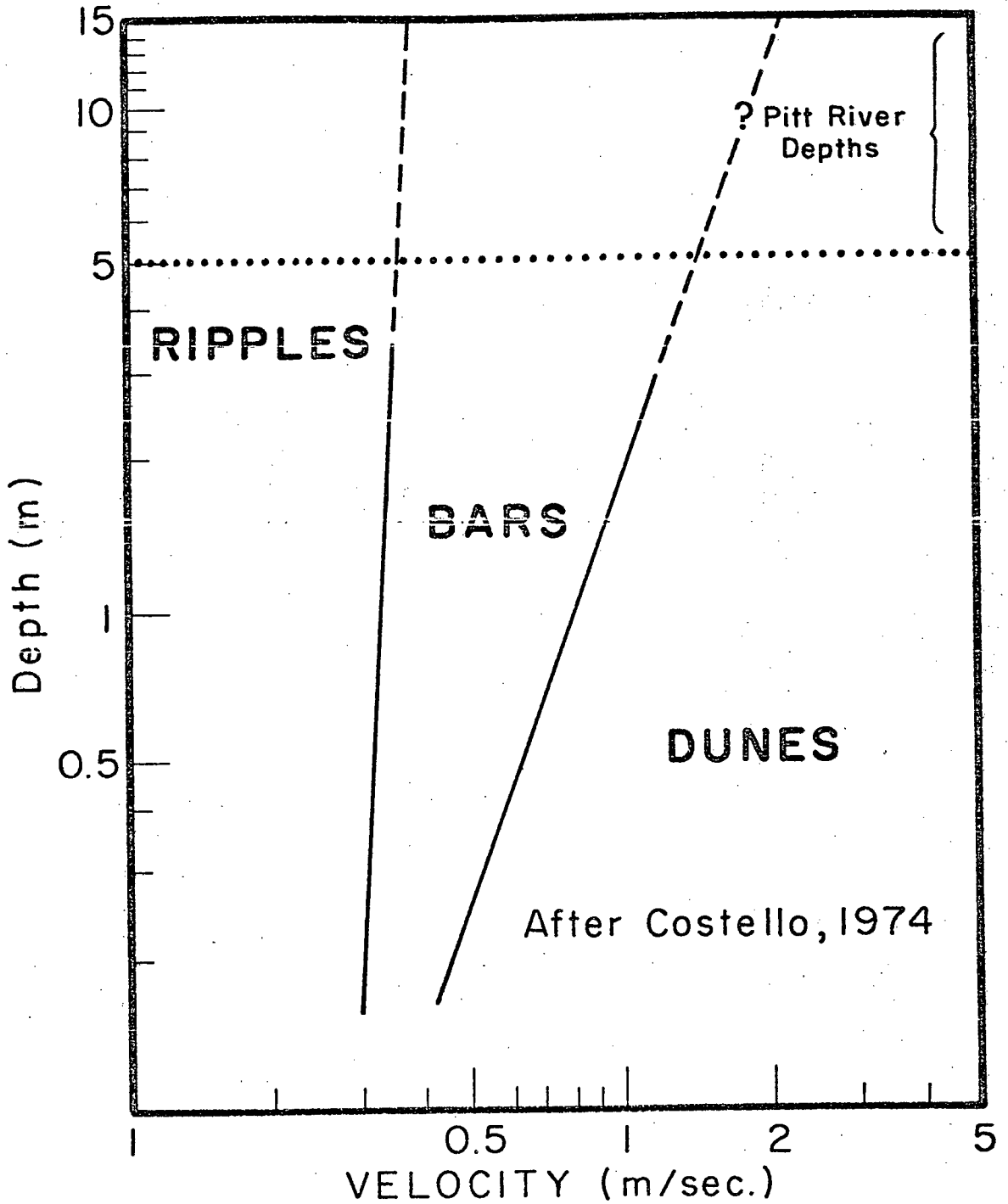
Recent flume studies (Pratt and Smith, 1972; Pratt, 1973; Costello, 1974) reveal bedforms intermediate between ripples and dunes. The flume bedforms were called "intermediate flattened dunes" by Pratt and "bars" by Costello, who equates them with sand waves. Costello adapted kinematic wave theory to explain the genesis of these forms. Although shallow water ( $\leq 3\text{m}$ ) transverse bars (Smith, 1971; Jackson, 1976A) may be adequately explained by "shock wave" aggradation of sediment, several characteristics of deep water sand waves in river channels are not consistent with Costello's model. For example, the regular geometry and spacing of sand wave trains in Pitt and other rivers (Pretious and Blench, 1951; Whetten and Fullam, 1969; Carey and Keller, 1957) conflict with Costello's conclusion that sand waves "are randomly generated and (that) this randomness carries over into their spacing and height". The occurrence of dunes in apparent equilibrium with sand waves at velocities considerably lower than predicted by Costello's depth-velocity diagram (Fig. 26) has been documented in a number of studies (Pretious and Blench, 1951; Coleman, 1969; Neill, 1969; Singh and Kumar, 1974; and many others). Jackson (1976A) has presented evidence that dunes and sand waves not only occur together but also migrate under essentially steady flow conditions.

It is unfortunate that these large-scale forms, characteristic of sandy rivers, estuaries, and marine shoals, are so poorly understood.

#### Relationship of meander wavelength to bedform spacing

Synthesis of quantitative data for rivers by Leopold and Wolman (1957) revealed a systematic relation between various parameters of channel geometry and bankful discharge or effective channel-forming discharge,  $Q_e$ . They demonstrated that meander wavelength ( $\lambda_M$ ) or resistance to flow is proportional to  $Q_e$  according to the relation  $\lambda_M \propto Q_e^{.5}$ ; however, the log-log plot of  $\lambda_M$  vs.  $Q_e$  shows considerable scatter. This scatter is not surprising as bed roughness and sediment transport, also important aspects of resistance, are not included. Leopold et al. (1964) suggested that channel geometry is controlled by continuous dissipation of energy by the river along its course. In addition, they showed that total resistance (the Manning  $n$  coefficient) is also a simple function of  $Q$  ( $n = aQ^b$ ). Since form resistance is an important part of total resistance, it is reasonable to expect channel configuration (bed roughness) as well as  $\lambda_M$  to be scaled to flow. Bedform spacing,  $\lambda_B$ , is known to increase with increasing  $Q_e$  (usually with some time lag) through flood events (Pretious and Blench, 1951; Carey and Keller, 1957; Allen, 1976A; 1976B). Thus, it is reasonable to expect a

FIGURE 26. Depth-velocity diagram of the three lower flow regime beforms extrapolated to depths found in Pitt River (after Costello, 1974).



particular  $\lambda_B$  in addition to  $\lambda_M$  for a given  $Q_e$ .

An attempt was made to obtain comparable data of  $Q_e$ ,  $\lambda_M$ , and  $\lambda_B$  from sandy meandering rivers with the criteria that are outlined in Table XI. Data are meager, as few studies have been concerned with both channel form and bed roughness. However, the most serious problem is the difficulty in ascertaining the bedform wavelength in equilibrium with bankful discharge. Compilation of available data from sandy rivers including the Pitt, reveal that neither  $\lambda_M$  or  $\lambda_B$  by itself is directly scaled (on arithmetic plot using English units) to  $Q_e$ , but the ratio  $\lambda_M:\lambda_B$  is (Fig. 27); thus, the two factors seem to be inter-related in their response to flow. There appears to be a correlation between the scale of energy input,  $Q_e$ , and the scale of energy-dissipating mechanisms ( $\lambda_M, \lambda_B$ ). Based on the preliminary findings shown in Figure 27 the following relationship for sandy meandering rivers is suggested:  $\lambda_M/\lambda_B \propto Q_e^{.5}$ . It is important to emphasize that this tentative relationship refers to the effective or channel-forming discharge, i.e., that discharge related to  $\lambda_M$  and the dominant bedform size in apparent equilibrium with that discharge, accounting for lag effects when necessary.

The apparent interrelationship between  $\lambda_M$  and  $\lambda_B$  in response to flow which certainly requires further examination is shown in the following comparison: Congaree

TABLE XI Criteria of parameters used in bedform-meander scaling.

PARAMETERS	CRITERIA
$Q_e$	Effective discharge (channel-forming discharge or bankful discharge) not maximum or mean annual discharge. That flow which determines the $\lambda_M$ .
$\lambda_M$	Meander wave length (twice distance between pools; in particular the "hydraulic" meander, which may not necessarily be the same as the river meander.
$\lambda_B$	Bedform wavelength, average or dominant size; that appears to be in equilibrium with $Q_e$ . Not the largest wavelength or range of lengths present. $\lambda_B > 5m$ , usually $> 10m$ . Large-scale bedforms are commonly referred to as sand waves, transverse bars, large dunes, or super ripples.

FIGURE 27. Plot of "resistance factors  $\lambda_M$  and  $\lambda_B$  against flow factor  $Q_e$  shows a systematic relationship in sandy rivers. This suggests that bedform spacing can be determined knowing bankfull discharge and meander wavelength.

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River, South Carolina (Levey, 1975) which has approximately the same discharge as Red Deer River (Neill, 1969) has sand waves which are twice as large. Significantly, the meander spacing is also doubled. Additional data would be necessary to firmly establish the empirical relation shown in Figure 27. However, the implication is that meander wavelength is not directly scaled to discharge, in agreement with Schumm's (1971) observation that  $\lambda_M$  can vary tenfold at constant  $Q_e$ . Although the underlying reasons for the variations in scale of meanders and sand wave length are unclear, it is interesting to note that the Congaree has coarser bed material (mean grain size, 0.59 mm) and higher sinuosity ( $s = 1.75$ ) than the Red Deer River (mean grain size, .37 mm;  $s = 1.11$ ). Thus, grain size may be a key factor in predicting the meander wavelength and bedform spacing for a given bankful discharge.

In conclusion, there appear to be several scales of sediment-flow interaction, all a function of energy dissipation. On a local level, small-scale turbulence (on the order of a few cm) and grains interact, resulting in sediment entrainment and transportation. Large-scale turbulence (on the order of meters), apparently related to scale of flow, interacts with the bed, molding it into a variety of configurations. Finally, interaction occurs on a regional scale (on the order of kilometers) where

size of major channel features such as meanders, point bars, riffles, and mid-channel bars are determined by scale of flow. Data from Pitt River clearly show a regular channel pattern with alternating pools, riffles, and islands. The fairly regular spacing of sand waves (70% with length of 25 - 30 m), and the inferred common genesis of the three discrete sand wave sizes imply a governing hydraulic control. Discharge (flow) and not depth, width, or velocity alone appears to be the controlling mechanism.

## SUMMARY AND CONCLUSIONS

Despite the tidal influence of Pitt River, it has few estuarine characteristics. This is related to its connection to Pitt Lake, which acts as a large reservoir, thus allowing bidirectional flow through Pitt River to occur with no more impedance than that of a normal river. The mineralogy of the channel sands is essentially identical to Fraser River mineralogy confirming the Fraser as provenance of Pitt River sediments. The river is a flood dominated system; although flow duration is shorter, flood flows have slightly higher peak velocities than the ebb. Thus, flood flow has higher basal shear stress, greater flow power and associated higher sediment entrainment potential. Water slopes are steeper on flooding tide during both winter and freshet. The steeper water slope provides the major driving force to move sediment (in flood direction) toward Pitt Lake even though the net discharge of water is in the opposite direction. Reflecting this direction of transport, mean grain size of bed material decreases from 0.37 mm at the Fraser-Pitt confluence to 0.25 mm at the entrance to Pitt Lake. <sup>137</sup>Cs dating of lake sediment indicates a total of  $150 \pm 20 \times 10^3$  tonnes is accumulating annually in the delta at the lower end of the lake.

The thalweg bed is covered with large-scale, low-amplitude, and straight-crested bedforms herein termed

sand waves. 60% are flood oriented, 25% symmetric or ebb-modified flood forms, and 15% are ebb oriented. The majority have smaller bedforms (dunes) on their stoss sides. Three distinct sizes (height/spacing = 0.8 m/10 - 15 m; 1.5 m/25 - 30 m; 3 m/50 - 60 m) of sand waves were found in the river and the linear relationship between log height and log spacing suggests a common genesis. The position of the various sand wave types and sizes appears to be related to channel geometry and not depth of flow. The largest forms, as well as the flood-oriented forms, occur on the downstream side of ramps (slope of  $\leq 1^\circ$ ) and the smallest sand waves on relatively flat topography.

The interaction of flow and channel alluvium occurs on at least three distinct scales, all related to energy dissipation by the moving fluid. First, grains and small-scale turbulence (on the order of centimeters) interact resulting in sediment entrainment and transport. The second level of interaction of flow with sediment produces a variety of configurations of bed roughness (ripples, dunes, and sand waves) on the scale of meters. Third, interaction on a regional scale (order of kilometers) creates the channel configuration of evenly spaced pools, riffles and bars. The larger two scales of sediment-water interaction appear to be proportional to channel forming discharge,  $Q_e$  (peak winter flood tide flows).

In conclusion, Pitt River is in a state of quasi-equilibrium with bidirectional and seasonal changes in discharge. The channel has not migrated significantly in the past several thousand years. The configuration of the channel bottom and magnitude of sediment flux appears to be consistent from one year to the next. Both these observations indicate relative stability and a balance of hydraulic and frictional forces in this unusual depositional system.

## REFERENCES CITED

- Allen, J.R.L., 1976A, Computational models for dune time-lag: General ideas, difficulties, and early results: *Sed. Geology*, v. 15, no. 1, p. 1-53.
- \_\_\_\_\_, 1976B, Time lag of dunes in unsteady flow: an analysis of Nasners data from R. Wesen Germany: *Sed. Geology*, v. 15, no. 6, p. 309-316
- \_\_\_\_\_, 1968, The nature and origin of bedform hierarchies: *Sedimentology*, v. 10, p. 161-182.
- Annambhotla, V.S.S., Sayre, W.W., and Livesey, R.H., 1972, Statistical properties of Missouri River bedforms: *Proc. Am. Soc. Civil Engineers, Waterways, Harbors, and Coastal Engineering Div.*, p. 489-510.
- Ashley, G.M., 1977, Sedimentation on a tidal lake delta, Pitt Lake, British Columbia: Part II (unpublished PhD thesis), Univ. of British Columbia, Vancouver, B.C.
- Ages, A. and Woolard, A., 1976, The tides in the Fraser Estuary: *Pacific Marine Science Rept. 76-5: Inst. Ocean Sci. Patricia Bay, Victoria, B.C.*
- Bagnold, R.A., 1963, *Mechanics of marine sedimentation* in Hill, M.N. (ed.), *The Sea: New York, John Wiley & Sons, Inc.*, v. 3, p. 507-528.
- Boggs, S. Jr., and Jones, C.A., 1976, Seasonal reversal of flood-tide dominant sediment transport in a small Oregon estuary: *Geol. Soc. America Bull.*, v. 87, p. 419-426.
- Boothroyd, J.C., and Hubbard, D.K., 1975, Genesis of bedforms in mesotidal estuaries: in Cronin, L.E. (ed.), *Estuarine Research: Academic Press, N.Y.*, v. 2, p. 217-235.
- Bowditch, N., 1962, *American Practical Navigator*, Hydrograph Office, pub. no. 9, U.S. Gov. Printing Office, Washington, D.C.
- Briggs, L.I., and Middleton, G.V., 1965, Hydromechanical principles of sediment structure formation: *S.E.P.M., Spec. Pub. 12*, p. 5-16.

- Carey, W.C., and Keller, M.D., 1957, Systematic changes in the beds of alluvial rivers: Proc. Am. Soc. Civil Engineers, J. Hydraulics Div., v. 83, Proc. Paper 1331, 24 p.
- Charnock, H., 1959, Tidal friction from currents near the sea bed: Geophys. Jour. Roy. Astron. Soc., v. 2, p. 215-221.
- Coleman, J.M., 1969, Brahmaputra River; channel processes and sedimentation: Sed. Geology, v. 3, p. 129-239.
- Costello, W.R., 1974, Development of bed configurations in coarse sands: p. 120, Rept. 74-1, Earth and Planetary Sciences Dept., M.I.T., Cambridge, Mass.
- Department of Public Works, Vancouver, British Columbia, (unpublished core data; bathymetric charts of Pitt system).
- Dyck, W., Fyles, J.G., and Blake, W. Jr., 1965, G.S.C. Radiocarbon Dates IV: Radiocarbon, v. 7, p. 24-46.
- Dyer, K.R., 1970, Current velocity profiles in a tidal channel: Geophys. Jour. Roy. Astron. Soc., v. 22, p. 153-161.
- Einstein, H.A., 1950, The bed-load function for sediment transportation in open channel flow: U.S. Dept. of Agriculture Tech. Bull., no. 1026.
- \_\_\_\_\_, and Abdel-Aal, F.M., 1972, Einstein bed-load function at high sedimentation rates, Am. Soc. Civil Engineers Proc. (HY1), p. 137-151.
- \_\_\_\_\_, and Barbarossa, N.L., 1952, River channel roughness: Am. Soc. Civil Engineers Trans., v. 117, p. 1121-1146.
- Fisk, H.N., 1951, Mississippi River valley geology, relation to river regime: Am. Soc. Civil Engineers Proc., v. 77, no. 80, 16 p.
- Folk, R.L., 1968, Petrology of Sedimentary Rocks: Univ. of Texas, Hemphills, Austin, Texas.

- Garg, S.P., Agrawal, A.K., and Singh, P.R., 1971, Bedload transportation in alluvial channels: Am. Soc. Civil Engineers Proc. (HY5), p. 653-664.
- Garrison, R.E., Luternauer, J.L., Grill, E.V., Macdonald, R.D., and Murray, J.W., 1969, Early diagenetic cementation of recent sands, Fraser River Delta, B.C.: Sedimentology, v. 12, p. 27-46.
- Geological Survey of Canada, Vancouver, British Columbia; (unpublished water well records).
- Gordon, C.M., 1975, Sediment entrainment and suspension in a turbulent tidal flow: Marine Geology, v. 18, p. 57 - p. 64.
- Grishanin, K.V., 1972, Stability of river channels and kinematic waves: Trans. State Hydrol. Inst., no. 190, p. 37-47.
- Harms, J.C., Southard, J.B., Spearing, D.R., and Walker, R.G., 1975, Depositional environments as interpreted from primary sedimentary structures and stratification sequences: S.E.P.M. Short Course No. 2, Tulsa, Oklahoma.
- Ippen, A.T., and Harleman, D.R.F., 1966, Tidal dynamics in estuaries, in Ippen, A.T. (ed.), Estuary and Coastline Hydrodynamics: New York, McGraw-Hill, p. 493-545.
- Jackson, R.G., 1975, Velocity-bedform-texture pattern of meander bends in the lower Wabash River of Illinois and Indiana: Geol. Soc. America Bull, v. 86, no. 11, p. 1511-1522.
- \_\_\_\_\_, 1976A, Large scale ripples of the lower Wabash River: Sedimentology, v. 23, p. 593-623.
- \_\_\_\_\_, 1976B, Sedimentological and fluid-dynamic implications of the turbulent bursting phenomenon in geophysical flows: J. Fluid Mech., v. 77, p. 531-560.
- Johnston, W.A., 1922, The character of the stratification of the sediments in the recent delta of Fraser River, British Columbia: Jour. Geol., v. 30, p. 115-129.



- Kachel, N.B., and Sternberg, R.W., 1971, The transport of bedload as ripples during an ebb current: *Marine Geology*, v. 10, p. 229-244.
- Keller, E.A., and Melhorn, W.N., 1973, Bedforms and fluvial processes in alluvial stream channels: in Morisawa, M., (ed.), *Fluvial Geomorphology*, pub. in Geomorphology S.U.N.Y. Binghamton, Binghamton, N.Y.
- Kennedy, J.F., 1969, The formation of sediment ripples, dunes and antidunes: in *Annual Review of Fluid Mechanics*, 1969: p. 147-168.
- Klein, G. de V., 1970, Depositional and dispersal dynamics of intertidal sand bars: *Jour. Sed. Petrology*, v. 40, p. 1095-1127.
- de Leliavsky, N., 1894, Currents in streams and the formation of stream beds: Sixth Internat. Cong. on Internal Navigation, The Hague.
- Leopold, L.B., and Maddock, T. Jr., 1953, Hydraulic geometry of stream channels and some physiographic implications: U.S.G.S. Prof. Paper 252, p. 31.
- \_\_\_\_\_, and Wolman, M.G., 1957, River channel patterns; braided meandering and straight: U.S.G.S. Prof. Paper 282-B.
- \_\_\_\_\_, and \_\_\_\_\_, 1960, River Meanders: *Geol. Soc. America Bull.*, v. 71, p. 769-794.
- \_\_\_\_\_, \_\_\_\_\_, and Miller, J.P., 1964, *Fluvial processes in Geomorphology*: W.H. Freeman and Co., San Francisco, 522 p.
- Levey, R.A., 1975, Characteristics of coarse-grained point bars, upper Congaree River, South Carolina in Hayes, M., & Kana, T. (eds.), *Terrigenous Clastic Depositional Environments*: Coastal Res. Div. Univ. S.C., Columbia, S.C.
- Ludwick, J.C., 1974, Tidal currents and zig-zag sand shoals in a wide estuary entrance: *Geol. Soc. America Bull.*, v. 85, p. 717-726.

- MacKintosh, E.E., and Gardner, E.H., 1966, Mineralogical and chemical study of lower Fraser River alluvium sediments: Canadian Jour. Soil Sci., v. 46, p. 37-46.
- Matthes, G.H., 1947, Macroturbulence in natural stream flow: Am. Geophys. Union Trans., v. 28, p. 255-262.
- Mathewes, R., 1973, A palynological study of postglacial vegetation changes in the University Research Forest, southwestern British Columbia: Canadian Jour. of Botany, v. 51, no. 11, p. 2085-2103.
- Mathews, W.H., Fyles, J.G., and Nasmith, H.W., 1970, Post-glacial crustal movements in southwestern British Columbia and adjacent Washington State: Canadian Jour. of Earth Sci., v. 7, no. 2, p. 690-702.
- McCave, I.N., 1973, Some boundary-layer characteristics of tidal currents bearing sand in suspension: Mem. Soc. Roy. Sci., 6th Series, Liege, v. 6, p. 107-126.
- Meade, R.H., 1969, Landward transport of bottom sediments in estuaries of the Atlantic coastal plain: Jour. Sed. Petrology, v. 39, p. 222-234.
- Milliman, J.D., 1977, Sedimentation in the Fraser River and its estuary (manuscript in preparation).
- Morton, K.W., 1949, History of improvements, 1871-1948, Fraser River system province of British Columbia: Public Works of Canada, mimeo rept., 66 p.
- Nece, R.E., and Smith, J.D., 1970, Boundary shear stress in rivers and estuaries: Proc. Am. Soc. Civil Engineers, v. 96, W.W.2, p. 335-357.
- Neill, C.R., 1969, Bedforms in the lower Red Deer River, Alberta: Jour. Hydrol., v. 7, p. 58-85.
- Olivier, J.P., Hicken, G.K., Orr, C. Jr., 1970/71, Automatic particle size analysis in subsieve range: Pow. Technology, v. 4, p. 257-263.
- Peacock, M.A., 1935, Fiord - Land of British Columbia: Geol. Soc. America Bull., v. 46, p. 633-696.
- Peters, N., 1973, The Pleistocene geology and the geotechnical aspects of the proposed Pitt River Bridge, Port Coquitlam, B.C.: (B.A.Sc. thesis), U.B.C., Vancouver, British Columbia.

- Pharo, C.H., 1972, Sediments of the central and southern Strait of Georgia, B.C.: (Ph.D. dissertation) U.B.C., Vancouver, B.C., 290 p.
- Postma, H., 1967, Sediment transport and sedimentation in the estuarine environment: in Lauff, G.H. (ed.), Estuaries: Am. Assoc. Adv. Sci., pub. 83, p. 158-179.
- Pratt, C.J., 1973, Bagnold approach and bed-form development: Proc. Am. Soc. Civil Engineers, J. Hydraul. Div., v. 99, p. 121-137.
- Pratt, C.J., and Smith, K.V.H., 1972, Ripple and dune phases in a narrowly graded sand: Proc. Am. Soc. Civil Engineers, J. Hydraul. Div., v. 98, p. 859-874.
- Pretious, E.S., and Blench, T., 1951, Final report on special observations of bed movement in lower Fraser River at Badner Reach during 1950 freshet: N.R.C. (Canada), Vancouver, British Columbia, 12 p.
- Pritchard, D.W., 1967, Estuarine circulation patterns: Am. Soc. Civil Engineers Proc., v. 81, no. 717, 11 p.
- Schumm, S.A., 1960, The shape of alluvial channels in relation to sediment types: U.S.G.S. Prof. Paper 352 B.
- \_\_\_\_\_, 1963, Sinuosity of alluvial rivers of the Great Plains: Geol. Soc. America Bull., v. 74, p. 1089-1100.
- Simons, D.B., Richardson, E.V., and Nordin, C.F.Jr., 1965, Sedimentary structures generated by flow in alluvial channels: in Primary sedimentary structures and their hydrodynamic interpretation: Spec. Pub. 12, p. 34-52.
- Singh, I.B., and Kumav, S., 1974, Mega- and giant ripples in the Ganga, Yamuna, and Son Rivers, Uttar Pradesh, India: Sed. Geology, v. 12, p. 53-66.
- Smith, J.D., 1970, Stability of a sand bed subjected to a shear flow of low froude no.: Jour. Geophys. Res., v. 75, no. 30, p. 5928-5939.
- Smith, N.D., 1971, Transverse bars and braiding in the lower Platte River, Nebraska: Geol. Soc. America Bull., v. 82, p. 3407-3420.

Sternberg, R.W., 1966, Boundary layer observations in a tidal current: *J. Geophysical Research*, v. 71, p. 2175-2178.

\_\_\_\_\_, 1968, Friction factors in tidals channels with differing bed roughness: *Marine Geology*, v. 6, no. 3, p. 243-260.

Sundborg, A., 1956, The River Kaeälven, a study of fluvial processes: *Geog. Annaler*, v. 38, p. 127-315.

Task Force on Bedforms in Alluvial Channels, 1966, Nomenclature for bedforms in alluvial channels: *Proc. Am. Soc. Civil Engineers*, J. Hydraulics Div. 92, (HY3), p. 51-64.

Toffaletti, F.B., 1969, Definitive computations of sand discharge in rivers: *Am. Soc. Civil Engineers Proc.* (HY1), p. 225-248.

Tywniuk, N., and Stichling, W., (1973), Sedimentation phenomenon of the Fraser River: *Inter. Assoc. Hy. Res.*, Inter. Symposium on River Mechanics, Bangkok, Thailand, A69-1-13.

Velikōnov, M.A., and Mikhailova, N.A., 1950, The effect of large-scale turbulence on pulsations of suspended sediment concentration: *Izv. Akad. Navk. SSSR. Ser. Geogr. Geofiz.*, 4, p. 421-424.

Visher, G.S., and Howard, J.D., 1974, Dynamic relationship between hydraulics and sedimentation in the Altamaha Estuary: *Jour. Sedimentary Pet.*, v. 44, p. 502-521.

Water Survey of Canada, Dept. of Environment, Vancouver, B.C., (unpublished stage recording data).

Whetten, J.T., and Fullam, T.J., 1967, Columbia River bedforms: *Int. Assoc. Hydraul. Res.*, 12th Cong. Proc., Fort Collins, p. 107-114.

Wright, L.D., Coleman, J.M., and Thom, B.G., 1972, River delta morphology: Wave climate and the role of the subaqueous profile: *Science*, v. 176, p. 282-284.

\_\_\_\_\_, \_\_\_\_\_, and \_\_\_\_\_, 1973, Processes of channel development in a high-tide-range environment: Cambridge Gulf-Ord River Delta Western Australia: *Jour. Geology*, v. 81, p. 15-41.

Yalin, M.S., 1974, On the formation of dunes and meanders:  
Int. Assoc. of Hydraulic Research, c 13, p.1-8.

Znamenskaya, N.S., 1963, Experimental study of the dune  
movement of sediment: Trans. State Hydrologic Inst.,  
no. 108, p. 89-114.

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\_\_\_\_\_, 1967, The analyses and estimation of  
energy loss: Proc. Int. Assoc. Hydraulic Research,  
12th Cong. Proc., Fort Collins.

## PART TWO:

## INTRODUCTION

Pitt River (North) - Pitt Lake - Pitt River (South) system is situated in a glacially scoured valley within the Coast Mountains of British Columbia approximately 30 km inland from the port of Vancouver (Fig. 1). The valley of the Pitt, 70 km in length opens abruptly into Fraser lowland. Pitt River (North) drains 816 km<sup>2</sup> including several mountain glaciers and provides a mean discharge of 80 m<sup>3</sup>.sec<sup>-1</sup> to the lake. A prominent sill, 5 km from northern end of lake, allows only clay-sized sediment to be carried to the lower end of the lake.

Pitt River (South) and Pitt Lake are tidal, being connected to the ocean (Strait of Georgia) by lower Fraser River. Although water levels in the Pitt system respond to the tides, salt water seldom extends closer than 10 km downstream of the Fraser - Pitt confluence. Rising water (flood tide) in the Strait retards flow of the Fraser and raises its elevation progressively eastward until the water level at the Fraser-Pitt confluence is higher than in Pitt River (South). Flow in the Pitt then reverses and water diverted from the Fraser flows northward up Pitt River (South) into Pitt Lake. As the water elevation falls (ebb tide) in the Strait, Fraser River flow is accelerated.

FIGURE 1. Location map of Pitt tidal system.

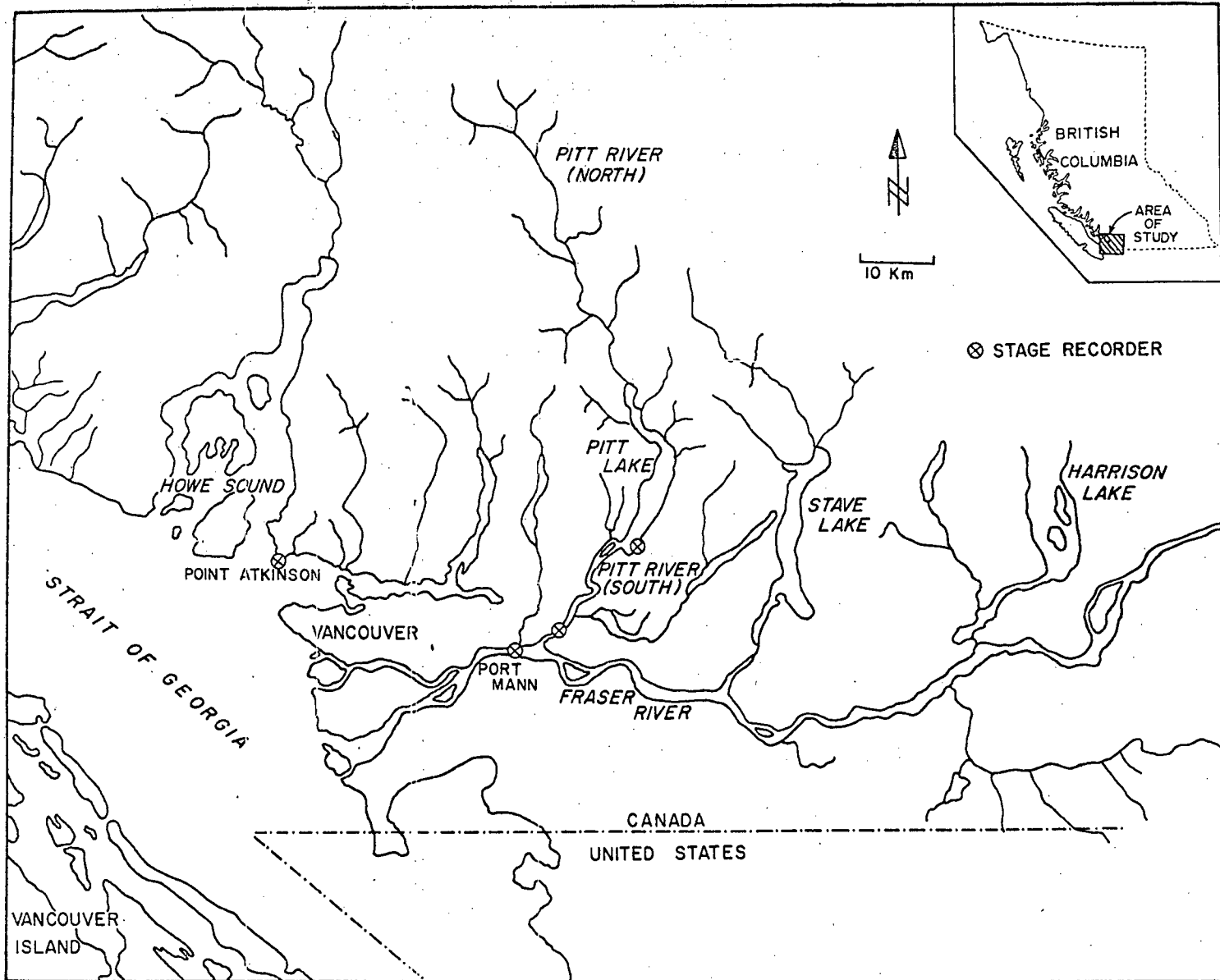
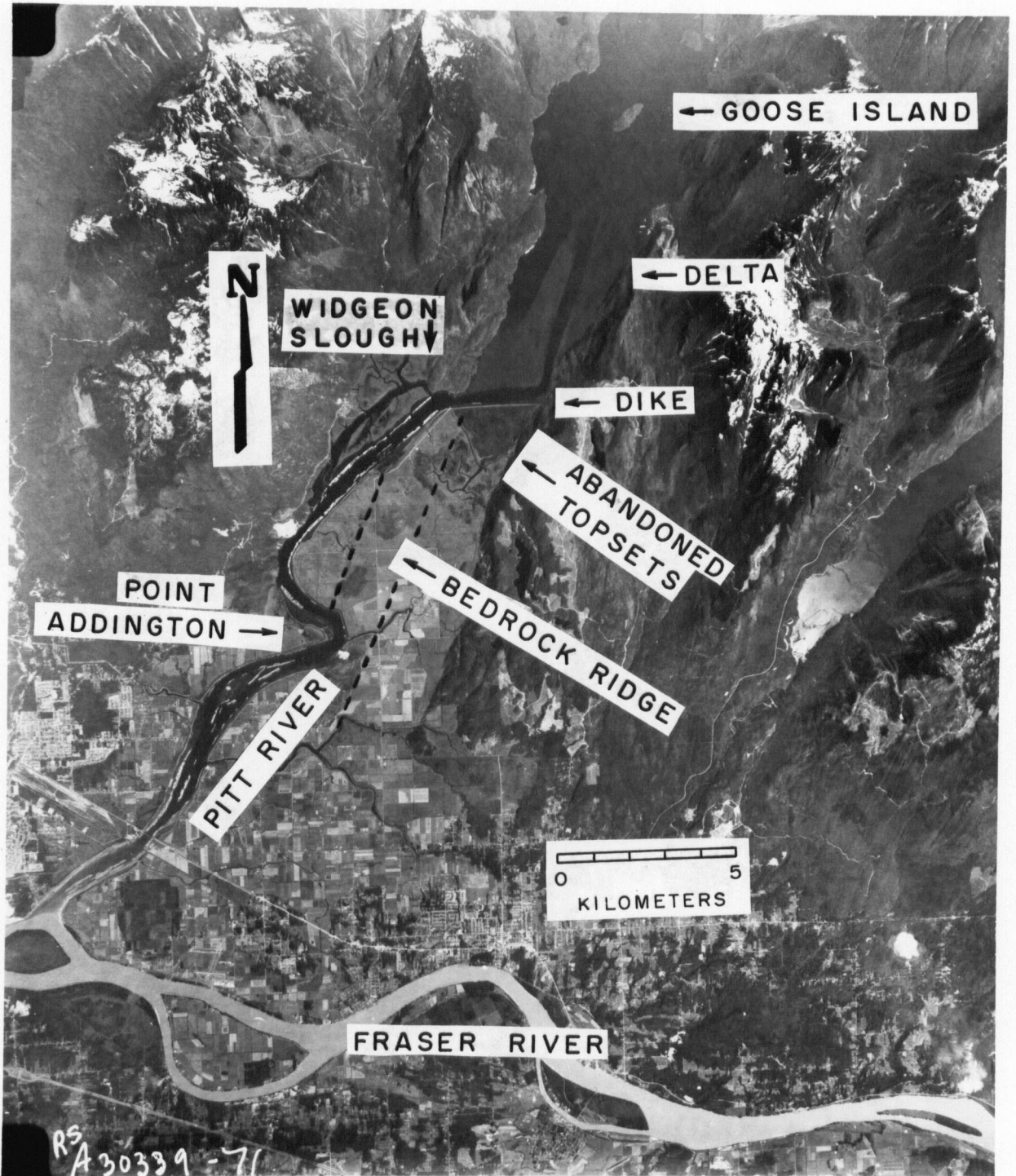




FIGURE 2. Aerial photo showing the main physiographic features of the lower Pitt system. The bedrock high is outlined with dashed lines. Its extent is based on isolated bedrock knobs that protrude through the flood plain.



The surface elevation is lowered progressively eastward until the level at the Fraser - Pitt confluence is less than that of Pitt River (South). Flow then reverses in the Pitt system and drains toward the sea. The elevation and magnitude of water level oscillations in the Pitt system are a function of the complex interaction of Pitt basin drainage, Fraser River discharge, and the tidal prism.

Upstream movement of sediment in Pitt River from Fraser River toward Pitt Lake is indicated by: (1) a predominance of flood-oriented bedforms in the river channel; and, (2) a decrease in grain size from the Fraser to the lake. In addition, velocity and stage measurements demonstrate that flood flows have higher peak velocities and that flood flows persist for a shorter time period than ebb flows.

A large tidal delta with a surface area of  $12 \text{ km}^2$ , has accumulated at the distal (draining) end of the lake (Fig. 2). Because of the unusual position of the delta there has been speculation on whether it is actively growing or a relict feature from earlier post-glacial time. The purposes of the present study are twofold: first, to determine if the delta is active and to estimate the present sedimentation rate; and second, to examine the hydraulics of the lake channel and to evaluate the effect of bidirectional flow on sediment dispersal and delta morphology.

## GEOLOGIC HISTORY

The Pitt tidal delta appears to represent a situation in which the past is the key to the present. An understanding of the historical development of the delta provides an important insight into the nature of the currently acting processes.

During the Pleistocene Epoch repeated glaciations aided by pre- and inter-glacial stream activity have eroded deeply the valleys along a northwest and northeast oriented joint pattern occurring in the Coast Mountains (Peacock, 1935). Following the most recent deglaciation (15,000 - 11,000 B.P.) the melting ice left numerous elongate lakes in interior valleys and a coastline dominated by fiords. However, in early postglacial time the exact location of the shore fluctuated as a result of a complex interaction of eustatic sea level changes and crustal rebound (Mathews et al., 1970). During the period of instability, ocean waters flooded past the mouth of Pitt Valley, as is evidenced by marine shells (12,690  $\pm$  190 B.P.; I-5959, Mathewes, 1973) collected at an elevation of 107 m on the east side of Pitt valley. Isostatic uplift of the Fraser lowland began around 13,000 B.P. and was essentially complete by 8,000 B.P. (Mathews et al., 1970). Fraser River, supplied with abundant glacial sediment, rapidly constructed a delta

westward and by  $8,290 \pm 140$  B.P. (G.S.C. 229, Dyck et al., 1965) "Pitt Fiord" was isolated from the sea at its southern end by this delta. It is likely that a short tidal channel maintained a connection between the fiord and the Fraser estuary. Tidal currents flowing through this channel must have carried sediment from Fraser River into the fiord, building a flood tidal delta which continued to grow northward as Fraser delta progressed westward. By  $4,645 \pm 95$  B.P. (I-7047; Mathews, 1972 pers. comm.) the leading edge of Pitt delta stood at least 20 km north of Fraser River near the present outlet of Pitt Lake (Fig. 1). The dated material was a log found in delta topsets 10 m north of the channel and buried under 60 cm of sediment. At some time during this period "Pitt Fiord" was flushed of saline water and became Pitt Lake; at present time no salt water is found anywhere in lake. As the sea-land relationship has been much the same as at present since 5,500 B.P. (Mathews et al., 1970), it is possible that Pitt Lake has been in existence for approximately 6000 years.

The boundary between Pitt River flood plain and Pitt Lake tidal delta has been a transitional one throughout their development. At present, dikes and ditches have created two entities, but the division is artificial. Historically, water flow and sedimentation have been a continuum from river to lake.

On the basis of aerial photo interpretation (scale 1:15,840; 1:31,680) of the Pitt River flood plain, it appears that the river has been consistently on its west side (Fig. 2). It is suspected that a bedrock ridge connects the isolated hills on the flood plain to the ridge bordering Pitt Lake's southwest shore and has prevented the river from flowing directly into the lake. This ridge may have separated lobes of ice disgorging from Widgeon and Pitt Valleys during the Pleistocene. The bedrock also deflects both flood and ebb flows at Addington Point, a sharp meander bend.

The triangular area directly south of the lake (Fig. 2) is abandoned delta surface and lies at approximately the same elevation as delta topsets in the lake. However, the area is slightly lower than the surrounding flood plain and diking in the 1920's on the east, south, and west borders and a dike placed on the north side (1959) have permanently sealed the location from further clastic sedimentation.

During the last 4,700 years the delta front has advanced from the present lake outlet approximately 6 km north into Pitt Lake at the average rate of 1.28 m/yr. However, with the change from paraglacial to nonglacial conditions sediment supply would decrease (Ryder and Church, 1973). In addition, containment of Fraser River within the last century may also have been important in altering sediment supply to the Pitt system. Thus this progradation

rate most likely has decreased exponentially, starting at meters per year and decreasing to the probable present rate of centimeters per year. A map produced by Richards (1860) shows the delta with the same general configuration as present, but accurate delta growth rate calculations for the last 118 years could not be made from it.

## GEOMORPHOLOGY

Delta

The present delta surface covers 12 sq. km. (5.8 km long and 2.2 km wide) and contains a single distributary channel with a right-angle bend (Fig. 3). Minor erosion in the form of a scalloped channel margin occurs near the bend (Fig. 4A); however a study of aerial photos dating back to 1940 indicates little change in 35 years. The channel is incised in the reach between the lake entrance and the bend, with nearly vertical channel banks in some places (Fig. 5). However, the channel banks gradually change from steep to gentle slopes toward the end of the delta (Fig. 5) in conjunction with a gradual shallowing of the channel. The delta surface is highest at its southern margin and slopes down ( $6.0 \times 10^{-4} \text{ }^{\circ}$ ) toward the topset/foreset slope break. During low water in Pitt lake the southernmost kilometer of delta is exposed and minor southerly draining channels in a dendritic pattern are eroded into the topsets (Fig. 3; Fig. 4A) by water draining from the delta surface into the channel during ebb flow. The drainage channels are 2 - 3 m wide and 1 m deep at their widest cross section. Levees border both sides of the major delta channel (Fig. 4B) and a few minor flood exit grooves are eroded diagonally through the levees (about 1 km from end) marking



FIGURE 3. Geomorphology of Pitt tidal delta with lake bathymetry. Depth contour interval is 10 m. A topographic "high" on the lake bottom connects islands and the bedrock ridge bordering the southwest side of lake. This "high" is coincident with the 70 m depth contour and  $6\phi$  mean grain size contour (Fig. 11) and is used as an arbitrary division between delta foresets and bottomsets - lake bottom. Cross section (A-K) locations of Figure 5 are illustrated. Cores used for  $^{137}\text{Cs}$  dating shown by \*.

# PITT DELTA GEOMORPHOLOGY

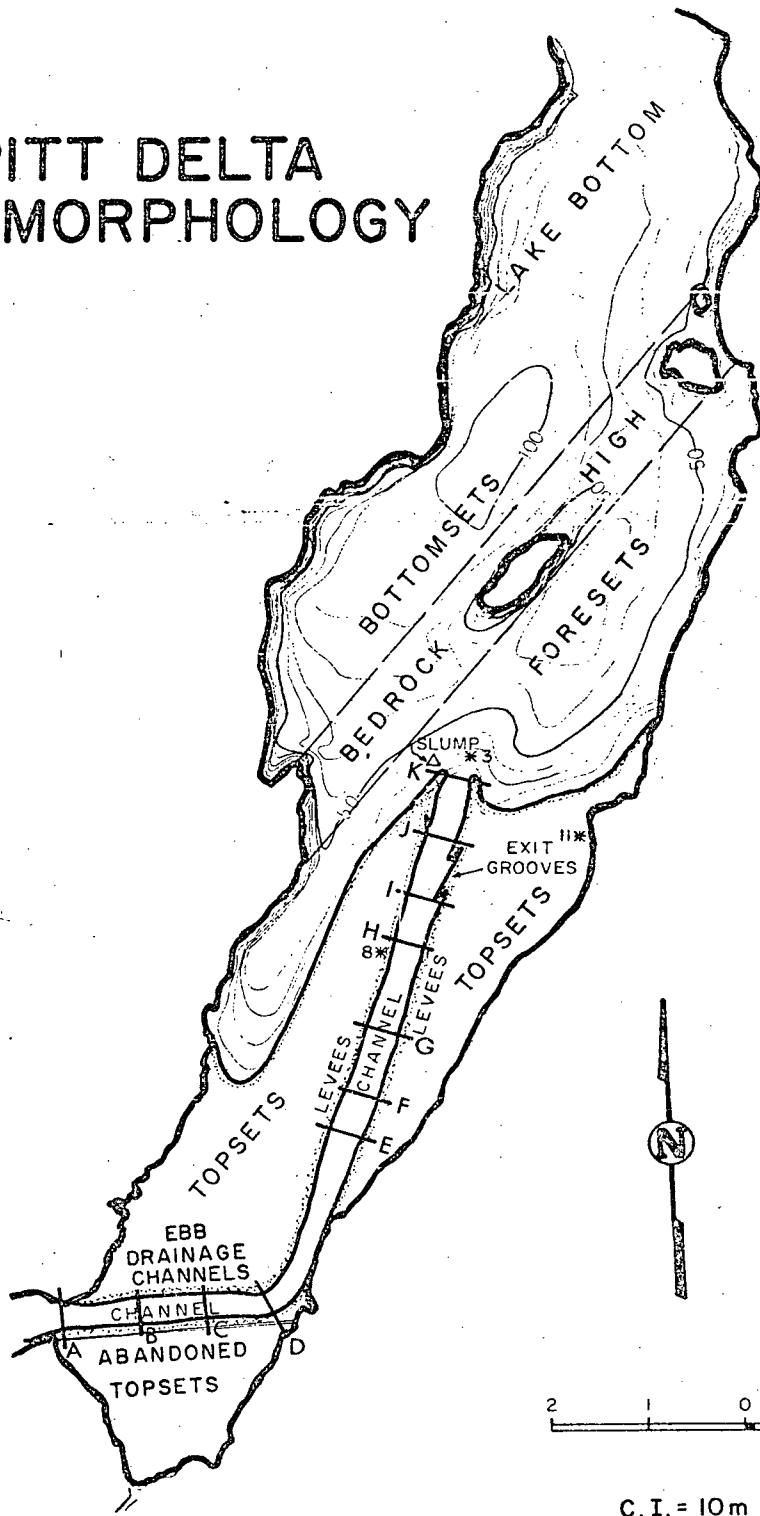


FIGURE 4. A. Oblique aerial photo looking east at right-angle bend. Note ebb drainage channels and scalloped margin of topsets. Wind-generated waves cover water surface.

B. West side of delta topsets. Levees can be seen bordering topset margin in the foreground. Boat wake (30 m) for scale.

C. View looking east across end of delta. Channel in center (bordered by levees) leads to a pointed fan-shaped deposit on delta foresets just left of the photograph.

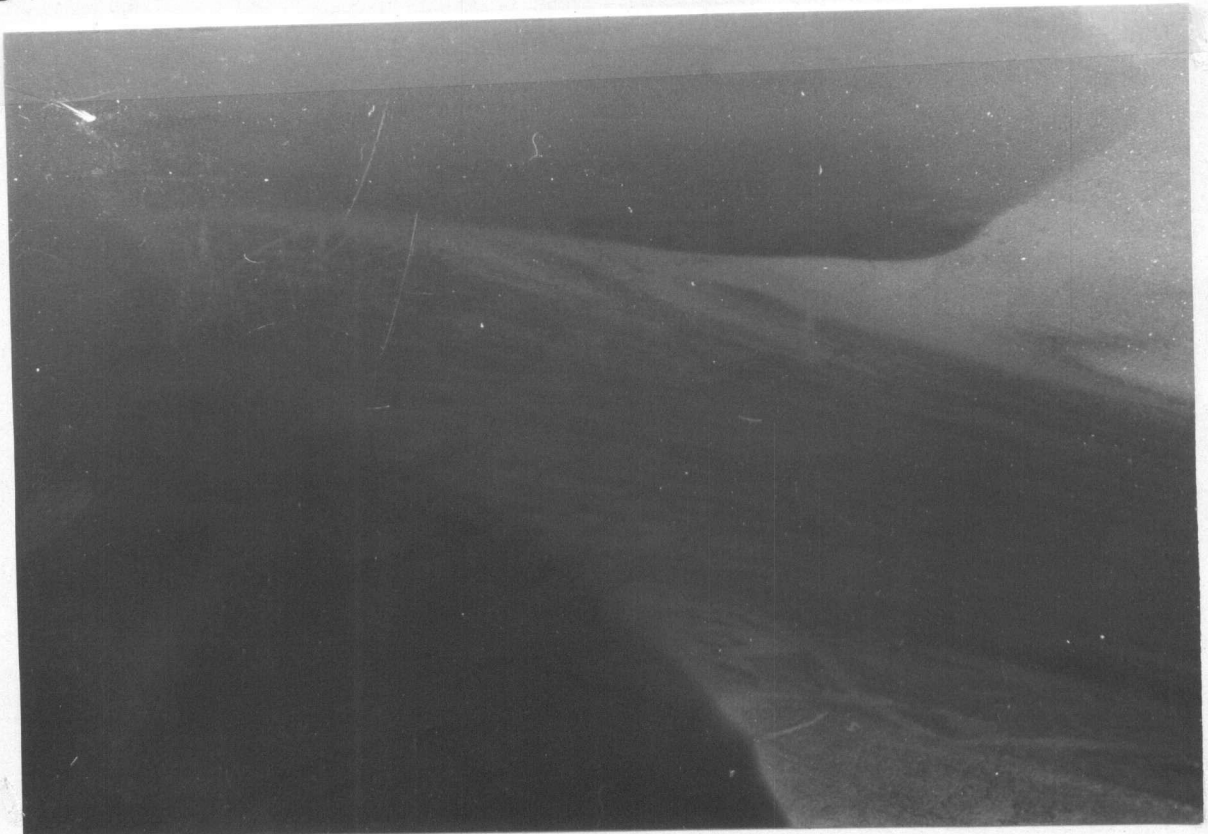
A



**B**



**C**

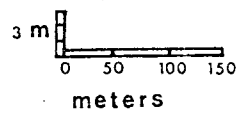
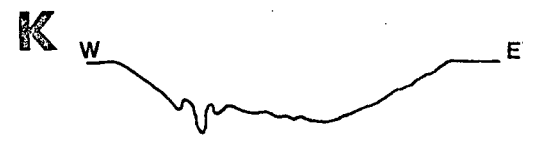
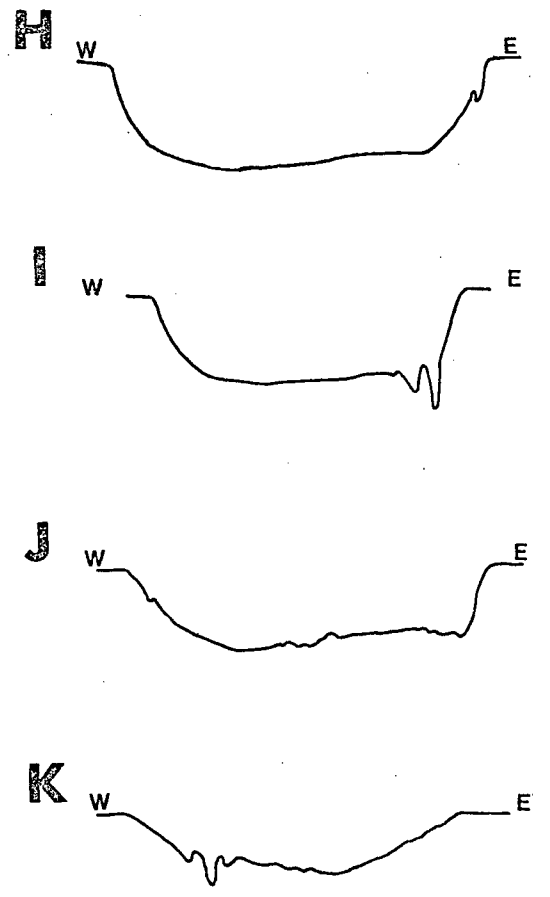
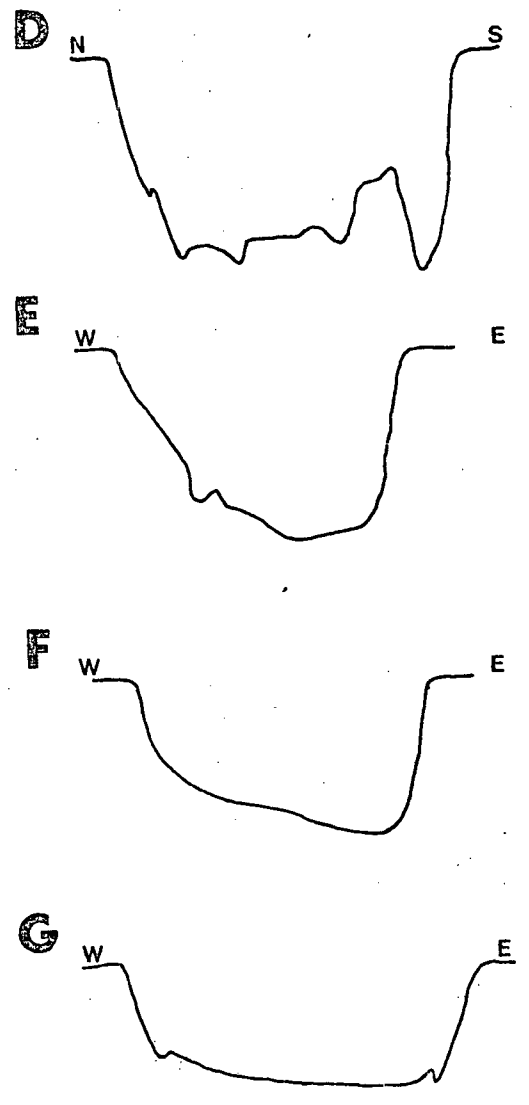
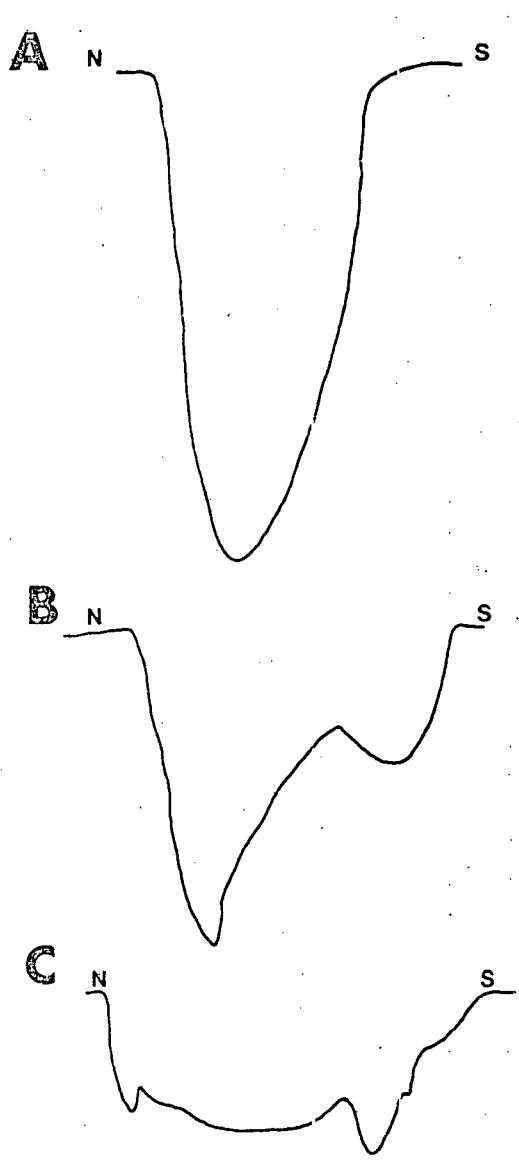


crevasse splays where sediment is carried up out of the channel onto the delta surface (Fig. 3).

A longitudinal profile along the thalweg (Fig. 6) shows the lake entrance and right-angle bend to be extremely deep (30 m) whereas the reach between the deeps is more shallow (10 m) and thus probably is an area of (temporary) deposition. The section of channel from bend to delta front is a ramp which shallows from 30 m to 4 m in a gentle slope of  $0.3^{\circ}$  to  $0.05^{\circ}$ . The thalweg appears to have one partial meander which is similar in length ( $\lambda_M = 600$  m) to meanders of Pitt River (South) (Ashley, 1977). The channel bottom projects as a wedge-shaped tongue (flanked by levees) into the lake (Fig. 3; Fig. 4C) pointing northeast in the direction of delta-front progradation (east side of island).

The delta topset surface is flat and devoid of any major topographic features with the exception of the ebb drainage channels and the levees. Occasional scour holes (0.5 m deep) on the surface reveal a horizontally stratified, highly cohesive sediment. The occurrence of nearly vertical banks bordering the delta channel supports this conclusion. The binding agent is thought to be organic in nature as little clay is present in the sediment. Isoetes echinospora dur. (quillwort), is ubiquitous on the delta surface. Roots of this plant are thin, white,

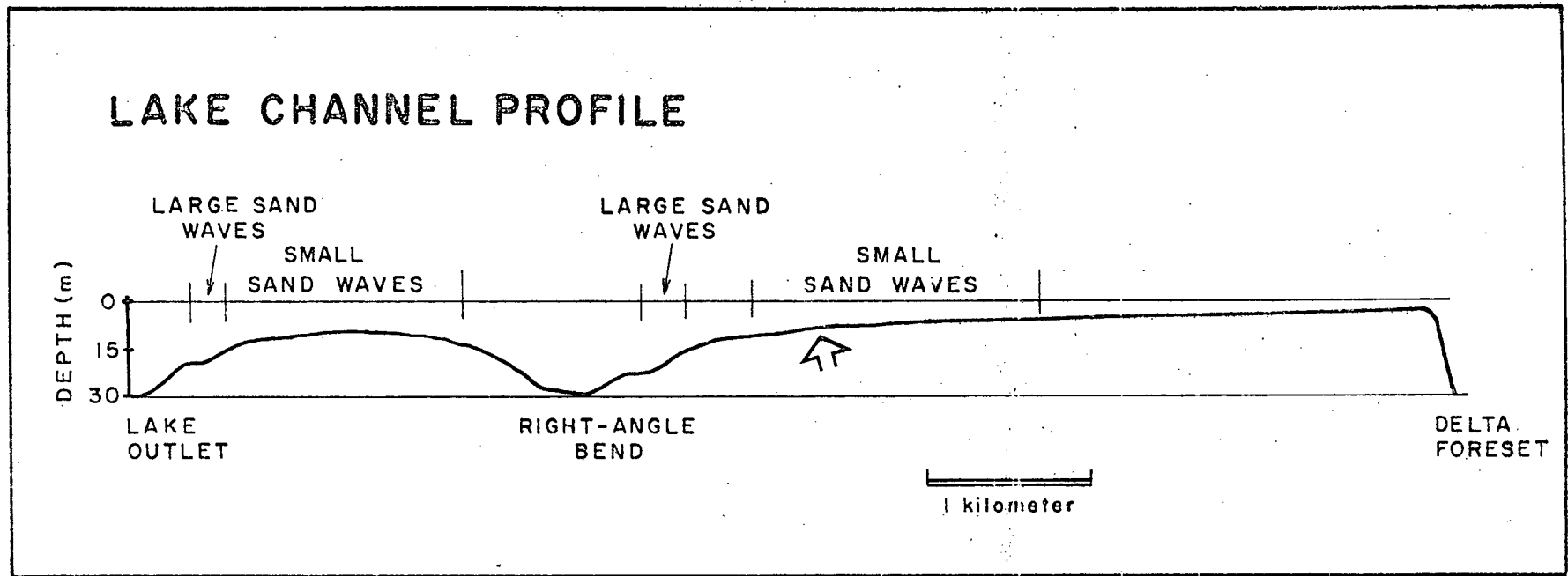
FIGURE 5. Cross sections drawn from depth sounding profiles (8X vertical exaggeration). Profile locations shown on Figure 3. A general shallowing of the channel and change of channel bank slopes from almost vertical to gently dipping occurs along the delta from outlet to the end.



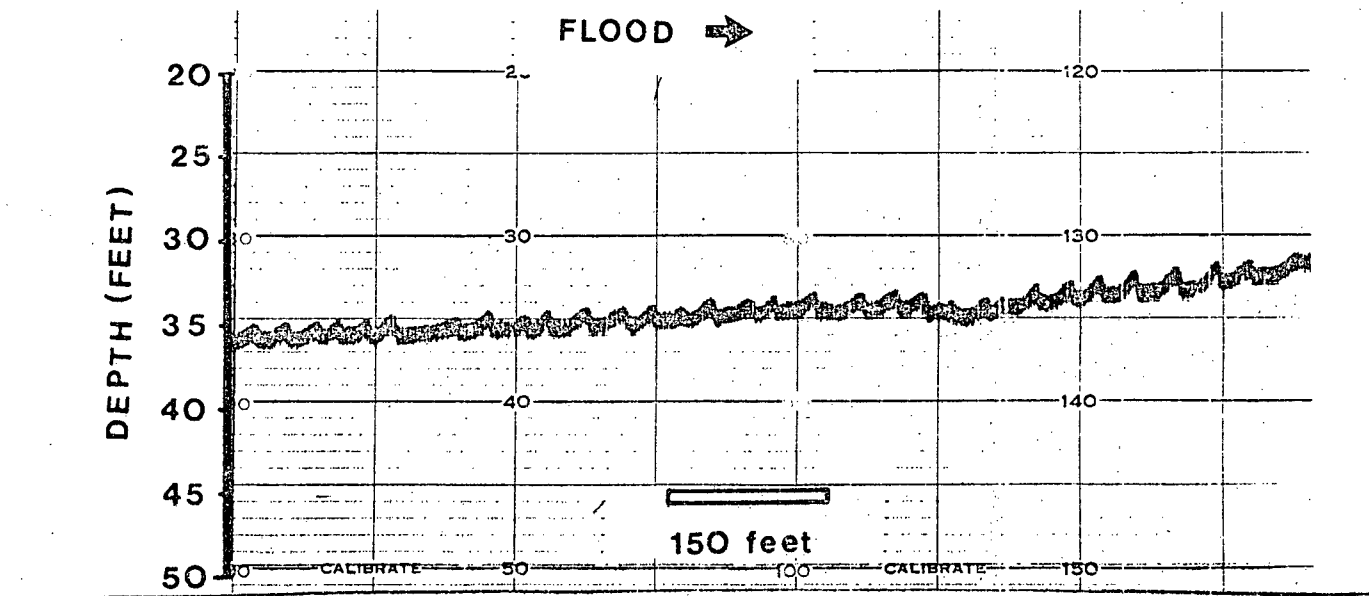


- FIGURE 6. A. Profile of thalweg of delta channel. Deep areas occur at outlet and right-angle bend. Large sand waves (L.S.W.) are found in areas of shallowing channel. Small sand waves are found to within 3 km of the end of the delta. The location of depth soundings taken in B. is indicated by arrow.
- B. Depth sounding of small sand waves in delta channel: note flood orientation. Spacing is 8 m; height is 30 cm.

A.



B.



threadlike filaments which do not decompose readily: they were found in all surface samples. It is interpreted that this macrophyte is an important agent in binding the sediment. Other Macrophytes (Scirpus validus Vahl., Myriophyllum hippuroides Nutt., and Potamogeton sp.) also populate the flats. Other possibilities for cementation are micro-organisms. Blue-green algae were found to be rare whereas diatoms are relatively abundant. Mucus produced by the diatoms may act as a temporary binding agent for the delta sediments. Unio clams, spaced 1 m apart, occur on almost the entire surface and appear to feed at the sediment/water interface, causing little noticeable bioturbation in the underlying sediments.

The foreset slope (Fig. 3) was examined by depth sounding. The contact between topsets and foresets is a sharp break in slope and is outlined in the figure. The foreset/bottomset contact is a gradational change in slope from  $4^{\circ}$  -  $1^{\circ}$  to an essentially horizontal surface and is positioned arbitrarily at the bedrock ridge (Fig. 3). This ridge line approximates the 70 m depth contour and is also coincident with the mean grain size contour of  $\phi$ . Delta foresets range in slope from  $1^{\circ}$  -  $2^{\circ}$  near the east shore to  $4^{\circ}$  -  $6^{\circ}$  at the end of the main channel and the "side-sets" bordering the western embayment have a slope of  $10^{\circ}$  -  $20^{\circ}$ . In general, the entire foreset-bottomset slope is gentler to the east side of Goose Island than to

the west and the general shape of the delta indicates that sedimentation has occurred consistently on the east side of the lake. The foresets are generally smooth with a gentle concave upward profile. Only one slump feature (Fig. 3) was noted on the entire foreset apron, indicating a relatively stable slope. The slump has a relief of about 3 meters and occurs just west of the fan (Fig. 4C) created at the end of the distributary channel. Seismic data from the lake (Mathews, unpublished data, 1976) indicates that a topographic high (Fig. 3) exists between the bedrock ridge (bordering the southwest side of lake) and Goose Island essentially splitting the lower end of the lake into two basins.

Based on its geomorphology, the Pitt delta can best be described as a single talon of a birdfoot delta which has been welded to the eastern lake shore. A depositional model for the birdfoot delta includes progradation of the distributary channel into relatively deep water (Scruton, 1960). Sediment is conveyed along the delta channel and is brought out periodically and deposited on the delta surface as levees. Along each side of the major channel are interdistributary troughs which slowly fill with fine-grained sediment. As the distributary channel extends into standing water, it broadens, becomes more shallow and gradually loses its identity (Reineck and Singh, 1975).

The Pitt appears to fit this general model. It is clearly dominated by fluvial processes. The depositional environment is one of very low energy and little reworking of the fluvial sediments occurs by waves or tidal currents.

#### Bed configurations in the channel

In conjunction with the study of Pitt delta geomorphology an examination was made of the bed configuration of the delta channel bottom. Soundings were made over an 18-month period, under both ebb and flood flows. Using depth sounding records (Raytheon, model #DE-119), side-scan sonar records (Klein, model #2000), and visual observation by divers, two bedform types were found; ripples/spacing ratio = 1:10; spacing 60cm) and sand waves (spacing ratio = 1:30, spacing 5m). Ripples are ubiquitous on the sandy substrate of the channel bottom, as well as on the sandy delta topsets. Small sand waves (10 - 15 m spacing and 0.15 - 0.3 m high) are found in the area between the outlet and the right-angle bend and on a portion of the ramp north of this bend (Fig. 6). Larger sand waves (25 m spacing and 0.7 m high) occur only in reaches of rapidly shallowing depth (Fig. 6A). All bedforms were found to be flood-oriented, which is interpreted as reflecting the dominant flow conditions and direction of net sediment transport (see Ashley, 1977).

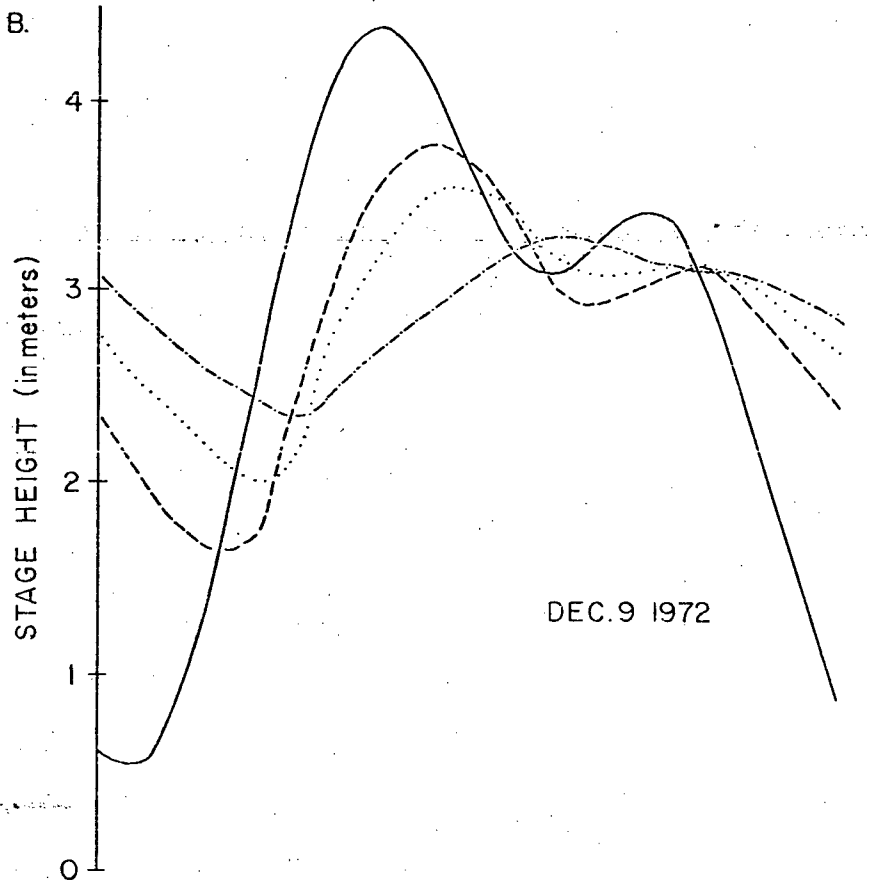
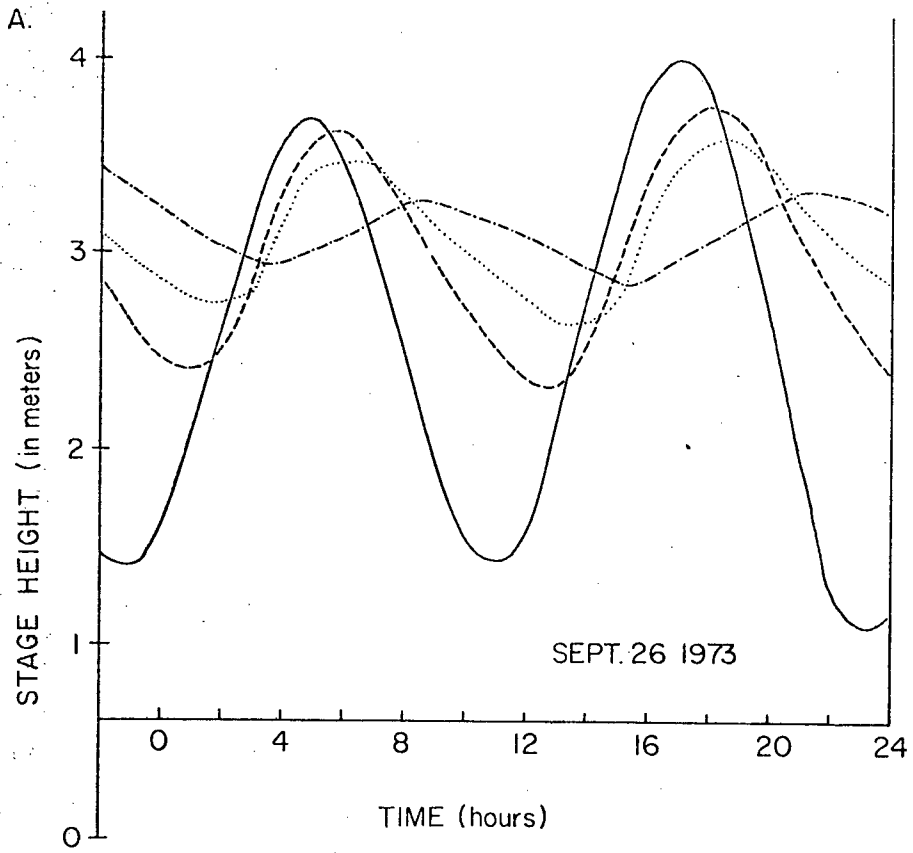
## HYDRAULICS

Tides

The main driving force behind the hydrodynamics of Pitt Lake is the tide. The mixed, mainly diurnal tide in the Strait of Georgia produces one or two tidal cycles a day in the lake, depending upon the nature of the tidal curve. Water level (stage) data used (Fig. 7) are unpublished records of the Water Survey of Canada. Minor features such as small stage fluctuations and quick short changes in flow direction are damped between the ocean and lake and are not expressed in lake stage. When flow conditions persist for several hours (symmetric diurnal tides in the Strait), diurnal lake stage curves are produced (Fig. 7A). On the other hand, highly asymmetric tidal curves, such as shown in Figure 7B, produce only one complete cycle a day. During winter, a delay of 5 hr 15 min. occurs between high tide in the Strait and high tide in the lake, while a 6 hr. 20 min. delay occurs for passage of low tide from Strait to lake. During the freshet when the contribution of Pitt basin drainage is high, it takes 15 hr 30 min for either high or low tide to pass from the Strait to the lake. Lake stage level fluctuations varied from 0.27 m to 1.16 m within a tidal cycle, during the

FIGURE 7. Time stage curves for Strait of Georgia ———, Fraser River - - - -, Pitt River ....., and Pitt Lake .-.-.-.-.

- A. Semi-diurnal tide in the Strait creates semi-diurnal fluctuations in Pitt Lake.
- B. The effect of mixed, mainly diurnal tide in the Strait is damped by the time it reaches the lake causing only one fluctuation in lake level.





year (1973) of stage data examined in detail. Table I gives maximum, minimum, and mean ranges for four representative months.

In addition to tidally induced oscillations in water level in Pitt Lake, the absolute level of these oscillations changes seasonally with a maximum during freshet run off (May - July) and a minimum during winter (Dec. - Feb.). Discharge (Q) contributed to Pitt system from Pitt River (North) and small streams surrounding the lake varies from  $210 \text{ m}^3/\text{sec.}$  (freshet) to  $30 \text{ m}^3/\text{sec.}$  (winter) (Water Survey of Canada, 1966). The result is that during the freshet more than 50% of water moving through the Pitt Lake - Pitt River (South) system is contributed by basin drainage contrasting with only 5% during the winter.

The magnitude of discharge flowing through Pitt River (South) (Ashley, 1977) and into Pitt Lake is directly related to the magnitude of the tidal range in the Strait, if Fraser and Pitt basin discharge are constant. With high discharges in the Fraser and Pitt during the freshet the tidal effect in Pitt Lake is small; however, when discharges of Fraser and Pitt systems are low (winter), the tidal effect is great. Peak flows estimated for both seasons and both flow directions are compared in Table II. Estimates were made using lake area, lake stage curves, velocity measurements at lake outlet, and cross sectional area of lake outlet. Thus, there are not only pronounced seasonal

TABLE I Range of lake stage levels (1973) in meters.

MONTH	MAXIMUM	MEAN	MINIMUM
March	1.04	.73	.67
June	.67	.45	.27
Sept.	.82	.64	.42
Dec.	1.16	1.04	.67

TABLE II Estimated peak discharges for Pitt system.

SEASON	FLOOD $\text{m}^3 \text{sec}^{-1}$	EBB $\text{m}^3 \text{sec}^{-1}$
WINTER	2400	2080
FRESHET	1800	950

differences, with winter having the highest discharge ( $2400 \text{ m}^3 \cdot \text{sec}^{-1}$ ) but also during either season the largest flood discharge is greater than the largest ebb discharge. The greater difference in discharge between flood and ebb of freshet (Table II) compared to flood and ebb discharge of winter, is due to the increase in volume of water moving through the Fraser-Pitt systems (during the freshet). Water added by streams draining into Pitt Lake raises the elevation of the lake surface as much as 3 m. The elevation of Fraser River is also increased and the net effect is a decrease in the water slope of the upstream flow (flood) into the Pitt. The raised lake elevation also accentuates the time-stage asymmetry of the tidal cycle and thus changes the proportion of time devoted to flood (lesser) and ebb flow (greater). The ebb current flows for a longer period of time (65% - 75% of total) at a lower discharge which produces a lower ebb water slope compared to the winter.

Flow pattern over the delta is significantly different on flood and ebb. Flow entering the lake from the river is mainly confined within the deep distributary channel (Fig. 8A). The flow is then deflected northward at the east side of lake causing considerable scour (35 m deep). Continuing along the delta, flood currents generally remain confined in the channel to within 1.5 - 1 km from the end where they spread out across the topsets. Some "over bank" flow occurs along the length of the distributary as evidenced

by the levees. Ebb flow has a much more diffuse pattern (Fig. 8B). During the beginning of the ebb, water drains off the topsets into the channel taking the shortest, most direct route. At lower ebb stage, flow becomes more channelized and is confined in the distributary.

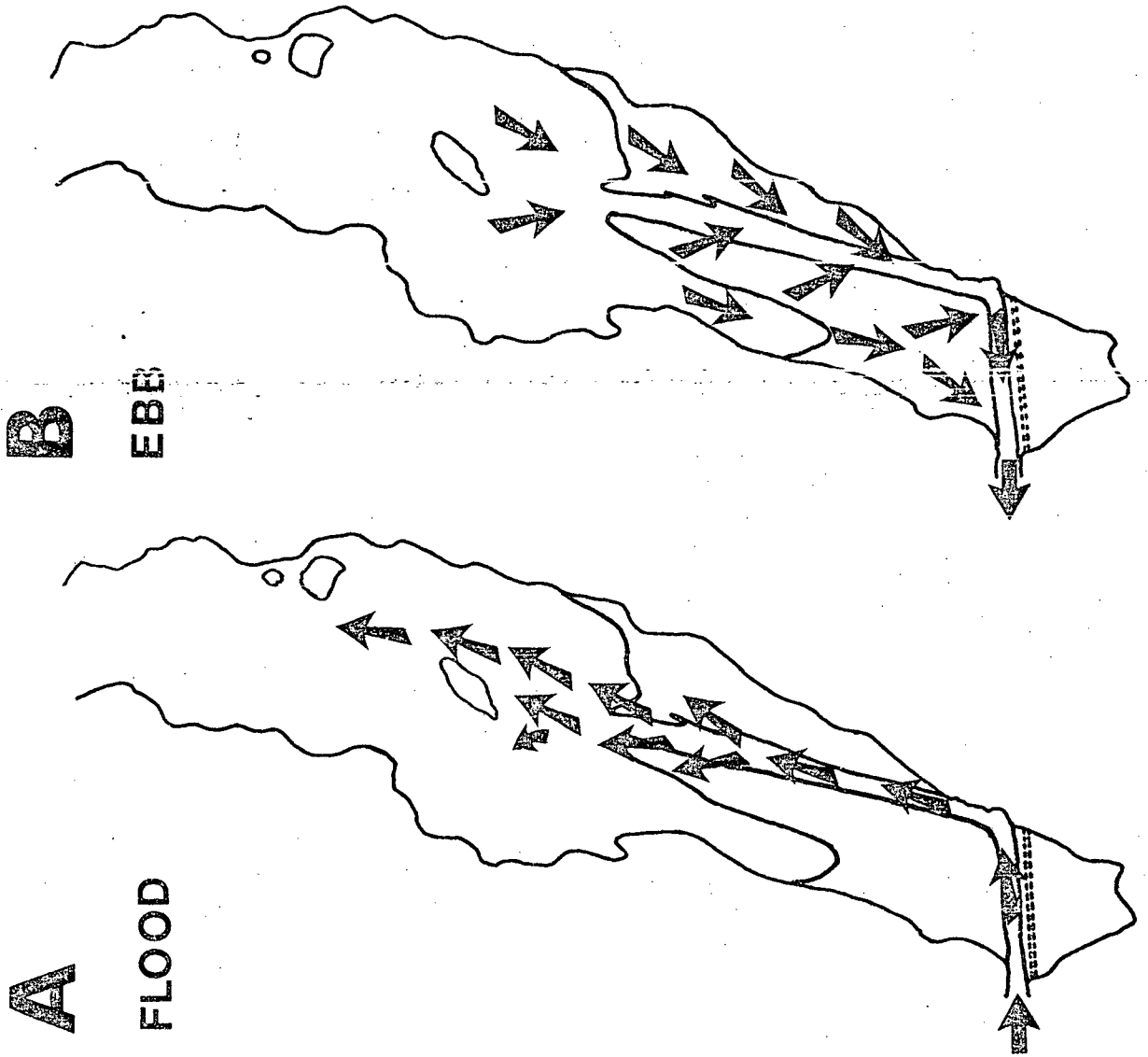
### Velocity in channel

A study of velocity was undertaken at the lake outlet and in the delta channel to determine the flow conditions that would likely entrain and transport channel bed material. Two different methods of current measurement were used: (1) four days of current profiles, taken at 30-minute intervals over a flood or ebb cycle, (2) readings taken at 7.5-minute intervals, with a tethered meter, one meter from bottom (19 days).

Current profiles (Hydro Products, Inc. Savonius Rotor with a direct readout for current speed (model #460A) and direction (model #465A) ) were made from a boat anchored at the lake outlet. Each profile included measurements at 7 depths ( $d$ ) (10 cm from bottom, one meter from bottom,  $0.2d$ ,  $0.4d$  (mean),  $0.6d$ ,  $0.8d$ , and surface). The measurements (both magnitude and direction) at each depth were based on readings averaged over a two-minute period, thus each profile spans 15 to 20 minutes. A digital counter integrating electrical pulses over a 10-second period was

FIGURE 8. Tidal flow pattern.

- A. Flood: flow is channelized until 2 km from end where it spreads over topsets in overbank flow. Flow pattern into lake appears to be that of a simple jet oriented to the northeast, i.e., east of Goose Island.
- B. Ebb: flow drains off topsets by shortest route to delta channel then along channel to outlet.



used to average velocity fluctuations caused by micro- and macroturbulence (Matthes, 1947). Mean velocity and velocity at 10 cm from bottom for one complete flood cycle (June 24, 1975) are shown in Fig. 9. Peak mean velocity (47 cm/sec) occurs early in the flood cycle. In contrast, ebb examples revealed that peak velocity occurs late in the cycle. This time-velocity asymmetry was found to be characteristic of velocity curves from Pitt River as well (Ashley, 1977).

Critical shear stress necessary for sediment entrainment at the lake outlet and in the channel near the outlet was determined from Shields' diagram as modified from Briggs and Middleton (1965). A friction velocity,  $V_*$ , of 1.47 cm/sec is necessary to move sediment (mean grain size = 0.25 mm) at the outlet while  $V_* = 1.54$  cm/sec is required to move material (mean grain size = 0.32 mm) in the southern delta channel.

The log velocity law (Prandtl-Von Karman equation) (Inman, 1963) was used on the lake profile data (June, July, and August) to calculate the basal shear stress. Results showed that a critical shear (friction) velocity 1.47 cm/sec was seldom reached in the outlet during this time period. Time series measurements were taken to determine if this were true for other seasons and for the lake channel as well.

The continuously recorded velocity measurements were made by a positively buoyant meter (General Oceanics, Inc. Film Recording current meter (model #2010) ) anchored to the channel bottom but free to sway with changing currents. The meter was located in the middle of the delta channel approximately 1 km from the lake outlet and recorded on film instantaneous readings of magnitude and direction of flow (one meter off bottom) at 7.5-minute intervals. The meter was placed in channel on several occasions, but only one record (April 15 - May 4, 1976) was readable. Portions of this record are shown in Figure 10; Table III summarizes the proportion of total time devoted to ebb (60%) and flood flow (40%). It is important to note that although total time of ebb flow is longer than flood, velocities are significantly lower. For instance, about 1% of ebb time flow is greater than 40 cm/sec in contrast to 13% of time under flood flow.

Analysis of the 19 days of data found that peak velocity and average velocity were higher on flood flows than on ebb (Table IV). It is inferred from this that mean velocity (0.4d measured from bed) is also higher on the flood. In both river and lake data the mean velocity of a profile was found to equal or exceed the velocity at 1 m (see Appendix). The use of the log velocity law on Pitt River velocity profile data (Ashley, 1977) demonstrated



FIGURE 9. Profile data from lake outlet, June 24, 1975. Mean velocity (0.4 depth) reaches maximum of 47 cm/sec. Time-velocity is asymmetric, i.e., peak is reached early, then decreases gradually.

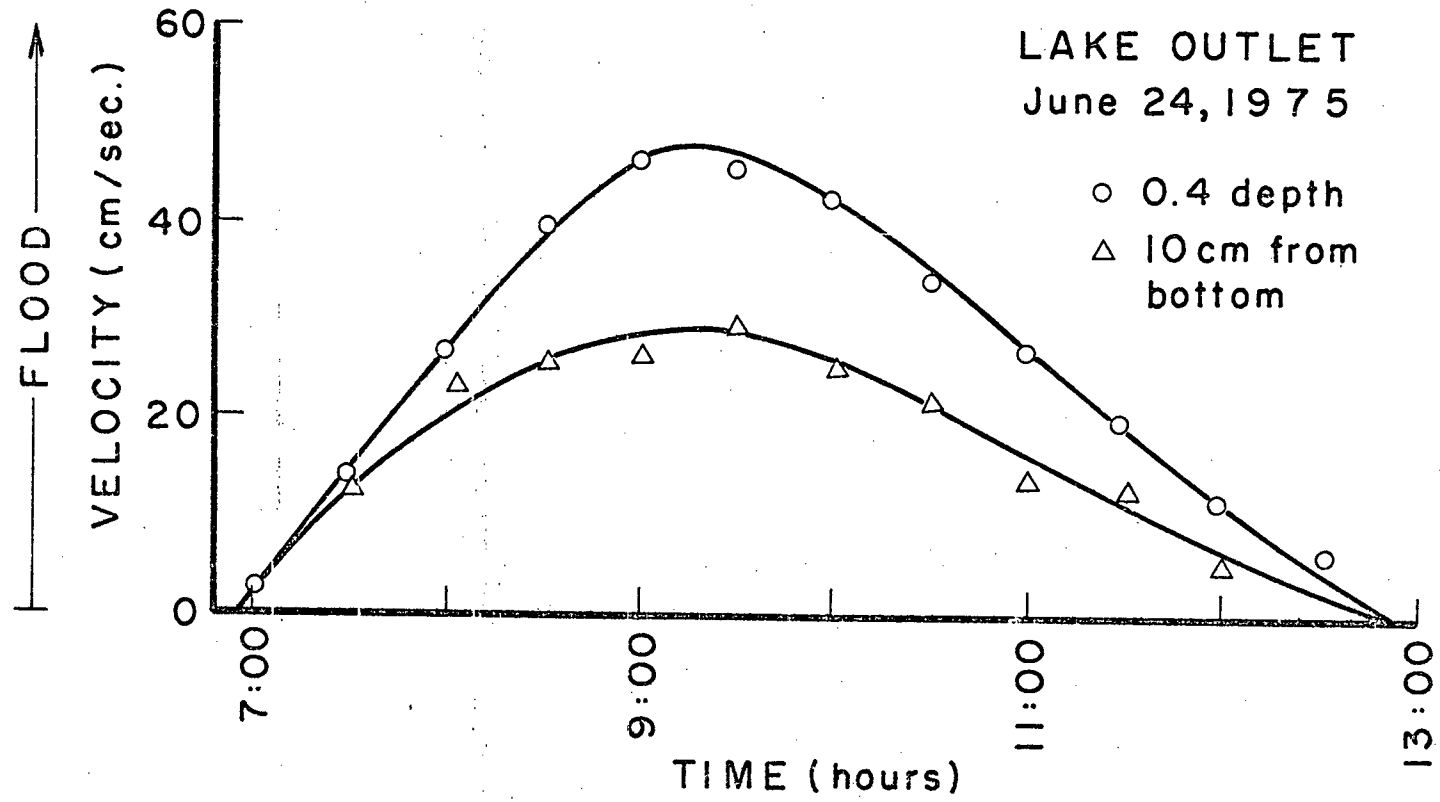
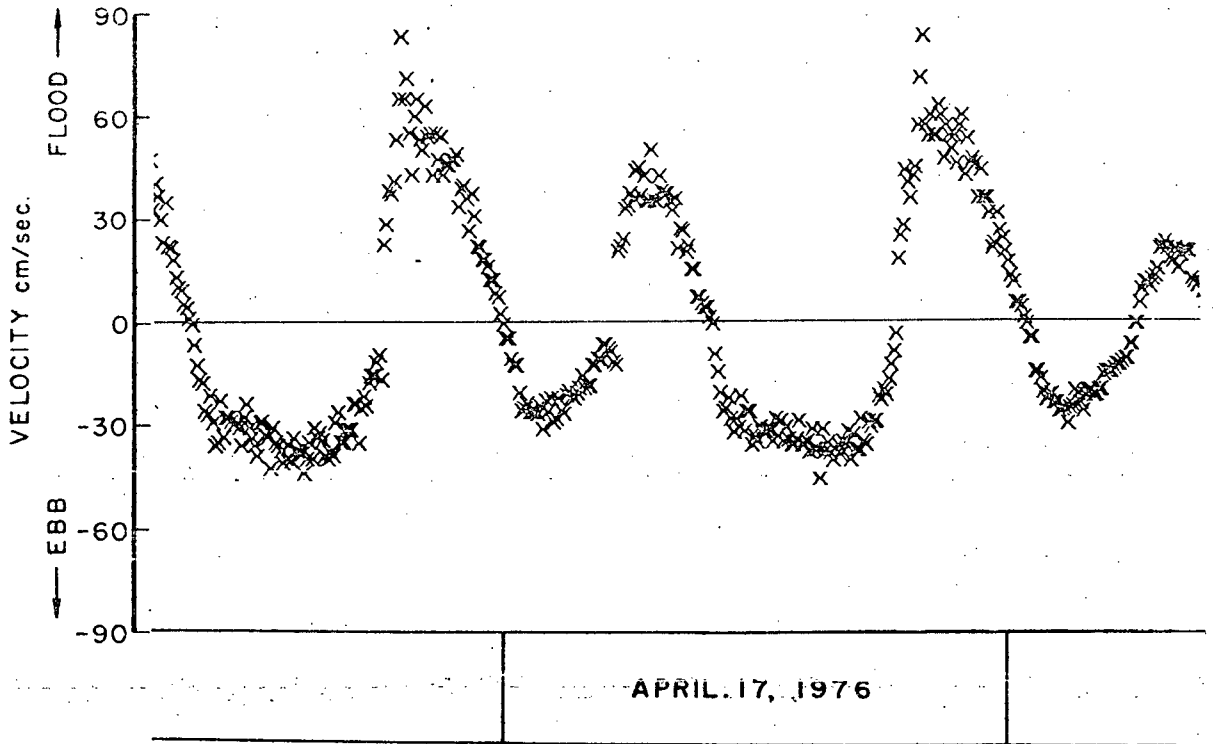


FIGURE 10. Computer plot of "continuously" recorded velocity data from southern delta channel. Each X represents an instantaneous velocity (magnitude and direction) measurement at 7.5-minute intervals. Measurements are one meter from bottom. Note flood velocities are higher than ebb. A. April 16-18, 1976; B. April 26-27, 1976. Data of entire record is summarized in Tables III and IV.

A



B

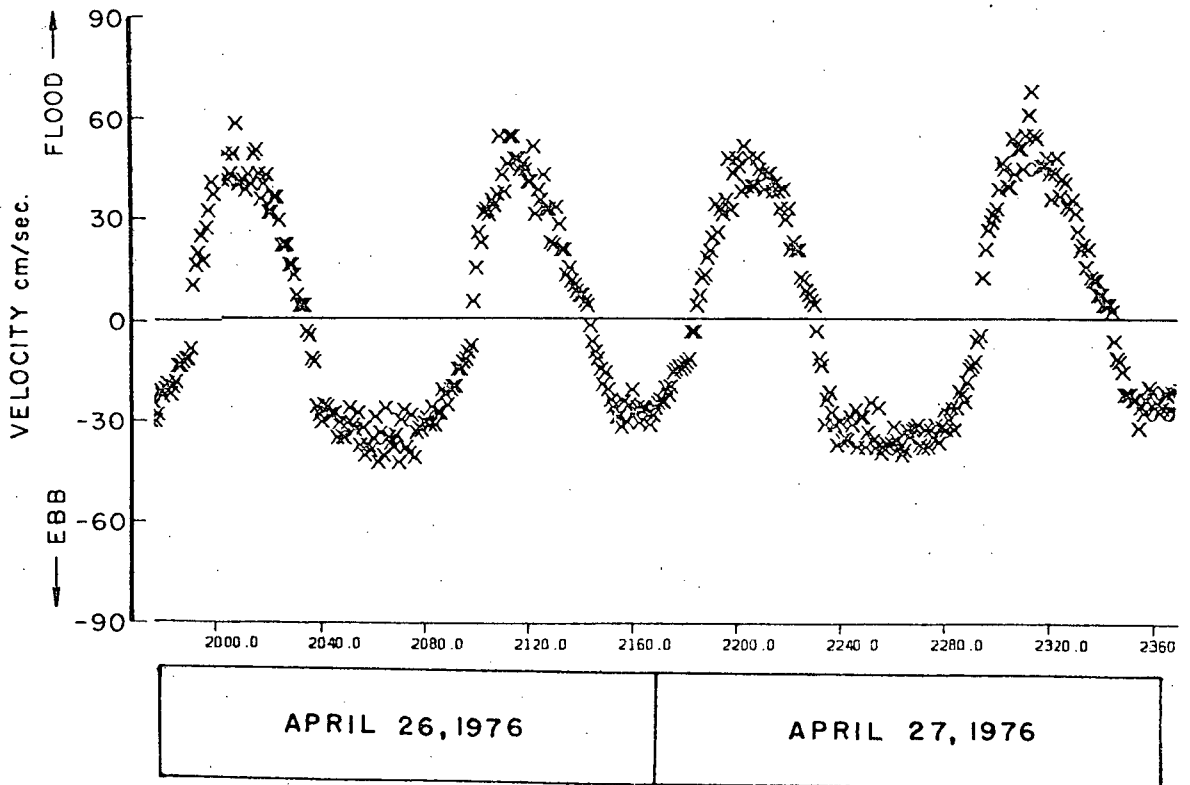


TABLE III Summary of velocity measurements (at one meter above bed) in lake channel April 15 - May 4, 1976: the proportion of time devoted to flood and ebb at 10 cm/sec intervals of velocity.

VELOCITY (cm/sec)	EBB				FLOOD			
	Data Pts.	Hrs.	Cum Hrs.	% Total	Data Pts.	Hrs.	Cum Hrs.	% Total
Vel. 80	0	0	0	0	3	0.75	0.75	0.08
Vel. 70	0	0	0	0	14	3.50	4.25	0.47
Vel. 60	0	0	0	0	29	7.25	11.50	1.30
Vel. 50	2	0.50	0.50	0.05	166	41.50	53.00	5.90
Vel. 40	45	11.25	11.75	1.30	244	61.00	114.00	12.75
Vel. 30	602	150.50	162.25	18.10	291	72.75	186.75	20.80
Vel. 20	764	191.00	353.25	39.50	183	45.75	232.50	26.00
Vel. 10	555	138.75	492.00	55.00	273	68.25	300.75	33.50
Vel. 0	175	43.75	535.75	60.00	230	57.5	358.25	40.00
TOTAL	2143	535.75	535.75	60.00	1433	358.25	358.25	40.00

TABLE IV Summary of velocity measurements (one meter off bottom in lake channel)  
(April 15 - 30, 1976); velocity in cm/sec.

Date (April, 1976)	Max. flood vel.	Ave. flood vel.	Max. ebb vel.	Ave. ebb vel.	Date (April, 1976)	Max. flood vel.	Ave. flood vel.	Max. ebb vel.	Ave. ebb vel.
15	55.5	35.0			23	15.0 45.0	10.0 38.0	31.0 32.0	22.0 22.0
16	41.0 71.0	27.0 39.0	30.5 40.0	20 30	24	52.0 24.0	37.5 14.0	32.0 28.0	26.5 22.5
17	42.0 67.0	31.5 40.0	27.0 38.0	20 31	25	51.0 34.0	32.0 21.0	38.0	27.0
18	22.0 68.0	13.0 40.5	27.0 41.0	18 30	26	47.5 51.0	31.0 30.0	29.0 38.0	22.5 28.5
19	16.0 68.0	10.0 40.0	19.0 45.0	17 28	27	42.5 59.0	29.5 33.0	29.0 38.5	20.5 29.5
20	15.0	10.0	23.0 42.0	16 28	28	38.0 54.0	26.0 32.0	26.0 38.0	20.0 29.0
21	61.0	42.5	28.5 36.0	22 28	29	33.0 55.0	23.5 35.0	27.5 39.0	19.0 29.0
22	61.0	38.0	31.0 33.0	23 23	30	30.0 59.0	22.0 37.0	26.5 36.5	20.0 28.0

that mean velocity of 32 cm/sec was necessary to obtain a critical velocity ( $V_* = 1.77$ ) at base of flow. It follows that a slightly lower mean velocity (approximately 30 cm/sec) would be necessary to create the  $V_* = 1.54$  needed to entrain sediment in the delta channel. When mean velocity is at 30 cm/sec, velocity at one meter from bottom is between 25 and 28 cm/sec. It can be seen in Table IV that more flood time (20.8%) is above 30 cm/sec compared to total ebb time (18.1%). However, the proportion changes drastically at velocity of 20 cm/sec; flood 26%, ebb 39.5%. Thus, it appears that there is more time devoted to ebb flow above critical velocity than to flood, even though the flood velocities are of greater magnitude. In a similar finding in the river data, it was concluded that as most aspects of the study indicate a flood-dominated system the higher velocities are more important in influencing the direction of net transport than total time above critical velocity.

In conclusion, a complex interaction of the tidal prism and varying discharge of Fraser River and Pitt basin results in a flood-dominated system. Highest peak discharges and related basal shear stresses occur during flood (winter) flows. Thus, net sediment transport would occur during the winter. The greater efficiency for entraining and moving sediment under flood flow supports the conclusions based on the morphology of the delta, that it is presently active and being constructed under flood conditions by Fraser derived sediments.

## SEDIMENTS

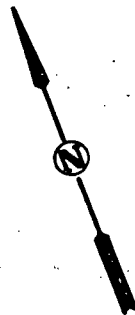
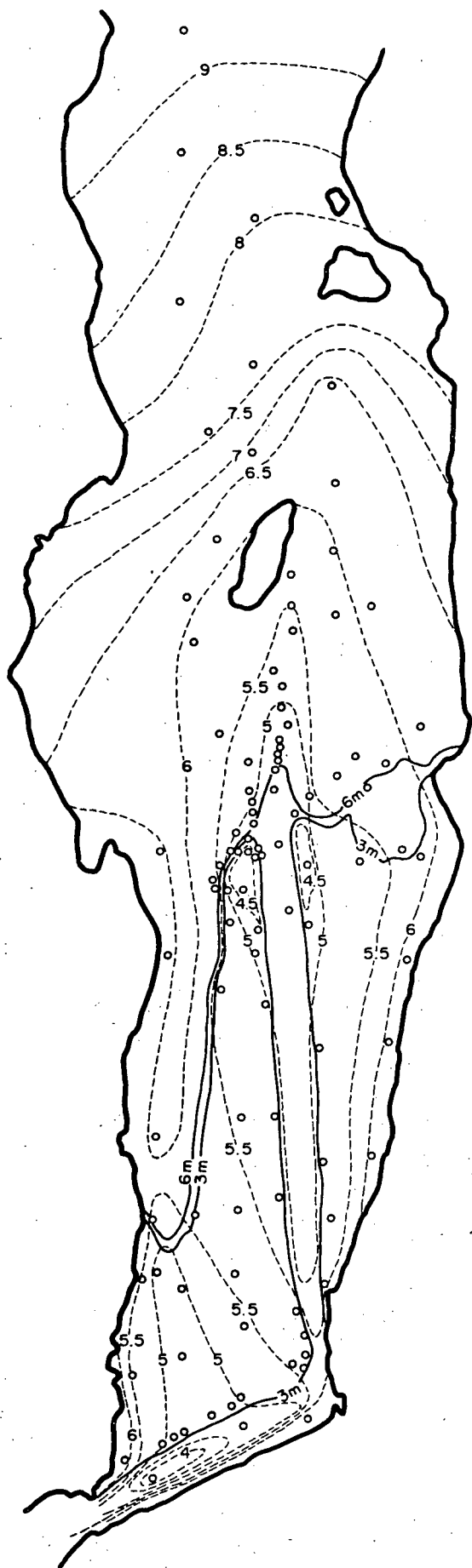
Stratigraphy of delta and lake bottom

Sediments of Pitt tidal delta can be grouped into three general environments: topset, foreset, and bottomset-lake bottom. The topset beds consist of fine sand to coarse silt and are horizontally laminated. The foresets consist of silt and clay layers, some of which are rhythmically layered, whereas the bottomset-lake bottom beds are laminated clays. Of the 160 samples in the study area, 60 were grab samples on delta topsets and in the delta channel and 100 were cores (3.5 cm in diameter) taken from delta foresets and bottomset-lake bottom (Figure 11). Cores ranged from 24 cm to 53 cm in length.

Topset beds consist of a monotonous section of laminated silts and sands. No cross beds and only a few graded beds were noted. On the other hand, the foreset beds were found to contain a variety of bedding structures. The nature of the layering ranges from well developed rhythmic silt and clay layers to stringy and discontinuous clay laminations (Fig. 12). In the rhythmites, silt layers are thicker than clay, but the absolute thickness of the individual layers varies with distance from the delta. Silt layers range in thickness from 1.3 cm at the distributary



FIGURE 11. Mean grain size distribution map. C.I. is 0.5  $\phi$ . Grain size distribution reflects the flood flow pattern (Fig. 8A). The pattern is a good example of sedimentation by diffusion from a simple jet with little, if any, reworking by waves or tidal currents.



— 3m — Depth contour  
--- 5.5 --- Mean grain size contour

C.I. =  $0.5\phi$

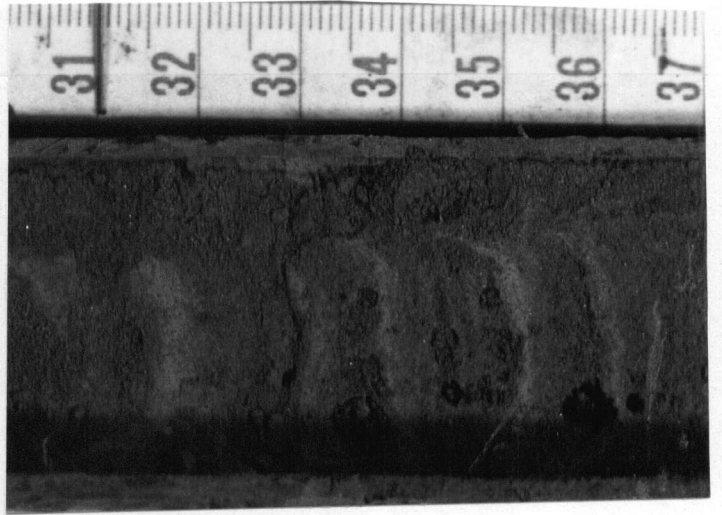
○ Sample localities

Scale :  
|-----|  
1km

FIGURE 12. Diagrammatic sketch of stratigraphy showing change from regular rhythmites through a few transitional couplets into thinly bedded sediments (30 laminations).

A. 3.5 cm diam. core. Top of stratigraphic section showing a sharp decrease in sedimentation rate from (B).

B. 3.5 cm. diam. core. Rhythmites are interpreted as varves deposited by the following mechanism: silt deposited during winter when tidal effect is great and clay during the freshet when tidal effect is minimal. Note large vesicles formed during escape of gas (methane?).



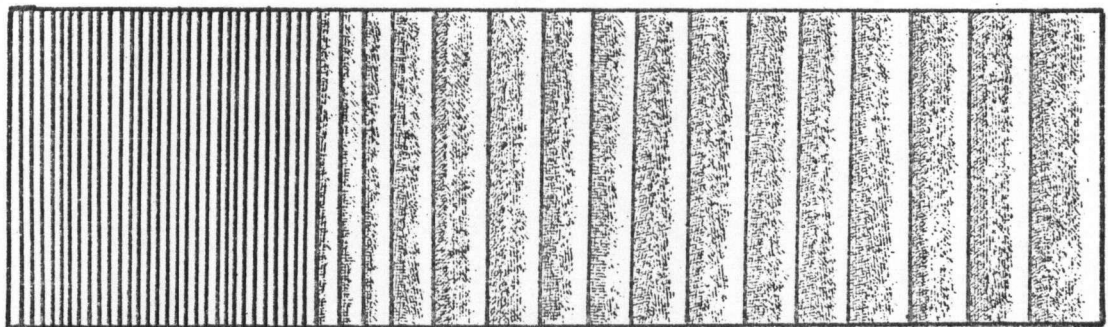
A

B

30 LAYERS

TRANSITION

RHYTHMITES



SILT  
CLAY

mouth to 0.016 cm, 2 km north of the mouth. Clay layers seldom are thicker than 0.016 cm near the delta and thin to an average thickness of 0.008 cm in the lake bottom sediments beyond Goose Island. All cores showed evidence that gas (methane?) had escaped after sampling. Houbolt and Jonker (1968) found gas "pockets" were ubiquitous in Lake Geneva sediments. Cores, cut open soon after sampling, have continuous layering with scattered gas vesicles (Fig. 12). Cores which were stored allowing gas to escape slowly, have streaky, uneven and discontinuous layers with no vesicles.

The best-developed rhythmic layering was found in cores to the west of the main delta lobe. The thickness of the layers was found to decrease abruptly at about 10 cm (or approximately 30 laminations) from the top of the sediment section (Fig. 12). Couplets below the 10 cm level are about 1 cm thick whereas those above are only 0.2 cm thick. The decrease (80%) in thickness occurs gradually over 4 - 6 couplets and suggests a sharp decrease in sediment reaching the site. This can be interpreted as a shift in locus of sedimentation from the west to east side of Goose Island. Another interpretation is that sedimentation has decreased over all the lake, but without rhythmic layering the change is not evident. Since the configuration of the delta has been constant

since at least 1860 (Richards, 1860), the latter explanation is favored.

The rhythmic layering was previously noted by Johnston (1922) in his work on Pitt Lake. His interpretation was that the alternating laminations were tidal in origin. It appears more likely that they are annual layers (varves). The coarse layer (silt and fine sand) is brought in as bed-load and suspended load during winter (November - March) when discharges of Fraser and Pitt systems are low and thus tidal effect is great. The fine layer (mainly clay) is deposited during the rest of the year. Presumably clay ( $9\phi$ ) is supplied to the lake mainly during spring run-off (May - July) and continues to settle during summer and fall. The volume of sediment represented in an average couplet for the entire foreset-bottomset-lake bottom area shown in Figure 3 was calculated to be  $150 \pm 20 \times 10^3$  tonnes. Calculations were based on average thickness of layers near tops of cores and their approximate areal distribution.

### $^{137}\text{Cesium}$ dating

An unexpected "spin-off" of atmospheric nuclear testing (1952 - 1972) is the subsequent use of radioactive isotopes released during the tests (such as  $^{137}\text{Cs}$ ) for dating of recent sediments (Pennington, 1973; Robbins and Edgington, 1975; Ritchie, 1975).  $^{137}\text{Cesium}$  was created during the nuclear testing and disseminated throughout the world by air currents

and rainfall. In fresh water, Cs is preferentially adsorbed, or "fixed", onto the micaceous (illite) component of the sediment (Francis and Brinkley, 1976), presumably trapped along grain (phyllosilicate minerals) boundaries. Once in contact,  $^{137}\text{Cs}$  is firmly attached so that further movement by natural chemical processes is limited (Davis, 1963; Tamura, 1964). Thus, the variation in  $^{137}\text{Cs}$  content present in the stratigraphic column can be compared with the local  $^{137}\text{Cs}$  activity record (usually measured in rainfall or in milk) to determine sedimentation rate.

In order to determine the present annual sedimentation rate on the Pitt tidal delta, 11 large diameter (6.3 cm) cores were taken on the delta topsets and foresets (Fig. 3; Fig. 13). A Kullenberg gravity corer (weighing 130 kg) was dropped from an anchored raft. Core lengths ranged from 15 cm to 85 cm and three cores with undisturbed bedding were chosen for dating (samples # 3, # 8, and # 11). Mean grain size variation of the cores is limited, ranging from coarse silt to very fine sand (50 - 70 $\mu$ ). As  $^{137}\text{Cs}$  is associated with micas or illites and as these minerals most often occur in the finer fractions, total  $^{137}\text{Cs}$  content would be expected to vary with grain size. Thus the homogeneous grain size of the Pitt samples made them particularly appropriate for dating by the  $^{137}\text{Cs}$  dating technique.

### Method

Cores were split horizontally along bedding planes into 1.5 cm thick slices. The samples were then dried, disaggregated by hand and placed in plastic vials. Each sample was analyzed for  $^{137}\text{Cs}$  using a standard detector for gamma ray spectroscopy (Ge(Li) detector) coupled to 1024-channel pulse height analyzer system (Fig. 14). The gamma ray energy of each isotope is unique and the detector converts gamma radiation to a pulse proportional to the energy of ray. This method assures clear separation of the 661 KeV energy of  $^{137}\text{Cs}$  from those of  $^{208}\text{Tl}$  (583 KeV) and  $^{214}\text{Bi}$  (609 KeV). Each sample was counted for 800 minutes, resulting in a detection threshold of 0.1 picocuries per gram of sediment.

### Results

An exceptionally good record (Fig. 15) was found in core # 3 collected off the mouth of the distributary channel in 50 m of water (Fig. 3). Average rate of sediment accumulation at this site from 1954 to 1972 was 1.8 cm/yr (no correction was made for compaction). The fluctuation in  $^{137}\text{Cs}$  content is consistent with that measured in Vancouver (milk) (G.Griffiths, pers. comm. ). Lake stratigraphy from Lake Windermere, England (Pennington, 1973) and fallout



FIGURE 13. Photo of core # 3 (Fig. 3) which was dated by  $^{137}\text{Cs}$ . Note that although the stratification is not rhythmic, it is undisturbed. Core diameter is 6.3 cm.

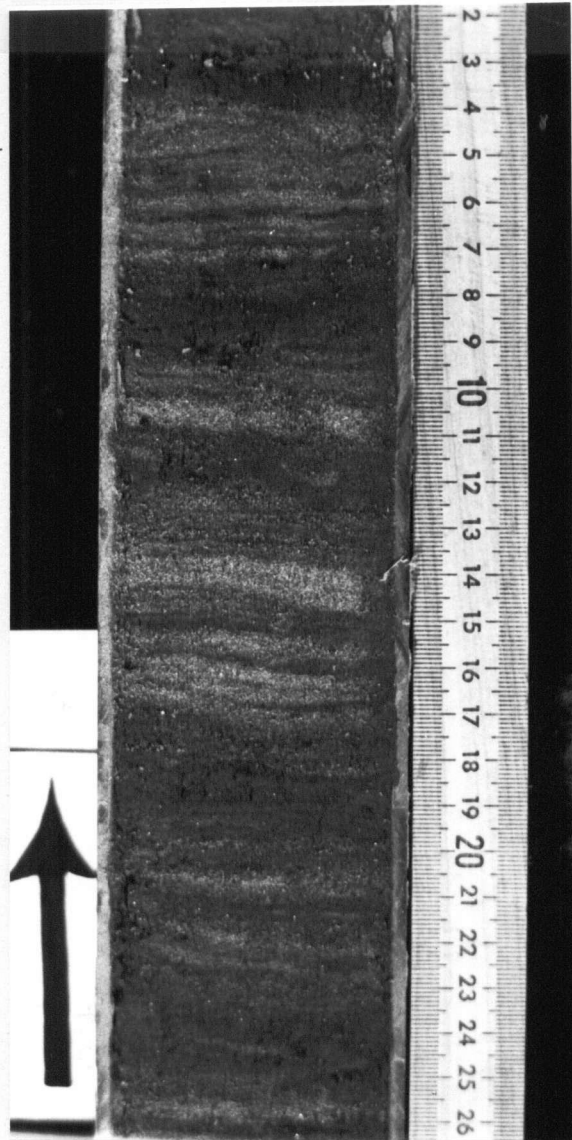


FIGURE 14. Diagram of the system involving gamma ray spectroscopy used in  $^{137}\text{Cs}$  dating. Samples were analyzed with a Ge(Li) detector coupled to 1024 channels of a pulse height system.

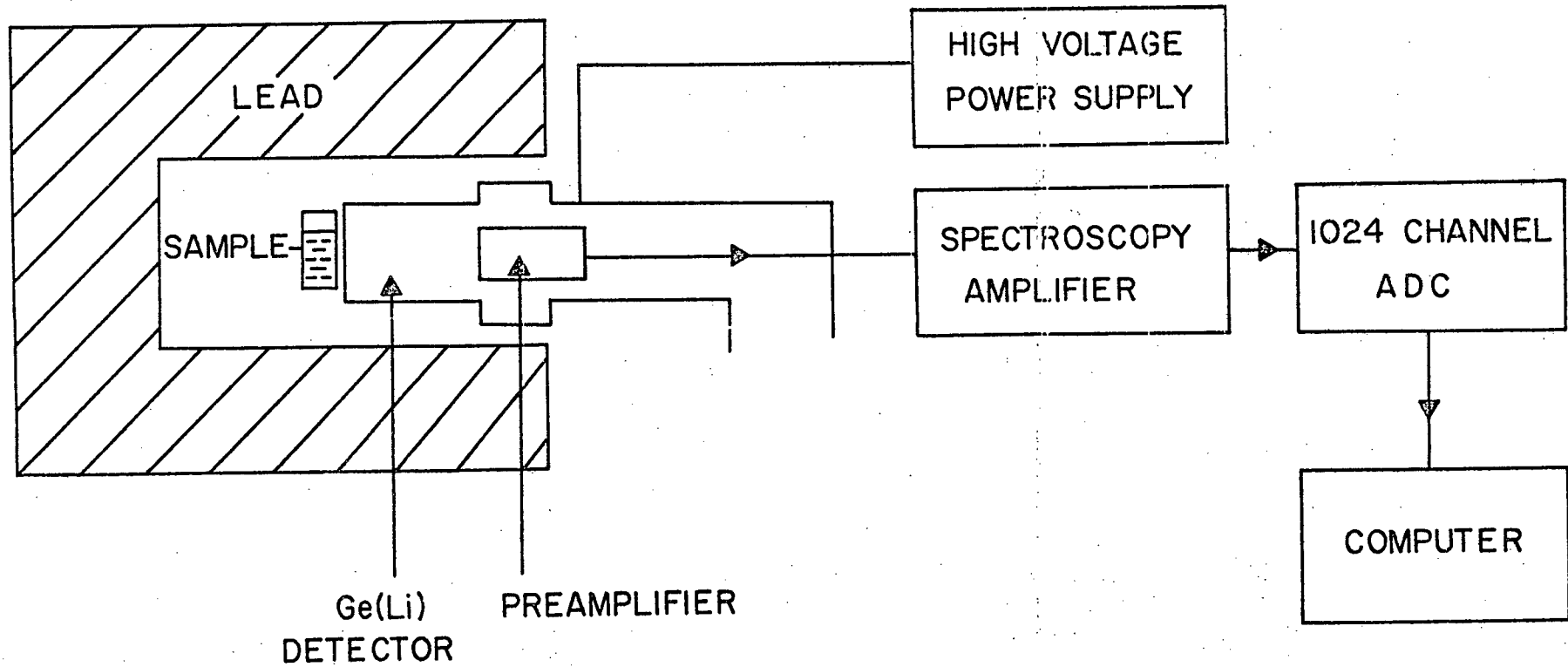
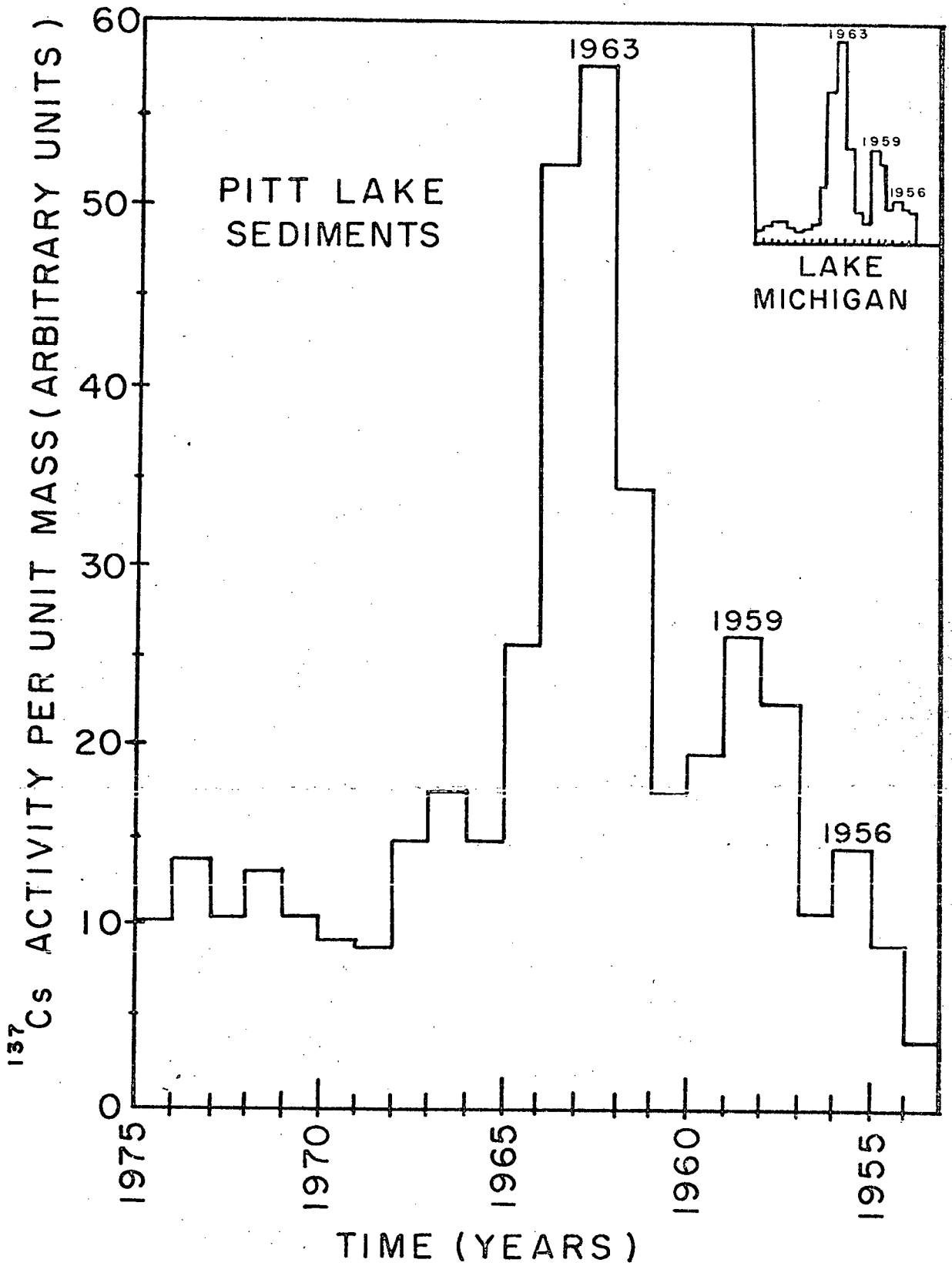


FIGURE 15. Plot of  $^{137}\text{Cs}$  dating results from core # 3 from Pitt Lake delta foresets. Cesium concentration per unit mass plotted against time (depth) results in a graph similar to the estimated annual flux of  $^{137}\text{Cs}$  to surface of Lake Michigan (Robbins and Edgington, 1975) shown in the inset.



recorded in Tallahatchie River watershed (Ritchie, 1973) showed a similar record. All show a minor peak in 1959 and a major one in 1963 with the  $^{137}\text{Cs}$  concentration dropping off to low levels thereafter. Core # 11 showed high levels of  $^{137}\text{Cs}$  equal to core # 3 on the delta front, but in a compressed record indicating a slow sedimentation rate of 3 mm/yr. The source of this cesium is probably slope wash from the nearby shore. However, core # 8 (Fig. 3) contained no excessive  $^{137}\text{Cs}$ , indicating no deposition occurred during the last 25 years at that site on the delta.

The above records are considered indisputable evidence for recent deposition and slow, but regular sedimentation on the delta. In addition, the difference in records from the three sites gives further information on the pattern of present day deposition which is examined in the following section.

#### Grain size analysis

A study of the grain size distribution of Pitt Lake sediments was carried out in order to gain insight into the nature of sedimentary processes active on the delta and lake bottom. Sediment samples were collected with a Dietz-LaFond grab sampler and a Phleger corer. A total of 190 samples were analyzed by one or more of the following analytical methods.

- (1) Rapid Sediment Analyzer (R.S.A.) - settling tube with automatic recording of weight accumulated versus time (Woods Hole Settling Tube, Univ. of R.I.).
- (2) Sieving - standard sieving procedure (Folk, 1968) using sieves with 0.5  $\phi$  interval.
- (3) Quantimet 720 - image analyzing computer (Perrie and Peach, 1973), Brock University.
- (4) Sedigraph 5000 (Micrometrics, Inc.) - particle size analyzer which measures the concentration of particles remaining suspended as a function of settling time using a finely collimated beam of x-rays (Olivier, et al., 1970/71).
- (5) Hydrometer - standard method for grain size analysis of soils (A.S.T.M. D422-63).

The range of sizes over which these methods were used in this study is shown in Figure 16. Weight percent for each 0.5 $\phi$  class was used to compute statistical parameters (using method of moments) and cumulative probability plots.

#### Analysis of polymodal sediments

It became evident during the early stages of grain size analysis that the sediments were polymodal. Bargraphs and cumulative curves (see Appendix) revealed complicated distributions with grain sizes 2  $\phi$ , 4.5  $\phi$ , and 8.5  $\phi$  being the areas of the distributions which consistently showed



irregularities. Attempts were made to resize some sediments by methods (Fig. 16) that would analyze across "problem" areas with a single method. The 4.5  $\phi$  size which is near the normal break between mechanical (sieve) and settling (hydrometer or pipette) sizing techniques needed particular attention and was examined by two additional methods.

As the interpretation of polymodal sediments is a controversial subject, a brief introduction to the problem will provide a background on which to present the results of this study.

#### Introduction

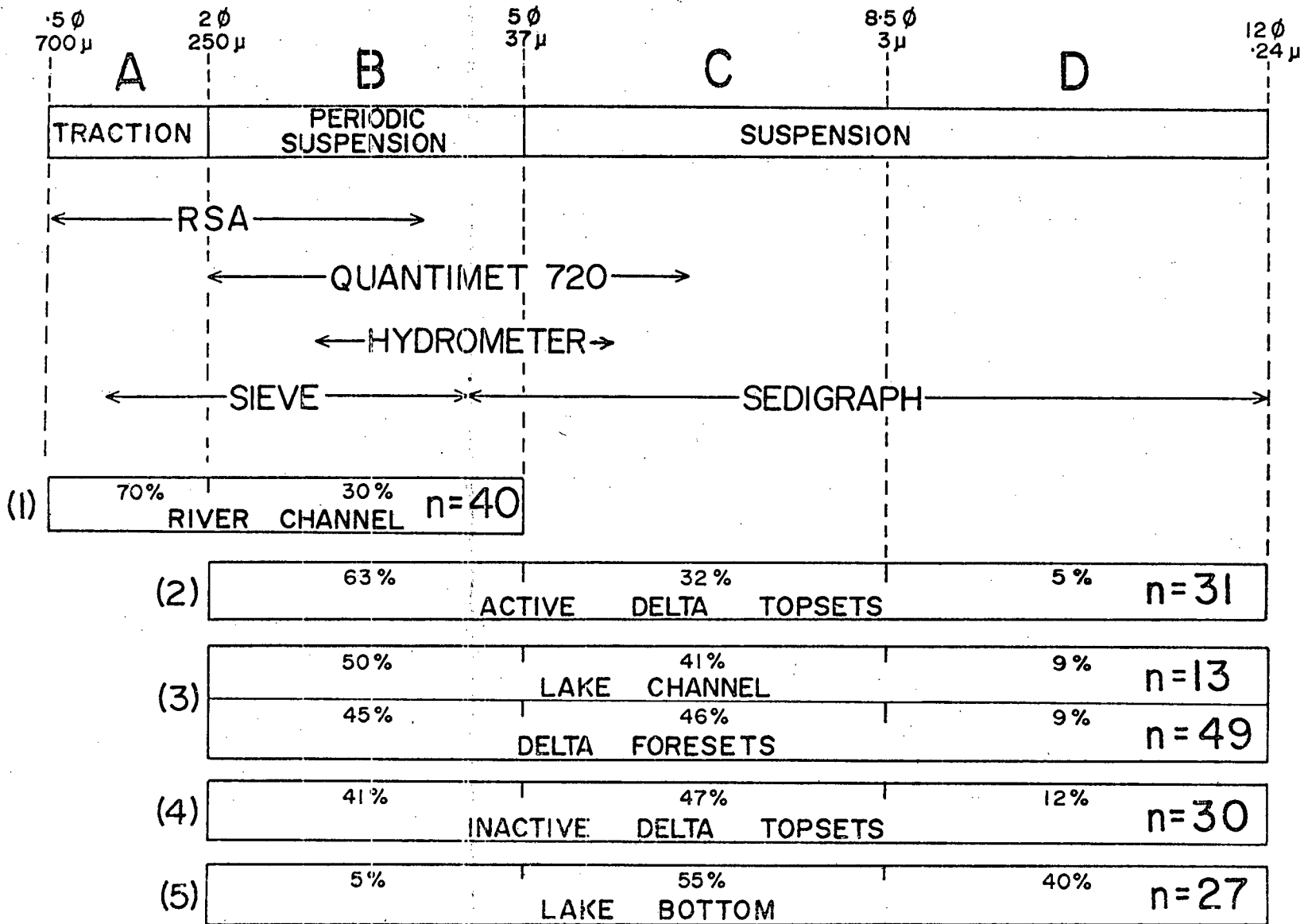
During the last two decades there have been significant advances in environmental interpretation of grain size analysis. Syndowski (1957) attempted to relate a particular cumulative log probability curve shape to a specific environment. At the same time Folk and Ward (1957) quantified curve interpretation by utilizing statistical parameters to characterize the curve and bivariate plots of statistical measures to distinguish environments. Because most sediments are polymodal, curve shape and statistical measures (such as skewness and kurtosis) simply reflect the relative magnitude and separation of modes. Although this problem was recognized early (Folk and Robles, 1964), the use of statistical parameters on polymodal sediments has

persisted (Duane, 1964; Martins, 1965; Friedman, 1967; Moiola and Weiser, 1968).

An alternative approach to the problem is to separate the constituent populations (modes) and to relate these to sedimentary processes and ultimately to an environment of deposition. Visher (1969) and Middleton (1976) have both separated subpopulations at breaks between fitted straight line segments of cumulative probability plots. However, this method makes the unlikely assumption that all the subpopulations are truncated distributions. Fuller (1962) and Spencer (1963) have separated overlapping modes by partitioning cumulative probability curves following the graphical method of Harding (1949). This technique is simple and shows the most promise in being able to break the sum into meaningful parts without the tedious calculations involved in the numerical methods (Clark, 1976).

Any attempts to relate grain size distributions to specific sedimentary environments should be based on a clear understanding of the polymodal distribution, in particular, the size distribution and proportions of the individual subpopulations. The proportions of modes between environments should reflect different sediment transport processes or at least varying intensity of these processes. Secondly, the effect of variability (grain size, mineralogy, etc.) of the sediment source material should be considered in the interpretation.

FIGURE 16. The range of grain sizes covered by the five sizing techniques used in this study. The percentage of each mode for each environment is summarized. 'n' is the number of samples used in each summary.



Five environments in the Pitt system have been delineated on the basis of the morphology as determined by air photo interpretation and bathymetry (Fig. 17). River channel, lake channel, inactive delta topsets, active topsets, delta front, and lake bottom can each be characterized by water depth, flow type (unidirectional or bidirectional), average velocity, and presence of macrophytes.

The analysis of polymodal sediments is based on 190 samples (160 stations) collected from the five environments. The purpose of this study is to partition representative samples using Harding's (1949) method and to interpret the significance of the resultant subpopulations in terms of hydraulic conditions of sedimentation.

#### Statistical method

There are three basic approaches to partitioning polymodal probability curves: analytical, numerical, and graphical (Clark, 1976). The analytical method is not practical for sediments as, at present, there are no solutions for a case with three components. A numerical method for trimodal populations has recently become available (Clark, 1970 in Clark, 1976); however, the procedure is relatively complex and access to an "on line" computing facility is desirable. Generally, the numerical method involves an iterative scheme where initial estimates of the

component parameters are improved, according to least squares criteria.

Harding's (1949) graphical method, which has been extensively used in exploration geochemistry, has been reviewed by Sinclair (1974, 1976). It provides a straightforward approach to partitioning distributions with up to four modes; however, the technique is subjective and may not always yield a unique solution for the curve being analyzed.

Briefly, Harding's method assumes that subpopulations (A,B,C,) composing a trimodal curve have lognormal distributions. Positive inflection points on the curve indicate the approximate proportions of, or the fraction (f) of, the total mixture that each mode comprises (Fig. 18). The cumulative probability of the modal mixture  $P_M$  at any point on the curve is equal to the sum of the products of the fraction,  $f_{A,B,C}$ , of each component in the mixture and the cumulative probability of each component,  $P_{A,B,C}$ :

$$P_M = P_A f_A + P_B f_B + P_C f_C \quad (1)$$

Using the point on the curve PL22A at  $6 \phi$  (Fig. 19F) as an example:

$$P_M = (98.7\%) (.24) + (42\%) (.46) + (1\%) (.3)$$

$$P_M = 43.01\%$$

FIGURE 17. Map of depositional environments with  
the Pitt system.

# PITT SYSTEM DEPOSITIONAL ENVIRONMENTS

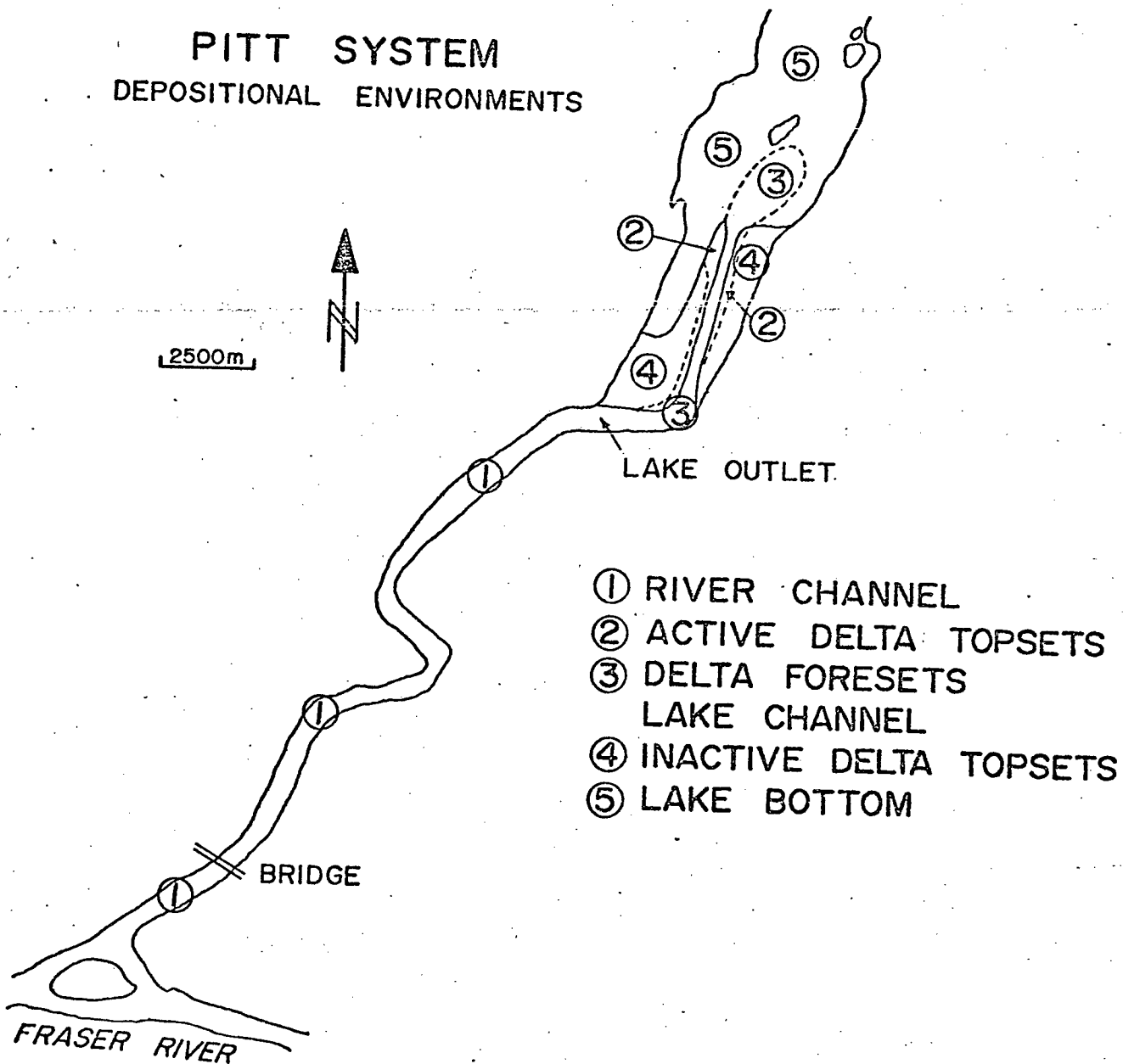




FIGURE 18. Bimodal and trimodal cumulative probability plots are constructed from equal proportions of two and three (respectively) lognormal populations (after Sinclair, 1976, Fig. VI - I).

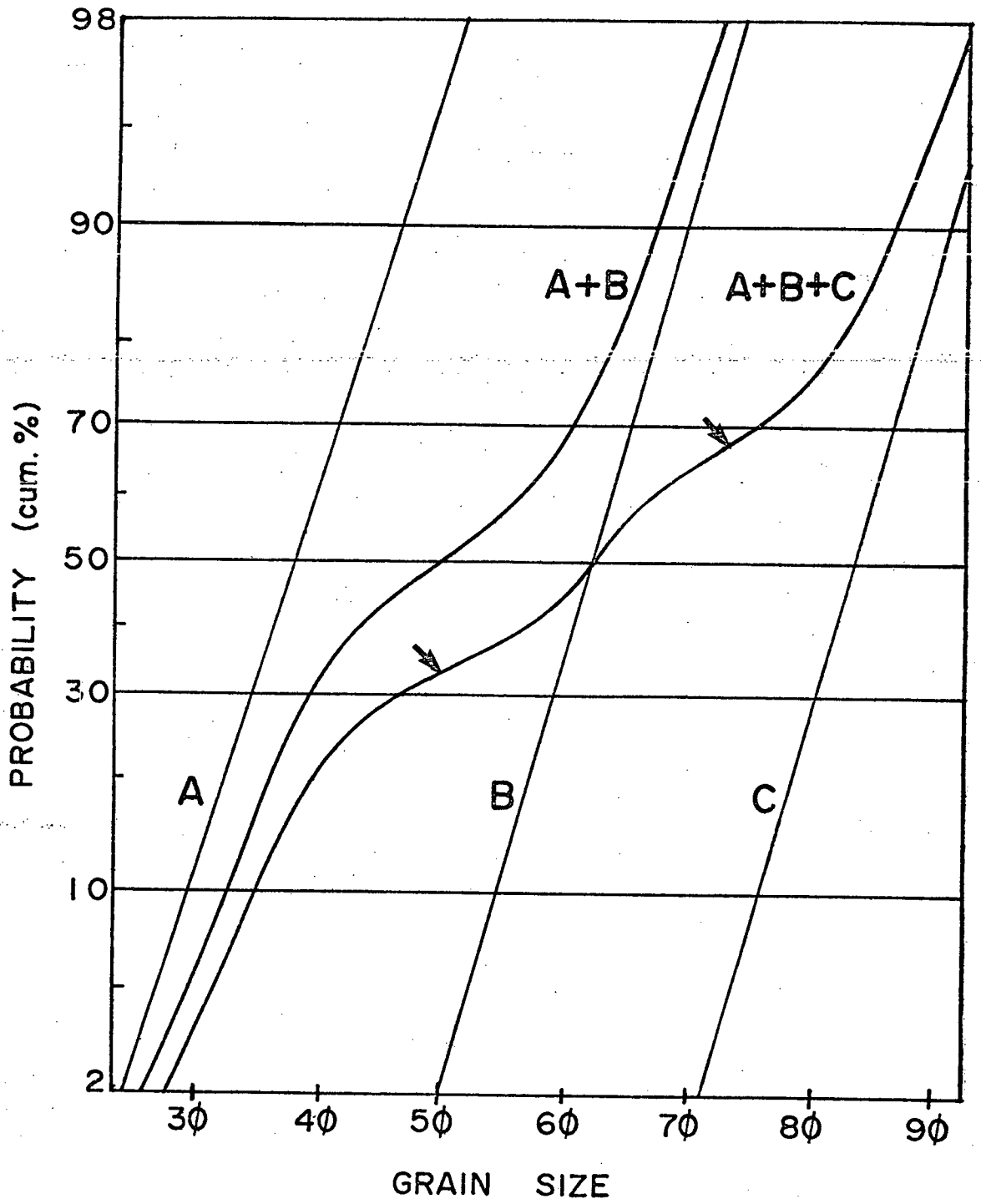
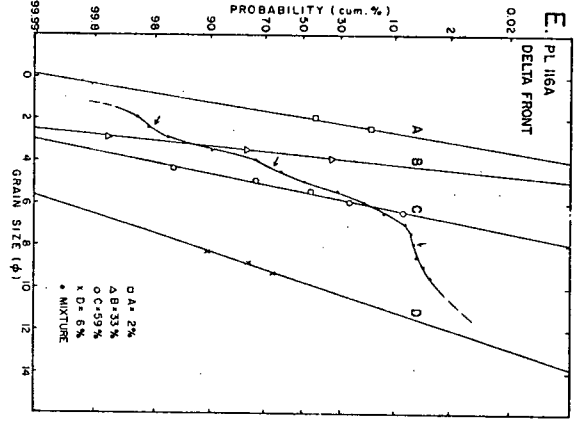
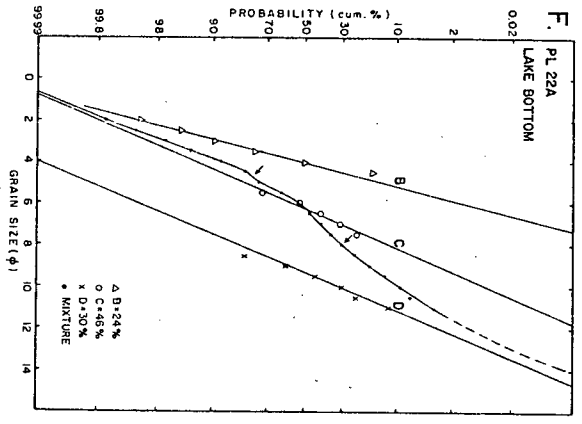
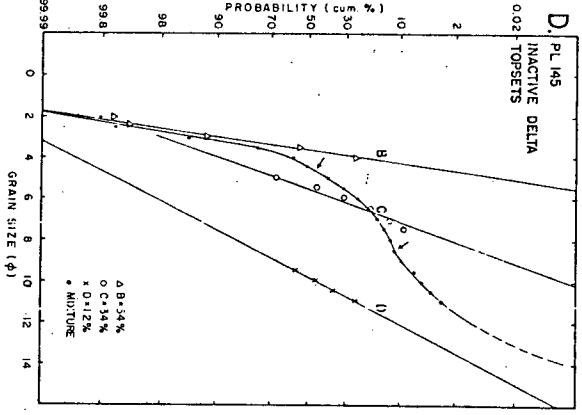
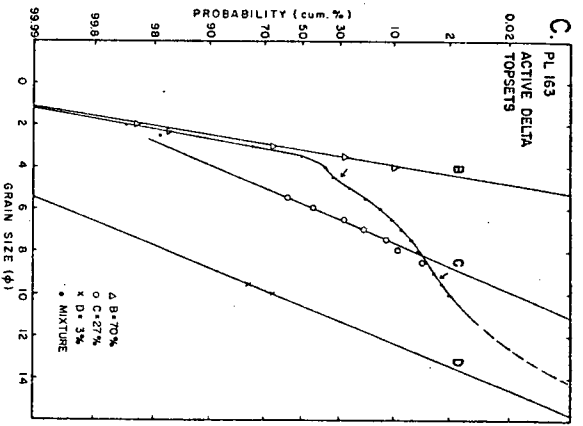
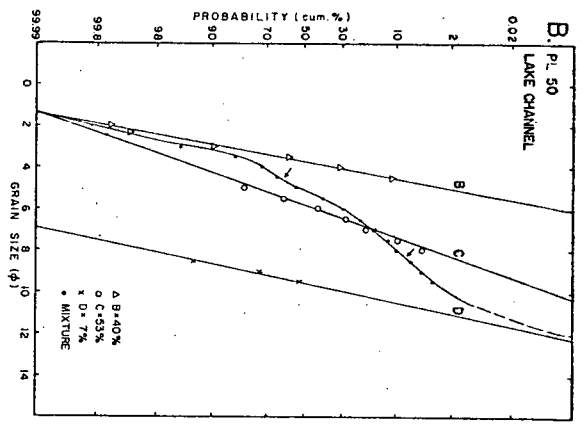
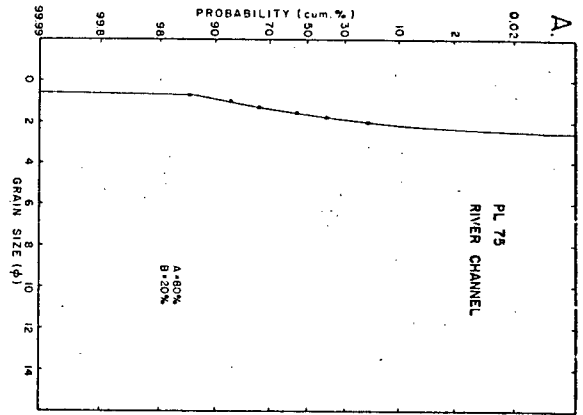


FIGURE 19. A polymodal cumulative probability curve from each of the five environments is shown with the lognormal subpopulations derived by partitioning from the curve. Examples from both the lake channel and the delta front are shown for environment (3). Arrows mark inflection points on the curves and are assumed to be points of modal overlap.



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A sampling of cumulative probability plots from the Pitt system (Fig. 19) shows positively skewed curves with irregularities at  $2\phi$ ,  $5\phi$ , and  $8.5\phi$ . Their shape is, in general, similar to that of the curve constructed from equal proportions of three lognormal populations (Sinclair, 1976) (Fig. 18). Thus, an effort was made to partition a number of curves into subpopulations. Almost all modes define a straight line on arithmetic probability paper inferring that each mode has a lognormal distribution. Note in Figure 16 the progressive changes from environment (1) through (5) in the proportion of modes. A and B proportions decrease with a corresponding increase in C and D. The five environments were originally defined on morphology, but are substantiated by the grain-size distribution study as each shows unique proportions of the four modes. Twenty probability plots were partitioned and the average of the medians ( $M_D$ ) and the average of the standard deviations ( $\sigma$ ) of each individual mode are summarized in Table V. The four modes and the inflection points where they overlap are shown schematically in Figure 20.

FIGURE 20. A schematic diagram showing standard deviation and median of the four modes. Arrows mark modal overlap and are coincident with the inflection points on curves (Fig. 18). Modal proportions for this particular example are:  
A - 7%; B = 33%, C = 50%, and D = 10%.

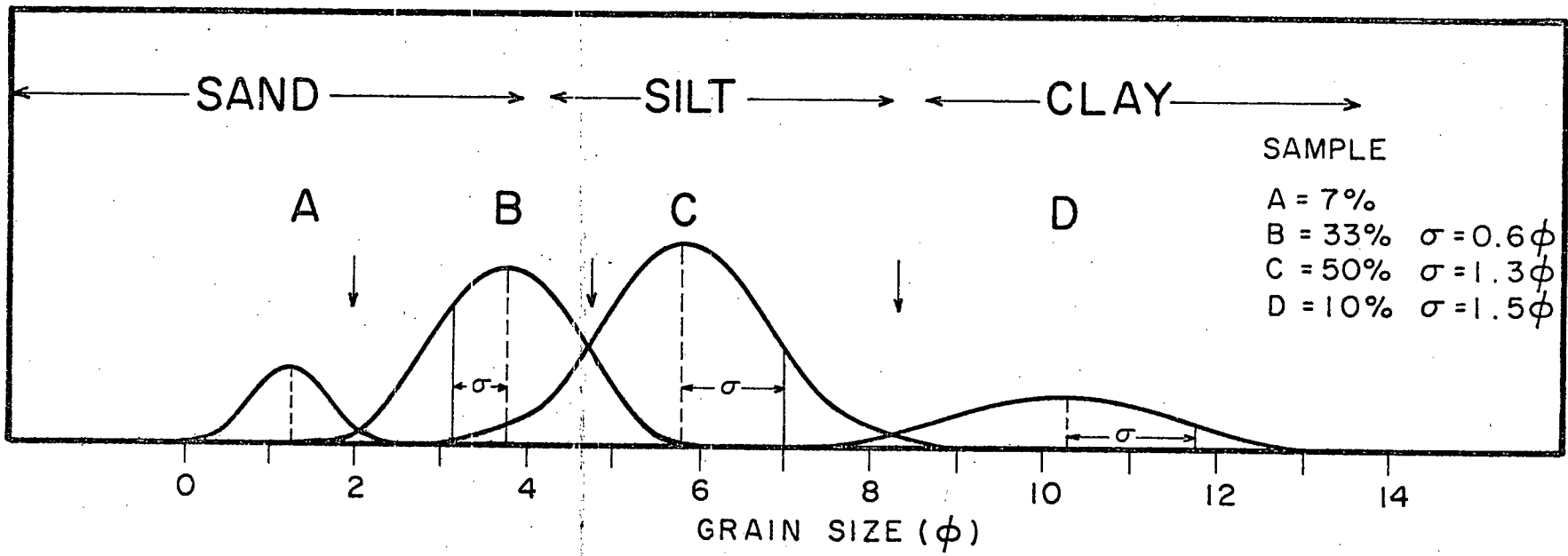




TABLE V Summary of modal statistics.

Mode	Avg. $M_D$	$\sigma$ Avg.	Range of $M_D$
A	1.2 $\phi$		
B	3.8 $\phi$	0.6 $\phi$	3.3 $\phi$ - 4.4 $\phi$
C	5.8 $\phi$	1.3 $\phi$	5.2 $\phi$ - 6.3 $\phi$
D	10.3 $\phi$	1.5 $\phi$	8.6 $\phi$ - 10.9 $\phi$

## SEDIMENTOLOGICAL PROCESSES

Sediment mixing

Grain size analysis and subsequent partitioning of the cumulative probability curves revealed four distinct populations that were either mixed prior to deposition, or during deposition. The technique of partitioning allows "unmixing" and provides an opportunity to examine each population by itself in order to gain further insight into their origin.

2  $\phi$  inflection

Most Pitt River sediments show an inflection near 2  $\phi$ . However Rapid Sediment Analyzer results are insensitive to small concentrations (in the tails of distribution curves) and resulting plots were not appropriate for partitioning. Few grains coarser than 2  $\phi$  are found within the delta or lake environments. Thus, the 2  $\phi$  inflection is interpreted to represent the division between the coarser grain sizes carried mainly by traction (population A) and fine-grained material (population B) moved mainly by periodic or intermittent suspension. Einstein et al. (1940) recognized a similar boundary at 1.5  $\phi$  and Fuller (1961) interpreted a curve irregularity at 2  $\phi$  as the grain size which separates grains affected by Impact Law and Stokes Law. A recent

paper by Middleton (1976) relates the grain size at the traction-intermittant suspension truncation point on cumulative probability plots to the hydraulics of flow. He theorized that the shear velocity of flow,  $V_*$ , should be greater than or equal to the fall velocity of the grain,  $w$ , at the truncation point described above. This idea was substantiated with data from Pitt River (Table VI).

#### 5 $\phi$ inflection

This inflection point could be interpreted as overlapping modes resulting from: (1) two distinct processes - periodic suspension (population B) and continuous suspension (population C); or (2) a single process, suspension, operating under the distinctly different summer and winter hydraulic conditions existing in the Pitt system.

Flume studies of suspension transport (Sengupta, 1975) are technically difficult and have been limited in scope. Sengupta's results are ambiguous in that, depending on flow conditions, either a single mode or a bimodal grain size distribution was found in the suspended material. Attempts at grain size analysis of natural suspended populations are hindered by the problems of low concentrations necessitating very large samples.

Available data (Visher and Howard, 1974) suggests that natural suspended material is polymodal. Milliman (pers. comm. 1976) noted in his work on suspended sediments of

TABLE VI Pitt data applied to Middleton's (1976) shear velocity - settling velocity relationship.

$$U_* = gds$$

(DuBoys Formula)

$$\frac{\omega}{U_*} < 1 \quad (\text{Middleton's criteria})$$

$$\frac{3 \text{ cm/sec}}{6.2 \text{ cm/sec}} < 1$$

$U_*$  = shear velocity

$\omega$  = settling velocity

$g$  = acceleration of gravity

$s$  = slope

$d$  = depth

$g$  = 980 cm/sec<sup>2</sup>

$s$  = .000053 (max. flood slope)

$d$  = 963 cm (ave. depth)

$\omega$  of 2 $\phi$  (.25 mm) = 3 cm/sec

$\omega$  **determined** from Blatt et al. (1972, Fig 3-12)

Reference: Blatt, H.; Middleton, G.; and Murray, R. 1972, Origin of Sedimentary Rocks: Prentice Hall, Inc., Englewood Cliffs, New Jersey.

Fraser River that the fine silt and clay concentration remained fairly constant throughout the year irrespective of discharge. This fine material can be referred to as continuous suspension or wash load. He also found that sand and coarse silt concentrations fluctuated directly with change in velocity. Data published annually by the Water Survey of Canada gives grain size distribution of the suspended sediment in whole  $\phi$  class intervals. Analysis was carried out to 9  $\phi$  only and thus there is not enough detail to determine bimodality. Evidence presented in this study of the Pitt system shows a consistent change in the proportion of populations B and C with sedimentary environment. This change is best explained by (1) above, the existence of two distinct suspension processes (periodic and continuous). Field studies clearly documenting the existence of two suspension processes are rare and the problem requires further study.

#### 8.5 $\phi$ inflection

This inflection point occurs near the silt-clay boundary and is probably a grain shape effect. Silt grains are more or less equant in shape whereas clay size particles tend to be more platy and may settle more slowly than expected by Stokes Law. Pharo (1972) found a similar curve inflection in plots of grain size distributions of Strait of Georgia sediment.

Flocculation is not thought to be significant as water is fresh and clay size minerals are predominantly chlorite. It is suspected that all grains finer than  $5 \phi$  are carried mainly by suspension, however the mechanisms creating the two populations need further examination.

### Conclusions

Cumulative probability curves of grain size data from the Pitt system can be partitioned into subpopulations which plot as straight lines on lognormal probability paper. These lognormal distributions are interpreted as populations produced by different methods of sediment transport in the river, delta, and lake environments: traction mode ( $0.5 \phi - 2 \phi$ ), periodic suspension ( $2 \phi - 5 \phi$ ), continuous suspension, silt ( $5 \phi - 8.5 \phi$ ), and continuous suspension, clay ( $8.5 \phi - 14 \phi$ ).

Each environment within the system is composed of a unique combination of proportions of the modes. As the source of sediment (Fraser River) is the same for all environments the difference in the proportions of modes between environments is a reflection of the relative importance of various processes acting within each environment.

### Grain size distribution

Figure 11 depicts with size contours (C.I. =  $0.5 \phi$ ) the aerial distribution of mean grain size of each grab sample

and sample from the top of each core. Mean grain size is fine (5.5  $\phi$ ) in the deep areas of the channel at the outlet and right-angle bend, with coarser (2  $\phi$  - 4  $\phi$ ) material in between. The rest of the channel distributary out to the delta tongue is coarse silt with a mean grain size of 5  $\phi$  (.03 mm).

In general, mean grain size contours follow the channel, diverging near the end, mimicking the flood flow pattern (Fig. 8A). The one exception to this generality, the triangle of coarser sediment in the middle of the southern topsets, is probably a result of removal of some fines during ebb flow. Ebb drainage channels on the southern margin of this area (Fig. 3; Fig. 4A) indicate that ebb-oriented flow has a pronounced effect on this portion of the delta. The coarsest sediment, with a mean grain size of 0.044 mm (4.5  $\phi$ ) to 0.075 mm (3.7  $\phi$ ), is found at the northern top end of the delta topsets immediately adjacent to the channel. As this material is slightly coarser than that in the channel from which it originated, winnowing is suspected.

Subsamples were taken from top, the middle, and bottom of 15 cores from the foresets and bottomsets to determine any vertical change in grain size within the couple hundred years of sedimentation present. Cores within 0.5 km of the end of the distributary channel show increasing grain size from bottom to top of core. Cores 0.5 km to 7 km

(farthest removed sample) away from the channel show a slight upward decrease in grain size (generally less than  $0.5\phi$ ). The implication from these changes in grain size stratigraphically is that the delta is prograding, but at a lesser rate than in the past.

On the delta foresets and bottomsets, mean grain size becomes finer away from the end of the distributary channel and the contour pattern indicates sedimentation occurs mainly to the east side of Goose Island. The distribution pattern depicted in Figure 11 is a reasonably good example of sedimentation by diffusion from a simple jet with little if any reworking by waves and tidal currents.

The application of the theory of submerged free jets to delta formation has been strongly influenced by the work of Bates (1953). He believed that the diffusion pattern depends on the relative densities of the two fluids (moving and stationary bodies of water). However, one of the major limitations of Bates' theory is the assumption that there are no boundary effects. Clearly, the basic assumptions for any theoretical model of sediment diffusion by jet flow (delta formation) should directly reflect the complexities of the natural environment and not an ideal situation.

A recent laboratory and computer model study by Ramsayer (1974) incorporated the effect of lateral and basal shear on jet flow under steady uniform flow. He explains morphological features such as levees and distributary



bars found at a delta distributary mouth by a model which predicts the distribution of effective bed shear stress. Time dependent runs using fine sand produced a sediment distribution pattern strikingly similar to that of the Pitt (Fig. 11). Thus, the Pitt appears to fit the general model of deposition from a jet. However, one feature of the model that is missing in the Pitt, is the distributary mouth bar. Jopling (1960), suggests that if the frontal slope over which the flow expands is less than  $10^\circ$ , the flow will not separate from the boundary at all (assuming the flow is homopycnal) and thus deposition in the form of a bar would not occur. This seems to explain the lack of bar development on the Pitt delta as the foreset slope is less than  $4^\circ$  and the system possesses homopycnal flow for most of the year.

In conclusion, the areal distribution of mean grain size substantiates the interpretation that flood flow is the dominant current in moving sediment across the delta. Sediment is then dispersed by jet flow oriented in a north-east direction into the lake.

#### Sediment dispersal and accumulation

The observations of delta morphology, the presence of bedforms in the channel, and the distribution (pattern) of grain size enable the processes involved in sediment dispersal to be delineated.

The single distributary channel, flanked by levees, which leads to a fan-shaped delta foreset indicates that the channel is the avenue for sediment movement. The fact that the channel is deeply incised along the southern margin and that the carbon-dated material ( $4.645 \pm 95$  B.P.) from the southern topsets was buried by only 60 cm of sediment suggests that the flow is channelized in this reach and little sediment is brought up onto the delta surface. Velocity data and orientation of large-scale bedforms reflect the dominance of the flood current moving through the channel.

North of the right-angle bend the distributary shallows and channel banks become less steep. Small flood-oriented sand waves (10 m in spacing) are found in the channel for the first 2 - 3 km where flow is more-or-less confined. However, in the last 3 km, only ripples are found on the channel bottom and channel bank slopes are low enough for flow to spill and spread over the topsets. Mean grain size distribution reflects this pattern of flow. Once sediment is on the delta surface it is winnowed and moved by wave-driven currents in addition to the tidal currents. Large waves and swells were observed to occur frequently in the lake, particularly during the winter months, shifting sediment in the form of ripples. Orientation of these ripples, which cover the outer topsets, reflects the

direction of currents at the time. Wind-generated currents were observed to incorporate and carry sediment into the lake as a plume.

No attempt was made to study mechanics of sediment dispersal from the end of distributary out into the lake. However, as medium silt is found as far out as 5 km, some type of density flow mechanism is probable for at least part of the year.

Stratigraphic data presented previously suggests that a total volume of  $(150 \pm 20 \times 10^3)$  tonnes of sediment is accumulating annually in the southern half of Pitt Lake.  $^{137}\text{Cs}$  dating has confirmed the existence of a steady sediment flux since at least 1954. 50% of the annual sediment accumulation is coarser than  $5 \phi$  and thus probably moves in the form of bedload and periodic suspension. This volume ( $75 \times 10^3$  tonnes) is on the same order of magnitude as the annual sediment flux calculated for the Pitt River (South) by Ashley (1977). It is suspected that the other 50% consists of: (1) material that is continually reentrained at points along the river and delta channels by flood flows and eventually arrives at the lake; and (2) fine silt and clay that is washed in from the Pitt watershed.  $^{137}\text{Cs}$  dating substantiates, first, the interpretation of the foreset rhythmites as annual couplets (varves) and, second, that the sedimentation rate on delta topsets is minor.

The possibility of a sharp decrease in sedimentation rate approximately 30 years ago is suggested by the stratigraphy (Fig. 12). Most cores taken away from the active delta channel show a decrease in grain size upsection indicating a slight waning in delta growth rate. Although definitive evidence is lacking, this apparent decrease in sedimentation rate is intriguingly coincident with the initiation of large-scale dredging in lower Fraser River. This dredging probably has had the effect of increasing the cross-sectional area of Fraser estuary and thus decreasing the magnitude (and thus competency) of tidally induced currents in Pitt River.

## CONCLUSIONS

The Pitt tidal delta is presently building into the lower end of Pitt lake. Its unusual position can be readily explained in terms of tidal dynamics. Unequal velocities of tidal currents (flood is greater) have caused landward transport of sediment up Pitt River (South) from the Fraser and into the lake. A complex interaction of Fraser discharge, Pitt basin drainage, and the tidal prism creates unequal tidal flow on a seasonal basis (winter has strongest flows).

Both the geomorphology and grain size distribution reflect the dominant flood flow pattern. Basically flow is channelized as it enters the lake and remains in the channel until its bank slopes are shallow enough to allow overflow onto delta topsets. Annually  $150 \pm 20 \times 10^3$  tonnes of sediment (1% of Fraser's total load; Mathews et al., 1970) are being deposited as varved couplets. The greatest thickness is on delta foresets in the vicinity of the main channel, with the best developed stratigraphy occurring adjacent to the delta lobe. These varved couplets are unusual in that the coarser silty layer forms during the winter and the clay layer during the summer, reflecting seasonal changes in the strength of tidal currents.

The present-day delta has been constructed during the last 6000 years at an average rate of  $1.28 \text{ m} \cdot \text{yr}^{-1}$ ; however, delta growth would be expected to have decreased exponentially.  $^{137}\text{Cs}$  dating and varve chronology suggest that the present growth rate is on the order of centimeters per year. A slight decrease in mean grain size upsection in cores (representing a couple hundred years sedimentation) also suggests a waning delta growth. Varve stratigraphy has revealed a sharp decrease in sedimentation rate 30 years before present. This decrease may be a response to large-scale dredging in the lower Fraser estuary.

Despite bidirectional flow and daily and seasonal fluctuations in lake stage, the delta has a simple constructional morphology. The morphology, the sand waves in channel, and sediment dispersal pattern are dominated by flood conditions. Weaker ebb currents make only minor modifications despite the average discharge of  $1700 \text{ m}^3 \cdot \text{sec}^{-1}$  which drains daily from the lake.

## REFERENCES CITED

- Ashley, G.M., 1977, Sedimentology of a tidal river, Pitt River, B.C.: (Ph.D. thesis), Univ. of B.C., Vancouver, B.C., Canada.
- A.S.T.M., 1963, Standard method for grain size analysis of soils: A.S.T.M. D422-63.
- Bates, C.C., 1953, Rational theory of delta formation: Am. Assoc. Pet. Geologists, v. 37, no. 9, p. 2119-2162.
- Briggs, L.I. and Middleton, G.V., 1965, Hydromechanical principles of sediment structure formation: S.E.P.M., Spec. Pub. 12, p. 5-16.
- Clark, I., 1970, IONA, a program for the resolution of a mixture of three normal distributions by the method of maximum likelihood: unpublished manuscript, Reading, 12p.
- Clark, M.W., 1976, Statistical analysis of multimodal distributions: Jour. Math. Geology, v. 8, p. 267-282.
- Davis, J.J., 1963, Cesium and its relationship to potassium in ecology: in Schultz, V., and Klements, A.W. Jr., (eds.), Radioecology Reinhold New York, p. 539-556.
- Duane, D.B., 1964, Significance of skewness in recent sediments, Western Pamlico Sound, N.C.: Jour. Sed. Petrology, v. 34, p. 864-874.
- Dyck, W., Fyles, J.G., and Blake, W. Jr., 1965, Geol. Sur. Canada Radiocarbon Dates IV: Radiocarbon, v. 7, p. 24-46.
- Einstein, H.A., Anderson, A.G., and Johnson, J.W., 1940, A distinction between bed-load and suspended load in natural streams: Am. Geophys. Union Trans., p. 628-633.
- Folk, R.F., 1968, Petrology of Sedimentary Rocks: Univ. of Texas, Hemphills, Austin, Texas.
- \_\_\_\_\_, and Robles, R., 1964, Carbonate sands of Isla Perex, Alacran Reef Complex: Jour. Geology, v. 72, p. 255-292.

- Folk, R.F. and Ward, W.C., 1957, Brazos River bar, a study in the significance of grain-size parameters: Jour. Sed. Petrology, v. 27, p. 3-26.
- Francis, C.W., and Brinkley, F.S., 1976, Preferential adsorption of  $^{137}\text{Cs}$  to micaceous minerals in contaminated fresh water sediment: Nature, v. 260, p. 511-513.
- Friedman, G.M., 1967, Dynamic processes and statistical parameters compared for size frequency distributions of beach and river sands: Jour. Sed. Petrology, v. 37, p. 327-354.
- Fuller, A.O., 1961, Size distribution characteristics of shallow marine sands from Cape of Good Hope, South Africa: Jour. Sed. Petrology, v. 31, p. 256-261.
- \_\_\_\_\_, 1962, Systematic fractionation of sand in the shallow marine and beach environment off the South African coast: Jour. Sed. Petrology, v. 32, p. 602-606.
- Harding, J.P., 1949, The use of probability paper for the graphical analysis of polymodal frequency distributions: Jour. Marine Biol. Assoc. U.K., v. 28, p. 141.
- Houbolt, J.J.H.C. and Jonker, J.B.M., 1968, Recent sediments in the eastern part of the Lake of Geneva (Lac Lemane): Geol. Mijnbouw, v. 47, p. 131-148.
- Inman, D.L., 1963, in Shephard, F.P. (ed.), Submarine Geology, Harper and Row, New York, N.Y., 557p.
- Johnston, W.A., 1922, The character of the stratification of the sediments in the recent delta of Fraser River, British Columbia, Canada: Jour. Geology, v. 30, no. 2, p. 115-129.
- Jopling, A.V., 1960, An experimental study on the mechanics of bedding: (Ph.D. thesis) Harvard University, Cambridge, Massachusetts.
- Martins, L.R., 1965, Significance of skewness and kurtosis in environmental interpretation: Jour. Sed. Petrology, v. 35, p. 778-770.
- Mathewes, R., 1973, A palynological study of postglacial vegetation changes in the University Research Forest, southwestern British Columbia: Canadian Jour. of Botany, v. 51, no. 11, p. 2085-2103.

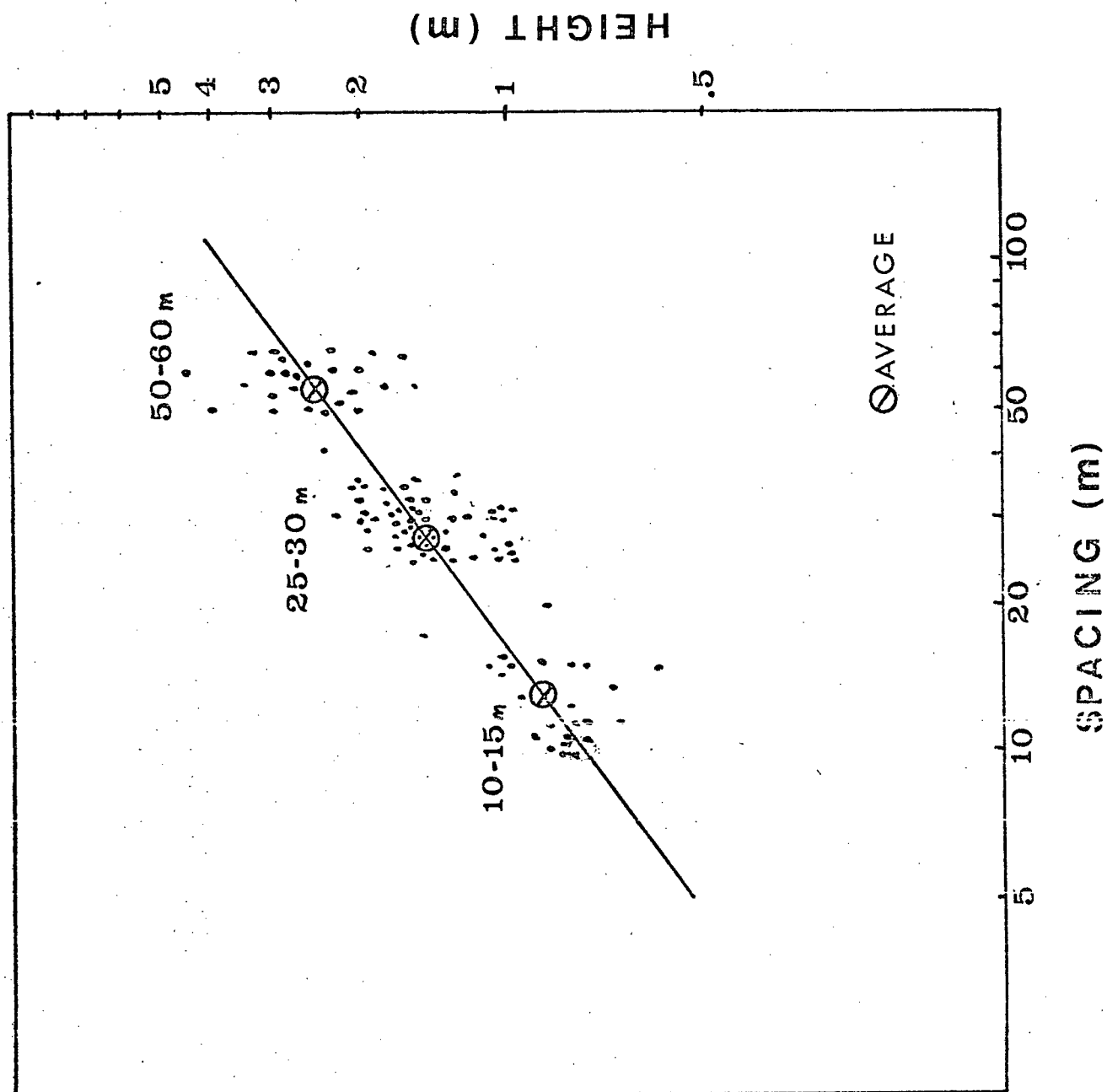


- Mathews, W.H., Fyles, J.G., and Nasmith, H.W., 1970, Post-glacial crustal movements in southwestern British Columbia and adjacent Washington State: Canadian Jour. of Earth Sci., v. 7, no. 2, p. 690-702.
- Matthes, G.H., 1947, Macroturbulence in natural stream flow: Am. Geophys. Union Trans., v. 28, p. 255-262.
- Middleton, G.V., 1976, Hydraulic interpretation of sand size distribution: Jour. Geology, v. 84, p. 405-426.
- Milliman, J.D., 1977, Sedimentation in the Fraser River and its estuary: manuscript in preparation.
- Moiola, R.J. and Weiser, D., 1968, Textural parameters: an evaluation: Jour. Sed. Petrology, v. 38, p. 45-53.
- Olivier, J.P., Hicken, G.K., and Orr, C. Jr., 1970/71, Automatic particle size analysis in subsieve range: Pow. Technology, v. 4, p. 257-263.
- Peacock, M.A., 1935, Fiord-land of British Columbia: Geol. Soc. America Bull., v. 46, p. 633-696.
- Pennington, W., Cambray, R.S., Fisher, E.M., 1973, Observations on lake sediments using fallout  $^{137}\text{Cs}$  as a tracer: Nature, v. 242, p. 324-326.
- Perrie, L.A. and Peach, P.A., 1973, Gelatin coated microscope slides in sedimentary size analysis: Jour. Sed. Petrology, v. 43, p. 1174-1175.
- Pharo, C.H., 1972, Sediments of the central and southern Strait of Georgia, British Columbia: Ph.D. thesis, Univ. of British Columbia, Vancouver, B.C. Canada, 290 p.
- Ramsayer, G.R., 1975, Experimental and theoretical study of deltaic sedimentation: (Ph.D. thesis), the Univ. of Rochester, Rochester, New York.
- Reineck, H.E. and Singh, I.B., 1975, Deposition Sedimentary Environments: Springer-Verlag, New York, 438 p.
- Richards, G.H., 1860, Fraser River and Burrard Inlet: British Admiralty Chart, 1922.
- Ritchie, J.C., McHenry, J.R., and Gill, A.C., 1973, Dating recent reservoir sediments: Limnology and Oceanography, v. 18, p. 254-263.

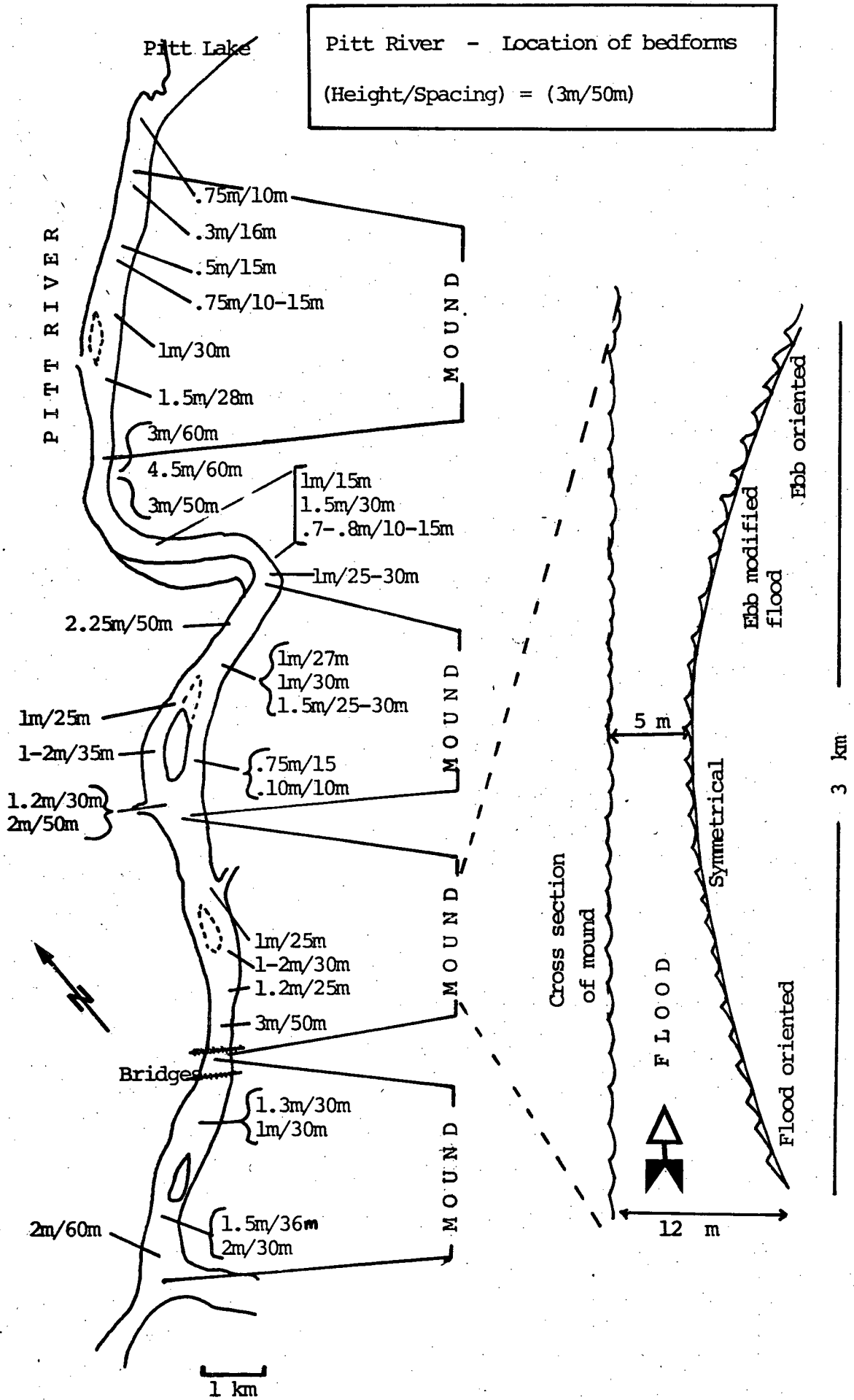
- Ritchie, J.C., Hawks, P.H., and McHenry, J.R., 1975, Deposition rates in valleys determined using Fallout Cesium-137: Geol. Soc. America Bull., v. 86, p. 1128-1130.
- Robbins, J.A. and Edgington, D.N., 1975, Determination of recent sedimentation rates in Lake Michigan using Pb-210 and Cs-137: Geochim. Cosmo. Chem. Acta, p. 285-304.
- Ryder, J.M. and Church, M., 1972, Paraglacial sedimentation: consideration of fluvial processes conditioned by glaciation: Geol. Soc. America Bull., v. 83, p. 3059-3072.
- Scruton, P.C., 1960, Delta building and the deltaic sequence: in Shepard, F.P., Phleger, F.B., Andel, T.H. (eds.), Recent Sediments, northwest Gulf of Mexico, Am. Assoc. Petroleum Geologist, Tulsa, Oklahoma.
- Sengupta, S., 1975, Size-sorting during suspension transportation-lognormality and other characteristics: Sedimentology, v. 22, p. 257-273.
- Sinclair, A.J., 1974, Selection of threshold values in geochemical data using probability graphs: Jour. Geochemical Explor., v. 3, p. 129-149.
- \_\_\_\_\_, 1976, Applications of probability graphs in mineral exploration: Assoc. of Explor. Geochemists, Spec. vol. no. 4., 95p.
- Spencer, D.W., 1963, The interpretation of grain size distribution of curves of clastic sediments: Jour. Sed. Petrology, v. 33, 180-190.
- Syndowski, K.H., 1957, Die synoptische method des Kornkurven-Vergleiches zur Ausdeutung fossiler sedimentations raume: Geol. Jahrb., v. 73, p. 235-275.
- Tamura, T., 1964, Selective sorption reaction of cesium with mineral soil: Nuclear Safety, v. 5, p. 262-268.
- Visher, G.S., 1969, Grain size distributions and depositional processes: Jour. Sed. Petrology, v. 39, p. 1074-1106.
- \_\_\_\_\_ and Howard, J.D., 1974, Dynamic relationship between hydraulics and sedimentation in the Altamaha Estuary: Jour. Sed. Petrology, v. 44, p. 502-521.

Water Survey of Canada, 1966, Vancouver, British Columbia:  
unpublished stage and discharge records.

## APPENDIX 1.



Log spacing-log height plot of sand waves found in Pitt River.



DATA USED IN THE MEANDER WAVELENGTH - BEDFORM WAVELENGTH SCALING  
RELATIONSHIP

River	$\lambda_M$ (in feet)	$\lambda_B$ (in feet)	$\lambda_M / \lambda_B$	$Q_e$	$\sqrt{Q_e}$	Sinuosity	Grain Size	Reference
Beaver	750	10	175	5,500	74	1.3	sand	Neill, 1973
Columbia (dammed)	43,000	67	641	400,000	632	-	sand	Whetten and Fullam, 1967
Congaree	13,120	88	149	17,650	133	1.75	0.59 mm	Lévey, 1975
Fraser	47,500	94	505	435,000	660	-	coarse sand	Pretious and Blench, 1951
Klaaralver	4,692	37	126	23,000	152	-	sand	Sundborg, 1956
Missouri	7,000	40	175	33,340	182	-	sand	Annambhotla et.al. 1972
Pitt	20,000	98	203	85,000	291	1.2	0.34 mm	This study
Red Deer	5,800	33	176	40,000	200	1.11	0.37 mm	Neill, 1973
Wabash	22,500	82	273	70,575	266	-	sand	Jackson, 1975

References under Part I except for:

Neill, C., 1973, Observations on river channel processes in Alberta: In Fluvial processes and sedimentation, Proc. of Hydrology Smposium, Univ. of Alberta, Edmonton, Alberta.

## APPENDIX 2

## VELOCITY PROFILE DATA

March 11, 1975 site (3) depth 8.8-9.7 m time - 1400 - 1830			March 11, 1975 (cont)		
depth (m)	vel. (cm/sec)		depth (m)	vel. (cm/sec)	
1400	0	35	1700	0	41
ebb	2.00	38	flood	2.00	40
	4.00	37		4.00	37
	6.00	38		6.00	37
	7.00	35		8.00	34
	8.25	29		9.00	27
	8.90	24		9.30	24
1430	0.00	33	1730		
ebb	2.00	30	flood	0	50
	4.00	30		2.00	47
	6.00	29		4.00	43
	7.00	30		6.00	40
	8.25	27		8.00	34
	8.80	24		9.00	29
1500 ebb	0	26	9.50	27	
	2.00	24	1800	0	58
	4.00	24	flood	2.00	58
	6.00	21		4.00	55
	7.00	20		6.00	50
	8.25	19		8.00	49
8.80	17	9.00		41	
				9.50	34
1530 ebb	0	14	1830	0	58
	2.00	15	flood	2.00	58
	4.00	15		4.00	55
	6.00	12		6.00	44
	7.00	13		8.00	43
	8.25	08		9.00	40
8.80	05	9.50		38	
Turn from ebb to flood			March 13, 1975 site (3) depth 8.8 - 9.2 m time - 730 - 1400		
1600 flood	0	08	730 flood	0	70
	2.00	05		2.00	64
	4.00	12		4.00	64
	6.00	03		6.00	61
	7.00	09		8.00	58
	8.00	12		8.60	42
1630 flood	8.90	05	9.20	40	
	0	20			
	2.00	20			
	4.00	20			
	6.00	20			
	8.00	20			
	9.00	15			
		12			

March 13, 1975 (cont)			March 13, 1975 (cont)		
	depth (m)	vel. (cm/sec)		depth (m)	vel. (cm/sec)
800	0	73	1100	0	05
flood	2.00	67	flood	2.00	07
	4.00	69		4.00	06
	6.00	58		6.00	06
	8.00	50		8.00	07
	8.60	30		9.00	06
	9.20	26		9.50	05
830	0	70	1130	0	23
flood	2.00	70	flood	2.00	24
	4.00	66		4.00	21
	6.00	55		6.00	21
	8.00	43		8.00	20
	8.60	37		9.00	20
	9.20	30			
900	0	56	1200	0	34
flood	2.00	56	flood	2.00	35
	4.00	58		4.00	34
	6.00	56		6.00	30
	8.00	44		7.00	37
	9.00	30		8.00	30
	9.20	26		9.00	27
930	0	47	1230	0	41
flood	2.00	43	flood	2.00	43
	4.00	43		4.00	40
	6.00	46		6.00	43
	8.00	40		7.00	41
	9.20	27		8.40	37
		18		9.00	28
					44
1000	0	37	1300	2.00	44
flood	2.00	37	flood	4.00	44
	4.00	35		6.00	43
	6.00	32		7.00	43
	8.00	28		8.40	38
	9.40	11		9.00	34
1030	0	21	1400	0	41
flood	2.00	20		2.00	43
	4.00	18		4.00	43
	6.00	17		6.00	37
	8.00	17		7.00	40
	9.00	12		8.40	38
	9.40	06		8.80	30
Turn from flood to ebb					



May 9, 1975 site (2) depth 11 -11.6 m time - 900 -1730			May 9, 1975 (cont)		
depth (m)		vel. (cm/sec)	depth (m)		vel. (cm/sec)
900 ebb	0	27	1200	0	59
	2.00	26	ebb	2.00	62
	4.00	22		4.00	59
	6.00	19		6.00	54
	8.00	19		8.00	54
	10.00	18		10.00	49
	11.60	12		11.40	30
930 ebb	0	48	1230	0	59
	2.00	46	ebb	2.00	62
	4.00	39		4.00	54
	6.00	33		6.00	59
	8.00	31		8.00	51
	10.00	26		10.00	44
	11.60	24		11.30	26
1000 ebb	0	50	1300	0	54
	2.00	51	ebb	2.00	62
	4.00	51		4.00	77
	6.00	50		6.00	57
	8.00	39		7.00	54
	10.00	33		8.00	49
	11.60	26		10.00	46
1030 ebb	0	77		11.30	26
	2.00	57	1330	0	51
	4.00	57	ebb	2.00	64
	6.00	51		4.00	57
	8.00	51		6.00	57
	10.00	41		8.00	54
	11.50	33		10.00	41
1100 ebb	0	51		11.20	36
	2.00	49	1400	0	54
	4.00	49	ebb	2.00	59
	6.00	49		4.00	54
	8.00	45		6.00	51
	10.00	31		8.00	49
	11.50	28		10.00	44
1130 ebb	0	57		11.20	41
	2.00	64	1430	0	57
	4.00	59	ebb	2.00	59
	6.00	59		4.00	57
	8.00	51		6.00	54
	10.00	41		8.00	51
	11.40	36		10.00	51
				11.10	46

May 9, 1975 (cont)			May 21, 1975 (cont)		
	depth (m)	vel. (cm/sec)		depth (m)	vel. (cm/sec)
1500 ebb	0	54	1530 flood	0	02
	2.00	59		2.00	03
	4.00	54		4.00	03
	6.00	51		6.00	03
	8.00	51		8.00	02
	10.00	49		9.10	02
	11.10	45			
1530 ebb	0	51	1600 flood	0	10
	2.00	51		2.00	10
	4.00	51		4.00	09
	6.00	51		6.00	09
	8.00	46		8.00	05
	10.00	46		8.80	04
	11.10	45			
1600 ebb	0	51	1630 flood	0	31
	2.00	49		2.00	31
	4.00	46		4.00	25
	6.00	44		6.00	25
	8.00	39		8.00	25
	10.00	28		10.00	17
	11.10	36(turbulent)		10.90	17
1630 ebb	0	39	1700 flood	0	39
	2.00	41		2.00	39
	4.00	40		4.00	39
	6.00	41		6.00	39
	8.00	39		8.00	31
	10.00	36		10.00	26
	11.10	24		10.90	23
1700 ebb	0	21	1730 flood	0	42
	2.00	21		2.00	44
	4.00	18		4.00	41
	6.00	18		6.00	40
	8.00	18		8.00	40
	10.00	21		10.00	32
	11.00	10		10.90	26
ebb to flood at 1715			1800 flood	0	40
May 21, 1975 site (2) depth 9.1 m and 10.9 m time - 1500 - 1900				2.00	40
				4.00	41
				6.00	40
				8.00	38
				10.00	35
				10.90	28
			1500 flood	0	08
2.00	08	2.00		36	
4.00	09=	4.00		40	
6.00	08	6.00		35	
8.00	08	8.00		33	
		10.00		27	
		10.90		23	

May 21, 1975 (cont)			June 12, 1975 (cont)		
	depth (m)	vel. (cm/sec)		depth (m)	vel. (cm/sec)
1900 flood	0	28	1300 ebb	0	36
	2.00	31		2.00	44
	4.00	28		4.00	46
	6.00	28		6.00	41
	8.00	28		8.00	28
	10.00	26		9.10	32
	10.90	23	11.00	26	
			12.20	18	
1930 flood	0	21	1330 ebb	0	45
	2.00	22		2.00	41
	4.00	19		4.00	46
	6.00	21		6.00	46
	8.00	19		8.00	41
	10.00	17		9.10	39
	10.90	14	11.00	28	
2000 flood	0	12	12.20	23	
	2.00	12	1400 ebb	0	45
	4.00	09		2.00	49
	6.00	08		4.00	49
	8.00	06		6.00	46
	10.00	05		8.00	45
10.9.	05	9.10		37	
Turn from flood to ebb 2045			11.00	31	
June 12, 1975 site (4)			12.20	26	
depth 11 - 12.2 m			1430 ebb	0	44
time - 1200 -2030				2.00	49
1200 ebb	0	26		4.00	46
	2.00	36		6.00	51
	4.00	36		8.00	46
	6.00	35		9.10	42
	8.00	39	11.00	28	
	9.10	31	12.20	24	
	11.00	21	1500 ebb	0	44
	12.20	10		2.00	46
1230 ebb	0	31		4.00	51
	2.00	39		6.00	50
	4.00	42		8.00	46
	6.00	35		9.10	39
	8.00	32	11.00	30	
	9.10	26	12.20	26	
	11.00	21	1600 ebb	0	51
	12.20	15		2.00	57
		4.00		51	
		6.00		51	
		8.00		49	
		9.10		49	
		11.00	39		
		12.20	28		

June 12, 1975 (cont)			June 24, 1975 site (4) depth 42 m time 700 -1230		
depth (m)		vel. (cm/sec)	depth (m)		vel. (cm/sec)
1630 ebb	0	41	730 flood	0	04
	2.00	51		6	13
	4.00	46		12	14
	6.00	49		18	15
	8.00	51		24	14
	9.10	49(turbulent)		30	12
	11.00	28		36	12
12.00	28	42	12		
1515 ebb	0	44	800 flood	0	27
	2.00	51		6	30
	4.00	49		12	30
	6.00	49		18	27
	8.00	46		24	24
	9.10	36		30	24
11.00	32	36	20		
1800 ebb	0	36	830 flood	0	38
	2.00	40		6	42
	4.00	45		12	42
	6.00	46		18	43
	8.00	41		24	40
	9.10	39		30	36
11.00	22	36	33		
1830 ebb	0	36	900 flood	0	47
	2.00	41		6	47
	4.00	39		12	44
	6.00	45		18	47
	8.00	44		24	38
	9.10	30		30	36
11.00	15	36	35		
1900 ebb	0	31	930 flood	0	40
	2.00	39		6	44
	4.00	39		12	45
	6.00	39		18	46
	8.00	32		24	47
	9.10	31		30	43
11.00	30	36	34		
2000 ebb	0	13	1000 flood	0	44
	2.00	13		6	47
	4.00	17		12	45
	6.00	15		18	44
	8.00	12		24	43
	9.10	12		30	43
11.00	08	36	33		
Ebb to flood at 2040			42	25	

June 24, 1975 (cont)			July 9, 1975 site (4) depth 28.5 - 31 m ; time 1030-1630		
depth (m)		vel. cm/sec)	depth (m)		(vel. cm/sec)
1030	0	40	1030	0	28
flood	6	43	ebb	5	30
	12	40		10	31
	18	35		15	31
	24	34		20	28
	30	31		25	31
	36	25		31	10
	42	22		0	29
1100	0	40	1100	5	30
flood	6	35	ebb	10	30
	12	35		15	28
	18	28		20	29
	24	27		25	27
	30	19		31	13
	36	19		0	35
	42	13	1145	5	32
1130	0	33	ebb	10	27
flood	6	31		15	25
	12	30		20	29
	18	24		25	28
	24	20		31	17
	30	21		0	35
	36	17	1215	5	35
	42	12	ebb	10	30
1200	0	27		15	27
flood	6	24		20	26
	12	21		25	26
	18	20		31	17
	24	12		0	34
	30	11	1245	5	34
	36	11	ebb	10	37
	42	05		15	29
1230	0	17		20	29
flood	6	15		25	28
	12	12		31	10
	18	10		0	38
	24	08	1315	5	37
	30	08	ebb	10	28
	36	08		15	31
	42	08		20	32
		06		25	24
				31	16

July 9, 1975 (cont)			August 6, 1975 (cont)		
depth (m)	vel. (cm/sec)		depth (m)	vel. (cm/sec)	
1400 ebb	0	37	1130 ebb	0	33
	5	39		2.0	33
	10	30		4.0	32
	15	30		6.0	28
	20	33		7.6	26
	25	30		8.0	26
	30	12		0	33
1430 ebb	0	34	1200 ebb	2.0	33
	5	40		4.0	31
	10	34		6.0	28
	15	32		7.6	26
	20	29		8.0	23
	25	27		0	33
	30	13		2.0	33
1515 ebb	0	42	1230 ebb	4.0	31
	5	40		6.0	28
	10	33		7.6	26
	15	31		8.0	15
	20	33		0	36
	25	28		2.0	33
	29	16		4.0	32
1545 ebb	0	39	1300 ebb	6.0	33
	5	38		7.0	46
	10	28		7.6	39
	15	18		8.0	27
	20	21		0	39
	25	21		2.0	35
	29	09		4.0	33
August 6, 1975 site (1B) depth 8 - 10 m time - 1030 -1815			1330 ebb	6.0	46
1030 ebb	0	35		7.0	46
	2.0	32		7.6	33
	4.0	31		8.0	28
	6.0	27		0	36
	7.6	33		2.0	40
	8.0	26		4.0	62
1100 ebb	0	33	6.0	55	turbulent
	2.0	33	7.0	46	
	4.0	32	7.6	31	
	6.0	28	8.0	29	
	7.6	28	0	71	
	8.0	31	2.0	65	
1400 ebb	0	33	1500 ebb	4.0	59
	2.0	33		6.0	49
	4.0	32		7.0	36
	6.0	28		7.6	22
	7.6	28		8.0	17
	8.0	31			

August 6, 1975 (cont)			August 6, 1975 (cont)			
	depth (m)	vel. (cm/sec)		depth (m)	vel. (cm/sec)	
1530 ebb	0	65	1815 flood	0	75	
	2.0	60		2.0	71	
	4.0	57		4.0	72	
	6.0	47		6.0	73	
	7.0	35		7.0	71	
	7.6	28		7.6	69	
	8.0	21		8.0	52	
1615 ebb	0	47	August 11, 1975 site (1B) depth 6.6 - 8 m time - 930 -1600			
	2.0	41	930 flood	0	29	
	4.0	35		2.0	32	
	6.0	33		4.0	34	
	8.0	19		5.6	37	
	9.0	09		6.0	27	
	9.7	07		6.6	25	
10.0	07	0		53		
Turned from ebb to flood			1000	2.0	56	
1645 1700 flood	0	12	flood	4.0	55	
	2.0	14		5.3	55	
	4.0	16		6.0	47	
	6.0	09		6.3	28	
	7.0	10		0	58	
	7.6	07		1030 flood	2.0	61
	8.0	12			4.0	61
1715 flood	0	14	5.0	51		
	2.0	12	6.0	36		
	4.0	14	0	65		
	6.0	15	1100	2.0	65	
	7.0	24		4.0	57	
	7.6	18		5.0	37	
8.0	12	6.0		26		
1745 flood	0	44	1115 flood	0	58	
	2.0	46		2.0	59	
	4.0	49		4.0	59	
	6.0	46		6.0	59	
	7.0	56		7.5	54	
	7.6	47		8.0	46	
	8.0	33		8.5	33	
1800 flood	0	69	1200 flood	0	45	
	2.0	62		2.0	45	
	4.0	68		4.0	47	
	6.0	65		6.0	40	
	7.0	66		7.2	35	
	7.6	61		8.0	26	
	8.0	56		8.2	18	

August 11, 1975 (cont)			August 13, 1975 (cont)		
depth (m)	vel. (cm/sec)		depth (m)	vel. (cm/sec)	
1300	0	11	1100	0	29
flood	2.0	09	ebb	6	19
	4.0	06		12	19
	6.0	03		18	18
	7.0	03		24.5	04
	8.0	03		25.5	03
Turned from flood to ebb at 1315			Turn from ebb to flood at 1115.		
1400	0	27	1200	0	14
ebb	2.0	32	flood	6.0	19
	4.0	30		12.0	19
	6.0	20		18.0	17
	7.0	16		24.0	17
1430	0	50		29.5	19
ebb	2.0	49		30.5	06
	4.0	43		0	31
	6.0	31	1230	6	30
	6.5	12	flood	12	28
	7.5	14		18	30
1500	0	59		24	29
ebb	2.0	55		30	28
	4.0	54		31.5	24
	5.3	37		32.5	22
	6.0	22		0	40
	6.2	20	1330	6	36
1530	0	58	flood	12	35
ebb	2.0	56		18	31
	4.0	44		24	30
	5.3	36		30	27
	6.0	25		31.5	24
	6.3	23		32.5	19
1600	0	55	1400	0	43
ebb	2.0	55	flood	6	32
	4.0	42		12	29
	5.5	39		18	27
	6.0	26		24	19
	6.5	21		30	16
August 13, 1975 site (4)				31	11
depth 25 - 32 m			1530	0	26
time - 1030 - 1530				6	13
1030	0	34	flood	12	12
ebb	6.0	36		18	09
	12.0	34		24	07
	18.0	28		29	03
	24.0	10		30	02
	25.5	01			



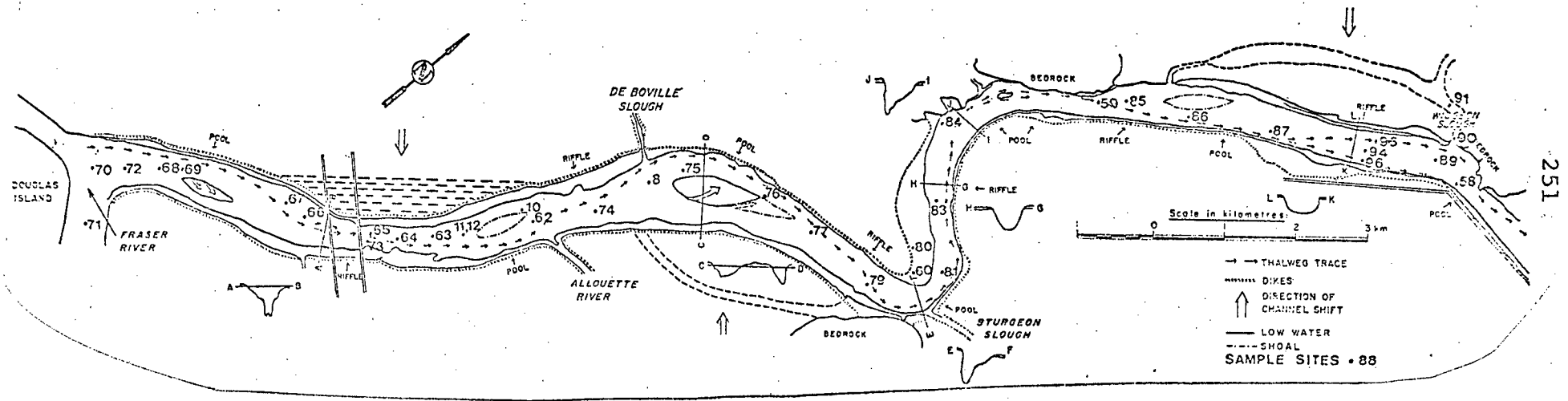
September 4, 1975, site (IA) depth 33 - 39 ft**** time - 1030 -1715			September 4, 1975 (cont)		
depth (ft) vel. (cm/sec) *****			depth (m) vel. (cm/sec)		
1030	0	30	1430	0	59
ebb	6	64	ebb	6	60
	12	64		12	52
	18	62		18	52
	24	59		24	53
	30	57		30	51
	33	53		35	43
	34	35		36	13
1100	0	62	1500	0	49
ebb	6	62	ebb	6	50
	12	60		12	50
	18	59		18	44
	24	55		24	45
	30	50		30	30
	33	28		35	18
	34	25		36	17
1130	0	67	1530	0	39
ebb	6	65		6	40
	12	64		12	37
	18	63		18	32
	24	60		24	28
	30	57		30	18
	33	53		33	13
	34	32		36	12
1230	0	61	1600	0	29
ebb	6	61	ebb	6	25
	12	62		12	17
	18	60		18	15
	24	60		24	13
	30	45		30	12
	35	46		35	10
	36	21		36	10
1300	0	65	Turned ebb to flood at 1615		
ebb	6	60	1700 - Very turbulent		
	12	58	1715	0	56
	18	57	flood	6	57
	24	54		12	57
	30	54		18	53
	33	38		24	37
	34	15		30	40
1330	0	57		34	33
ebb	6	59			
	12	57			
	18	55			
	24	51			
	30	47			
	35	44			
	36	27			

October 8, 1975 site (2) depth 12- 13 m time 1100 - 1700			October 8, 1975 (cont)		
depth (m)	vel. (cm/sec)		depth (m)	vel. (cm/sec)	
1100	0	70		0	36
flood	2.0	70	1600	2.0	39
	4.0	68	ebb	4.0	38
	6.0	67		6.0	36
	8.0	60		8.0	32
	10.0	62		10.0	30
	11.0	53		11.2	21
	12.0	52		12.0	21
				12.2	15
1215	0	66	1700	0	37
flood	2.0	65	ebb	2.0	41
	4.0	64		4.0	31
	6.0	58		6.0	31
	8.0	55		8.0	31
	10.0	52		10.0	26
	11.2	45		11.0	26
	12.0	36		12.0	20
	12.2	30		12.1	16
1300	0	58	November 5, 1975 site (2) depth 13 m time - 945 - 1100		
flood	2.0	56	945	0	46
	4.0	54	flood	2.0	40
	6.0	53		4.0	36
	8.0	47		6.0	43
	10.0	39		8.0	35
	11.6	24		10.0	25
	12.0	24		12.0	23
	12.6	19		13.0	14
1345	0	38	1100	0	32
flood	4.0	31	flood	2.0	23
	6.0	27		4.0	22
	8.0	21		6.0	15
	10.0	10		8.0	16
	11.6	09		10.0	20
	12.0	09		12.0	06
	12.6	07		13.0	06
Turn from flood to ebb at 1430.					
1530	0	21			
ebb	2.0	20			
	4.0	24			
	6.0	27			
	8.0	27			
	10.0	26			
	11.0	23			
	12.0	12			

February 20, 1976 site (2)		
depth = 13 m		
time - 900 - 1430		
	depth (m)	vel. (cm/sec)
900 flood	0	72
	2.0	51
	5.2	64
	7.0	64
	9.0	64
	11.0	59
	12.0	51
	12.8	36
	13.0	21
1145 flood	0	59
	2.0	59
	4.0	57
	6.0	51
	8.0	51
	10.0	41
	12.0	28
turned from flood to ebb at 1330.		
1400 ebb	0	21
	2.0	21
	4.0	26
	6.0	28
	8.0	33
	10.0	31
1430 ebb	12.0	10
	0	33
	2.0	51
	4.0	54
	6.0	49
	8.0	49
	10.0	15
	12.0	10

PITT RIVER - SEDIMENT SAMPLE LOCATIONS

APPENDIX 3



## Sediments sized with R.S.A. (Rapid Sediment Analyzer)

$\phi$	Cum. %	$\phi$	Cum. %	$\phi$	Cum. %
Pitt River(North)#4		PRSC #10		PRC #60	
0.64	0.0	0.43	0.0	1.18	0.0
0.75	4.00	0.50	2.99	1.25	2.08
1.00	12.80	0.75	13.79	1.50	12.47
1.25	23.20	1.00	26.44	1.75	21.30
1.50	40.00	1.25	52.29	2.00	34.29
1.75	54.40	1.50	65.57	2.25	65.45
2.00	74.00	1.75	86.21	2.50	91.95
2.12	100.00	1.86	100.00	2.53	100.00
PLC #6		PRSC #11		PRC #62	
1.0	0.0	0.97	0.0	0.51	0.0
1.5	4.35	1.00	1.02	0.75	9.79
1.75	8.50	1.25	8.77	1.00	22.68
2.00	16.00	1.50	21.54	1.25	36.08
2.25	36.9	1.75	32.62	1.50	51.55
2.50	60.0	2.00	47.60	1.75	71.13
3.00	78.0	2.25	84.31	1.89	100.00
3.50	83.0	2.47	100.00	PRC #63	
4.00	89.6	PRC #12		0.83	0.0
PRSC #8		1.26	0.0	1.00	4.37
0.56	0.0	1.50	13.70	1.25	10.92
0.75	7.08	1.75	26.03	1.50	25.14
1.00	16.81	2.00	42.81	1.75	32.51
1.25	25.66	2.25	83.56	2.00	45.90
1.50	46.90	2.40	100.00	2.25	77.56
1.75	62.83	PRC #58		2.47	100.00
2.00	84.07	1.26	0.0	PRC #66	
2.18	100.00	1.50	8.31	0.53	0.0
		1.75	10.00	0.75	8.42
		2.00	19.14	1.00	15.17
		2.25	61.06	1.25	35.39
		2.50	93.19	1.50	58.99
		2.53	100.00	1.75	79.21
		PRC #59		1.84	100.00
		1.43	0.0	PRC #67	
		1.50	6.74	0.73	0.0
		1.75	24.35	0.75	9.52
		2.00	50.77	1.00	10.08
		2.18	100.00	1.25	19.76
				1.50	36.82
				1.75	50.39
				2.00	73.64
				2.13	100.00

$\phi$	Cum. %
PRC #68	
0.51	0.0
0.75	15.38
1.00	32.31
1.25	52.31
1.50	84.62
1.60	100.00
PRC #69	
0.47	0.0
0.50	1.12
0.75	6.74
1.00	24.72
1.25	26.40
1.50	39.33
1.75	62.92
1.78	100.00
PRC #70	
0.47	0.0
0.50	0.51
0.75	10.71
1.00	21.43
1.25	35.71
1.50	55.10
1.75	82.34
1.88	100.00
PRC #71	
0.56	0.0
0.75	1.25
1.00	12.50
1.25	27.06
1.50	42.50
1.75	68.75
1.78	100.00
PRC #72	
0.97	0.0
1.00	1.94
1.25	11.63
1.50	28.68
1.75	42.63
2.00	65.50
2.18	100.00

$\phi$	Cum. %
PRC #73	
0.64	0.0
0.75	4.00
1.00	12.80
1.25	22.40
1.50	44.00
1.75	58.40
2.00	77.60
2.12	100.00
PRC #74	
0.97	0.0
1.00	1.65
1.25	14.50
1.50	35.00
1.75	54.00
2.00	77.50
2.06	100.00
PRC #75	
0.65	0.0
0.75	5.35
1.00	14.29
1.25	25.89
1.50	44.20
1.75	61.61
2.00	80.58
2.06	100.00
PRC #76	
0.57	0.0
0.75	3.02
1.00	15.09
1.25	24.90
1.50	40.75
1.75	53.58
2.00	71.69
2.12	100.00
PRC #77	
0.89	0.0
1.00	6.32
1.25	20.00
1.50	42.11
1.75	60.53
2.00	86.32
2.06	100.00

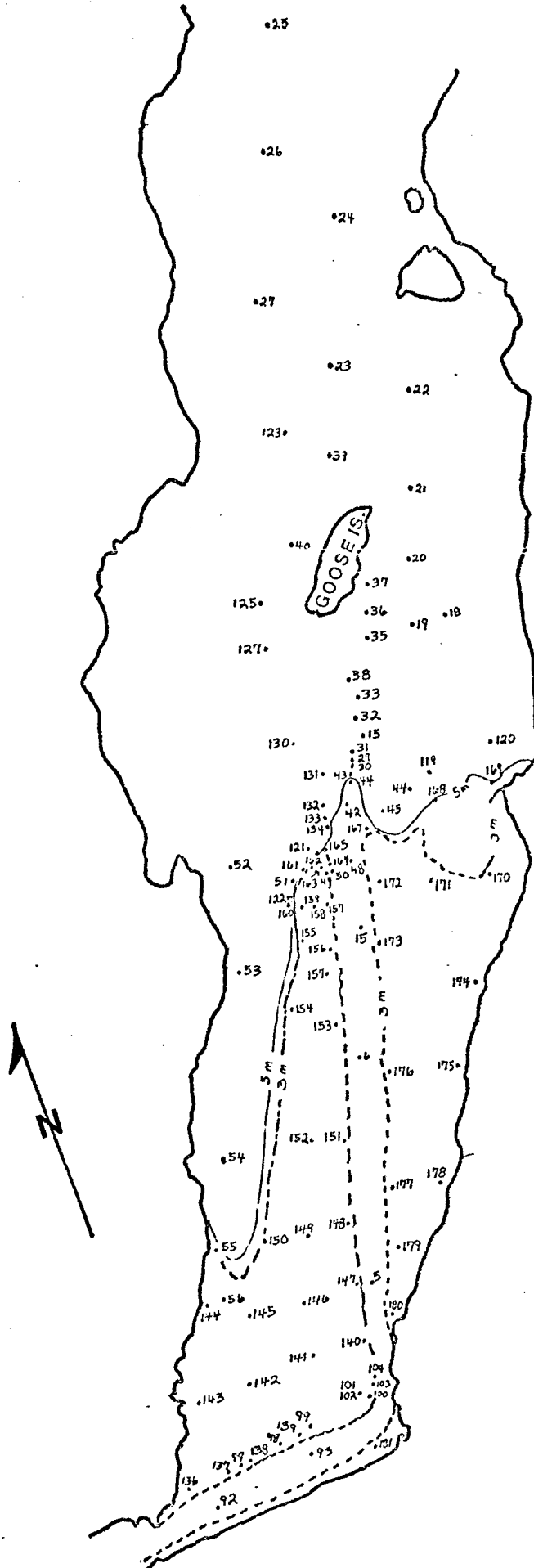
$\phi$	Cum. %
PRC #79	
0.84	0.0
1.00	8.06
1.25	17.74
1.50	35.08
1.75	49.60
2.00	69.76
2.12	100.00
PRC #80	
1.39	0.0
1.50	3.85
1.75	10.77
2.00	22.12
2.25	45.00
2.50	73.08
2.73	100.00
PRC #81	
0.62	0.0
0.75	0.74
1.00	5.18
1.25	8.52
1.50	14.81
1.75	21.11
2.00	30.37
2.25	48.89
2.50	65.93
2.75	94.81
2.80	100.00

	Cum. %
PRC #83	
24	0.0
25	0.68
50	9.15
75	17.39
00	28.61
25	55.84
50	86.96
56	100.00
PRC #84	
64	0.0
75	5.56
00	17.78
25	31.11
50	55.56
75	74.44
89	100.00
PRC #85	
12	0.00
25	5.53
50	18.46
75	29.54
00	44.62
25	80.62
39	100.00
PRC #86	
90	0.0
00	5.58
25	17.20
50	37.21
75	53.49
00	76.28
12	100.00
PRC #87	
77	0.0
00	2.86
25	8.57
50	17.14
75	27.14
00	60.07
25	97.14
26	100.00

$\phi$	Cum. %
PRC #89	
0.83	0.0
1.00	1.76
1.25	5.99
1.50	29.99
1.75	42.61
2.00	59.86
2.18	100.00
Widgeon S.90	
0.43	0.0
0.50	1.38
0.75	8.62
1.00	16.21
1.25	23.10
1.50	39.66
1.75	53.45
2.00	68.97
2.18	100.00
Widgeon S.91	
0.19	0.0
0.25	1.49
0.50	7.20
0.75	16.00
1.00	25.20
1.25	34.80
1.50	52.00
1.75	66.40
2.00	86.00
2.25	90.00
2.28	100.00
PLC #92	
0.73	0.0
0.75	1.16
1.00	8.91
1.25	19.37
1.50	34.49
1.75	48.84
2.00	73.64
2.11	100.00

$\phi$	Cum. %
PRC #94	
2.40	0.00
2.50	1.00
2.75	11.30
3.00	25.00
3.25	39.00
3.50	54.00
4.00	72.00
PLC #96	
1.18	0.0
1.25	2.10
1.50	14.97
1.75	25.75
2.00	40.42
2.25	76.05
2.47	100.00

PITT LAKE - SEDIMENT SAMPLE LOCATIONS

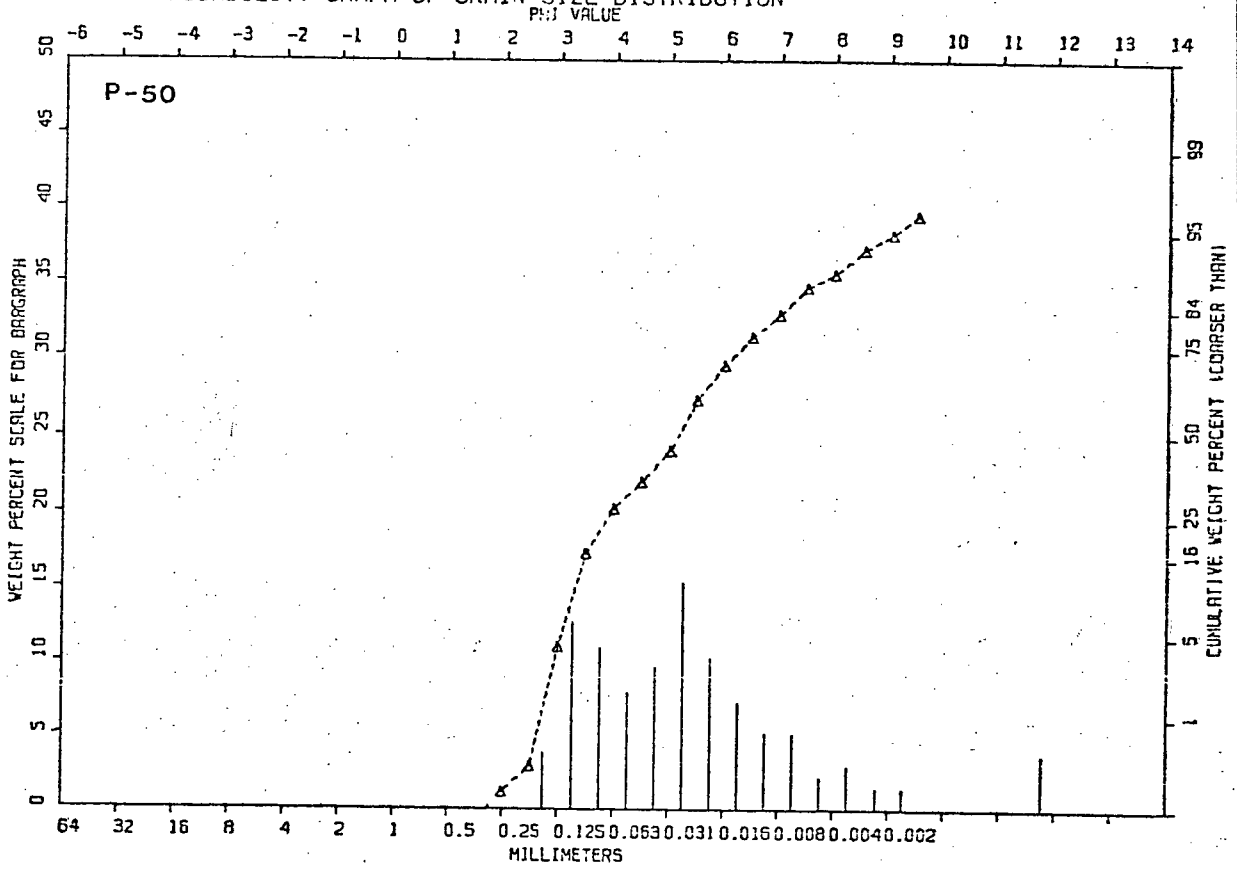


Depth Contours  
—— 5 m  
- - - 3 m

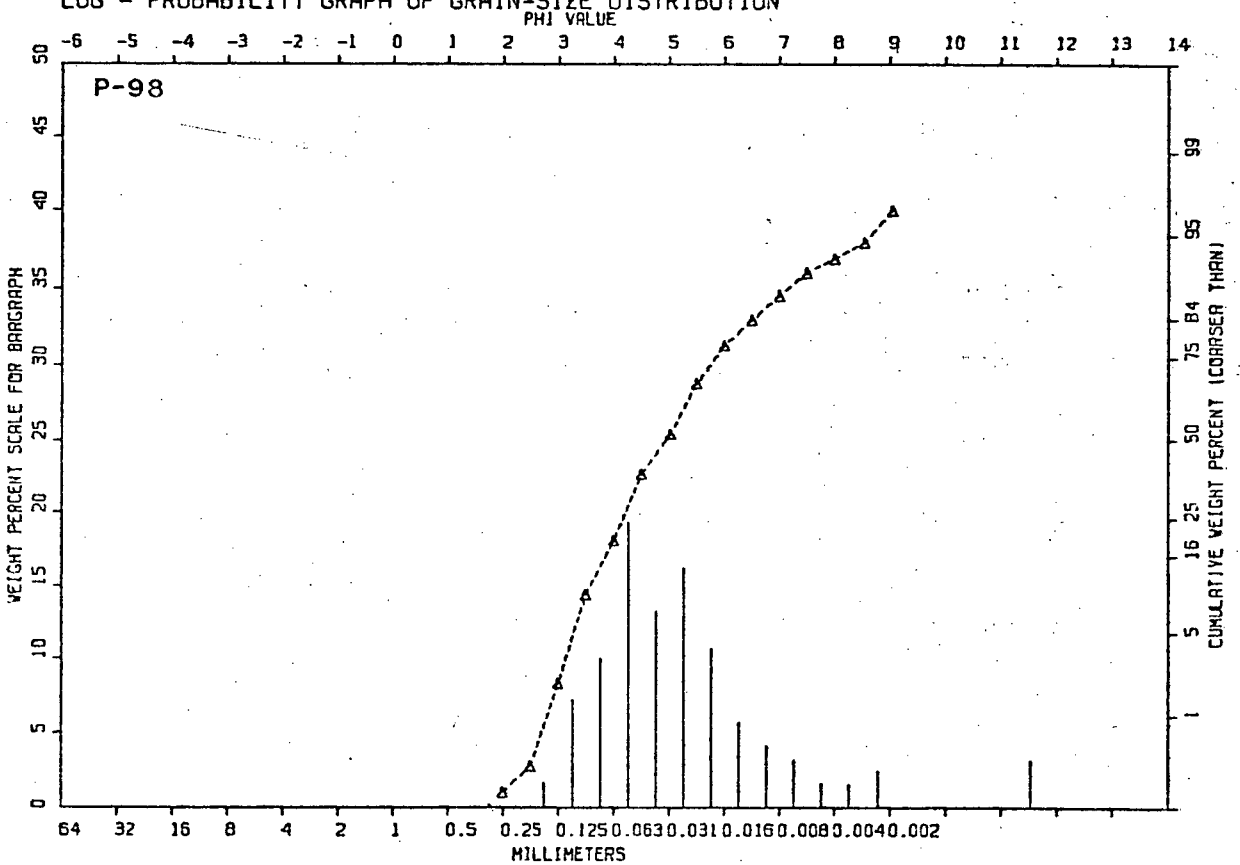
1 km



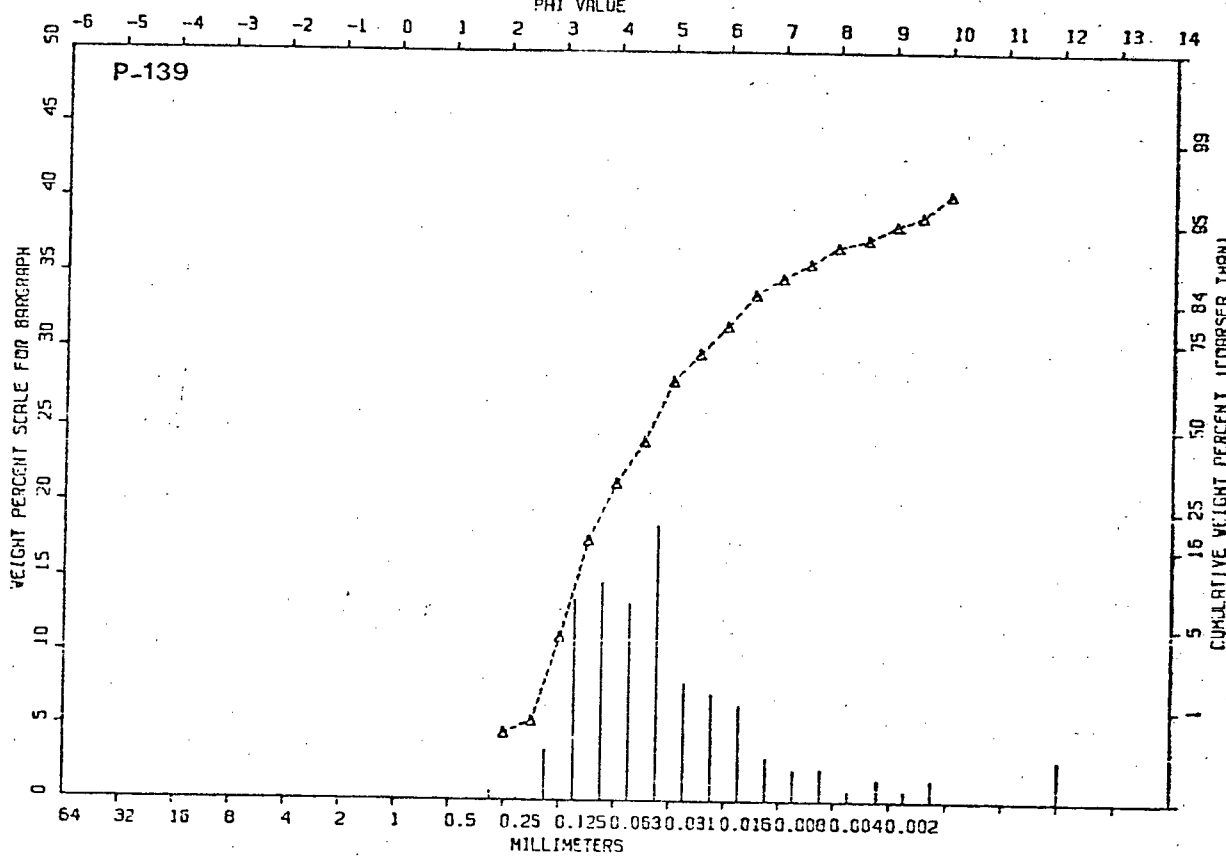
LOG - PROBABILITY GRAPH OF GRAIN-SIZE DISTRIBUTION



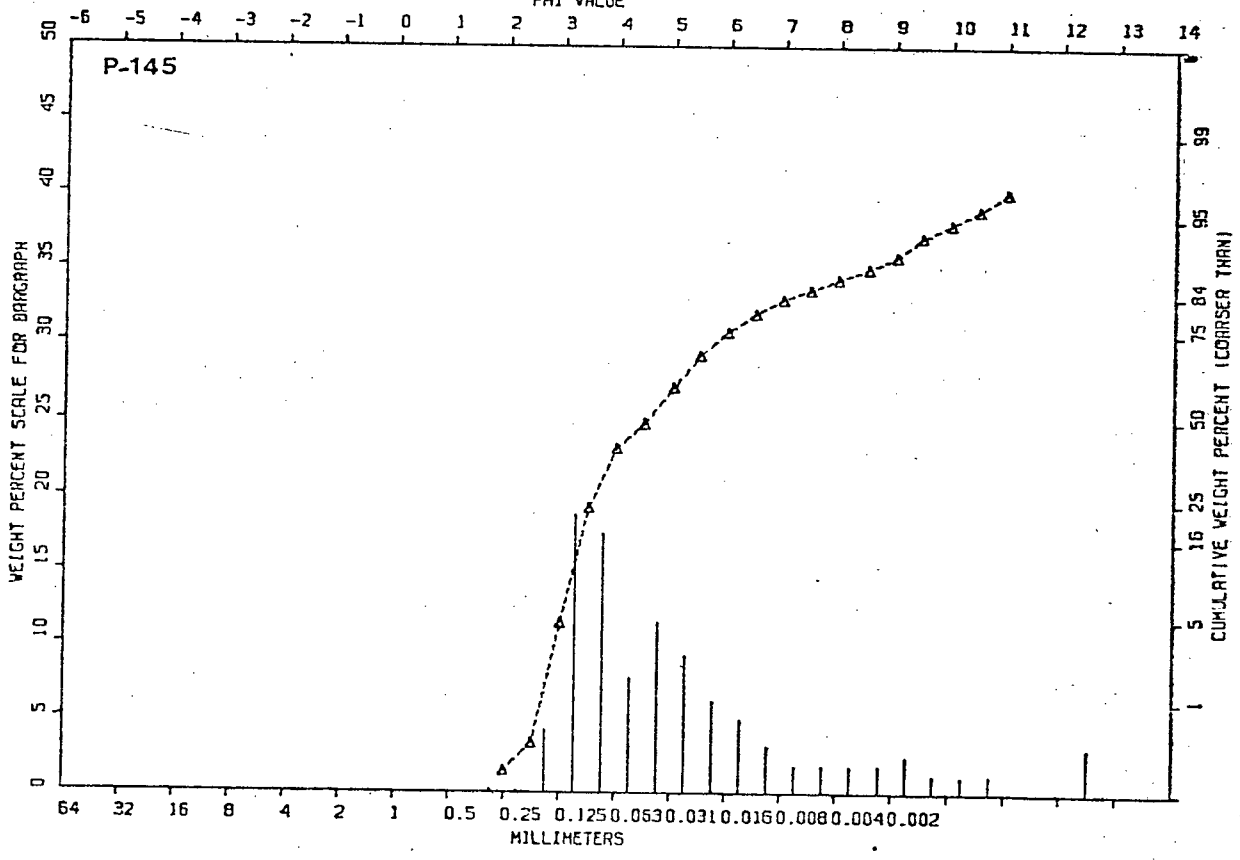
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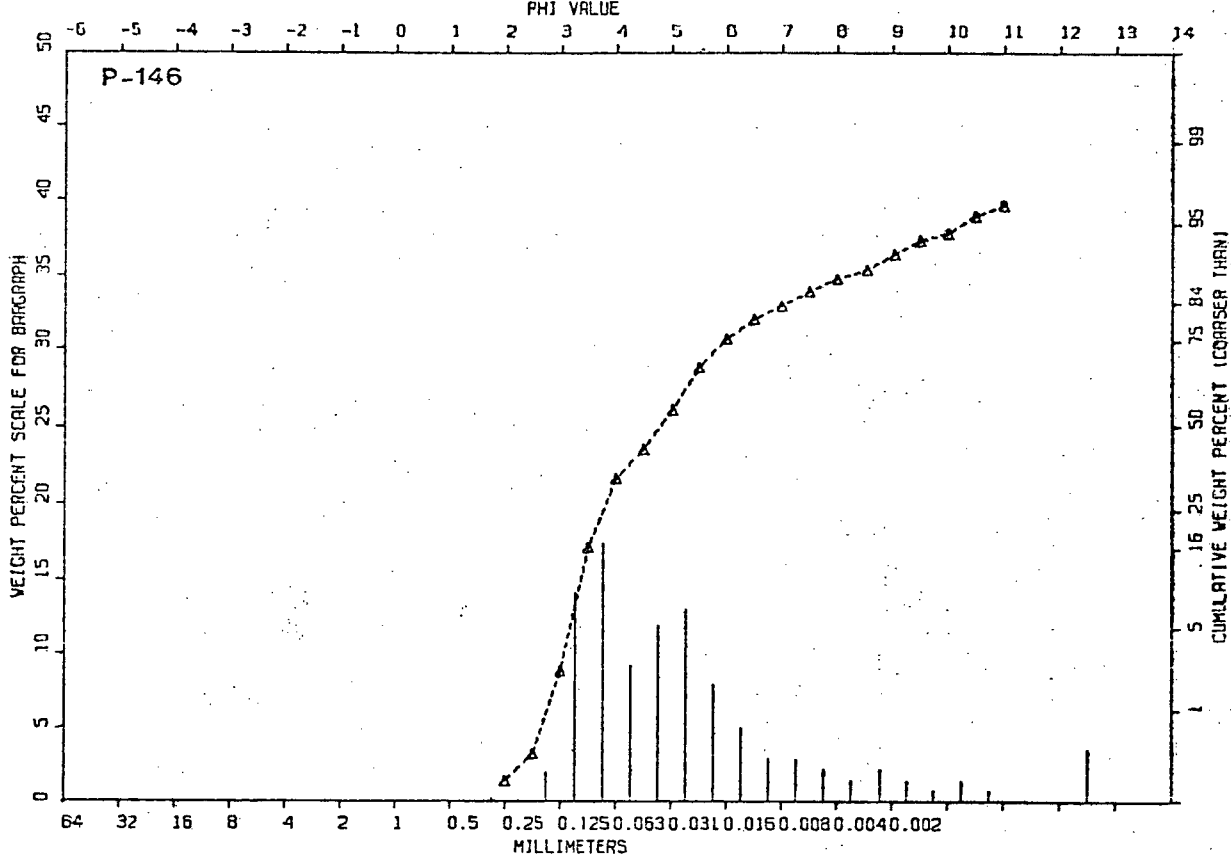
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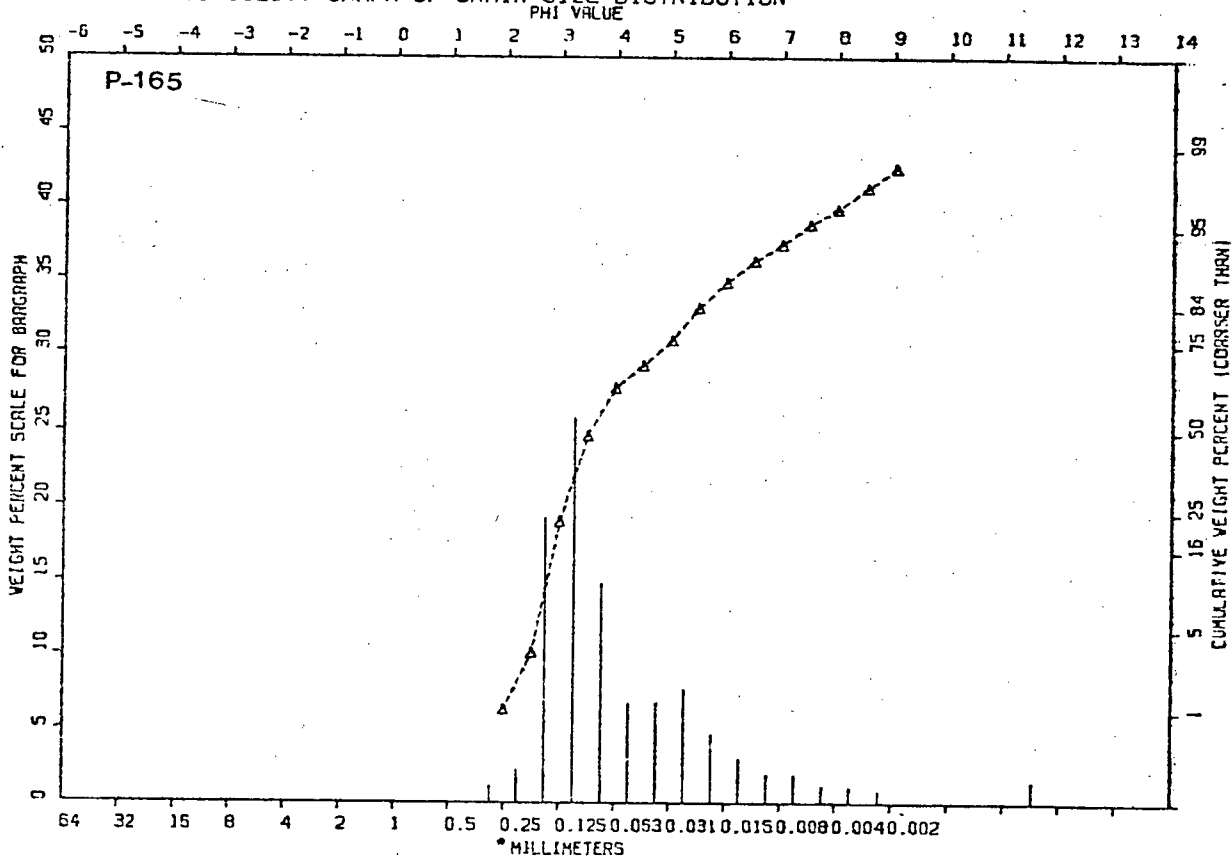
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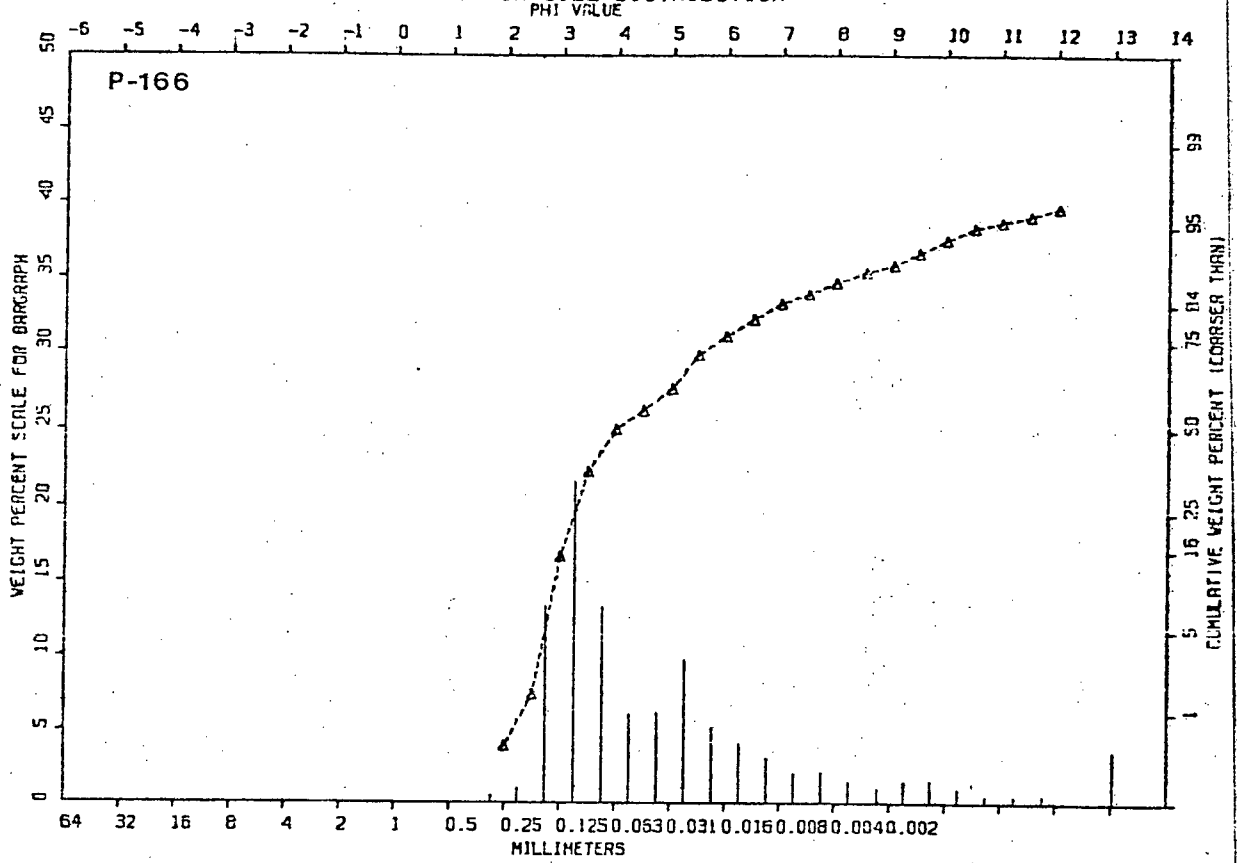
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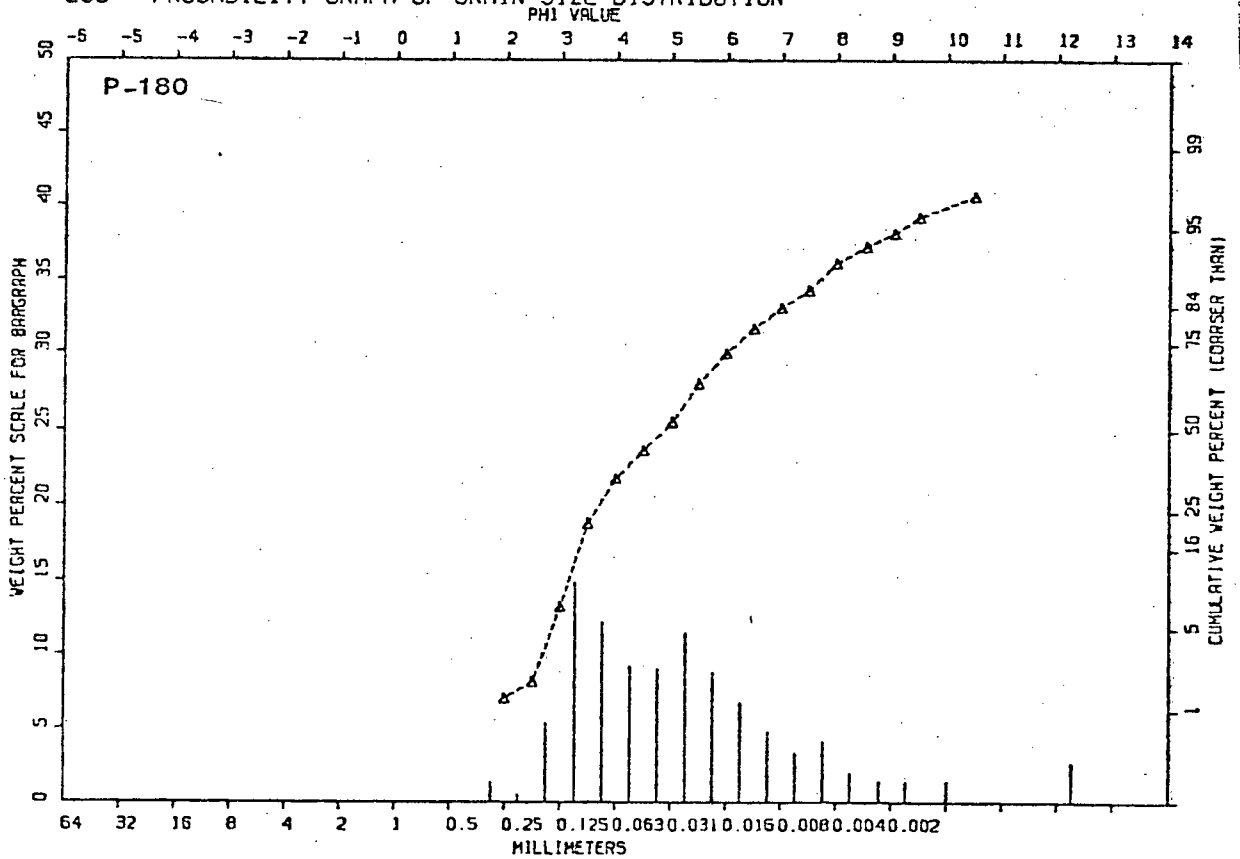
LOG - PROBABILITY GRAPH OF GRAIN-SIZE DISTRIBUTION



LOG - PROBABILITY GRAPH OF GRAIN-SIZE DISTRIBUTION



LOG - PROBABILITY GRAPH OF GRAIN-SIZE DISTRIBUTION



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0 0.0 0 0.0 0

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 \*\*\* MULTIMODAL SAMPLE \*\*\*  
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WFT WT	DRY WT	SALT	ORGANIC	MOISTURE	WEIGHT LOSS DUE TO HANDLING	0.0
1000.0000	3.6200	0.0	0.0	0.0 (GRAMS)	GRAVEL CORRECTION FACTOR	1.000
100.0000	100.0000	0.0	0.0	0.0 (PCT WET WT)	SIZES ELIMINATED (<0.01*)	NONE
					TRASK SORTING COEFFICIENT	2.955
					USING PROBABILITY EXTRAP.	2.945
					MEAN CUBED DEVIATION	7.347
					USING PROBABILITY EXTRAP.	4.591

PERCENTAGE COMPOSITION		TABLE OF STATISTICAL DATA IN PHI UNITS					PERCENTILES		LINEAR EXTRAP.		PROBABILITY EXTRAP.	
		MEAN	STD DEV	SKEWNESS	KURTOSIS	MM.	PHI UNITS	MM.	PHI UNITS			
GRAVEL	0.0	MOMENT	5.79256	2.43440	0.50919	3.44447	5.0	0.29265	1.77276	0.26576	1.91181	
SAND	22.65	P-MOMENT	5.77423	2.31737	0.36888	2.97328	10.0	0.18966	2.39853	0.16923	2.40180	
SILT	63.12	FOLK	5.62766	2.41173	0.00397	1.30856	16.0	0.09682	3.36861	0.09622	3.37745	
CLAY	14.23	P-FOLK	5.62721	2.38469	0.01222	1.29174	25.0	0.05259	4.24898	0.05236	4.25541	
MUD	77.35	INMAN	5.57278	2.20417	-0.07470	0.96075	50.0	0.01874	5.73743	0.01875	5.73738	
S/M	0.29	P-INMAN	5.57227	2.19479	-0.07509	0.93352	75.0	0.00805	6.95614	0.00808	6.95100	
		KRUMPEIN		2.00530	-0.13467	0.20735	84.0	0.00456	7.77695	0.00459	7.76707	
		P-KRUM.		1.95674	-0.13387	0.20680	90.0	0.00206	8.92647	0.00207	8.91919	
		FOLK (TRANSFORMED)				0.56683	95.0	0.00073	10.41642	0.00074	10.40793	
		P-FOLK (TRANSFORMED)				0.56365						

DATA FOR CONSTN OF BARGRAPHS AND CUM. CURVES

SIZE FRACTION	WT.(GMS)	WT.PCT.	WT.PCT.	MID PHI(LINEAR)	MID PHI(Prob.)	MODE
MM	PHI	UNCOR	COR	PHI	MM	PHI
0.250000	2.000	0.330	0.330	9.116	9.116	1.751
0.177000	2.496	0.040	0.040	1.105	10.221	2.249
0.125000	3.000	0.100	0.100	2.762	12.983	2.749
0.088000	3.506	0.150	0.150	4.144	17.127	3.253
0.062500	4.000	0.200	0.200	5.525	22.652	3.753
0.044000	4.506	0.173	0.173	4.775	27.427	4.253
0.031000	5.012	0.341	0.341	9.432	36.859	4.759
0.022000	5.506	0.143	0.143	3.946	40.805	5.259
0.015600	6.002	0.714	0.714	19.732	60.537	5.754
0.011000	6.506	0.057	0.057	1.577	62.115	6.254
0.007800	7.002	0.514	0.514	14.207	76.322	6.754
0.005500	7.506	0.200	0.200	5.525	81.847	7.254
0.003500	8.002	0.143	0.143	3.946	85.793	7.754
0.002700	8.533	0.086	0.086	2.369	88.162	8.268
0.001900	9.040	0.086	0.086	2.367	90.529	8.786
0.001360	9.561	0.057	0.057	1.579	92.198	9.270
0.000980	9.995	0.057	0.057	1.579	93.686	9.748
0.000690	10.501	0.057	0.057	1.577	95.264	10.248
0.000490	10.995	0.057	0.057	1.579	96.843	10.748
0.000061	14.000	0.114	0.114	3.157	100.000	12.497
TOTALS		3.620	3.620	100.0		

PI+ 5 0 0.0 0 0.0 0

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 \*\*\*\* MULTIMODAL SAMPLE \*\*\*\*  
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WET WT	4.8800	SALT	0.0	ORGANIC	0.0	MOISTURE	0.0	WEIGHT LOSS DUE TO HANDLING	0.0
1000.0000	4.8800	0.0	0.0	0.0	0.0	0.0	(GRAMS)	GRAVEL CORRECTION FACTOR	1.000
100.0001	100.0000	0.0	0.0	0.0	0.0	0.0	(PCT WET WT)	SIZES ELIMINATED (<0.01%)	NONE
								TRASK SORTING COEFFICIENT	3.104
								USING PROBABILITY EXTRAP.	3.091
								MEAN CUBED DEVIATION	16.003
								USING PROBABILITY EXTRAP.	13.096

PERCENTAGE COMPOSITION	TABLE OF STATISTICAL DATA IN PHI UNITS				PERCENTILES		LINEAR EXTRAP.		PROBABILITY EXTRAP.	
	MEAN	STD DEV	SKEWNESS	KURTOSIS	MM.	PHI UNITS	MM.	PHI UNITS		
GRAVEL 0.0	5.22597	2.50875	1.01353	3.88768	5.0	0.22834	2.13076	0.22101	2.17783	
SAND 34.63	5.21929	2.42354	0.52001	3.48396	10.0	0.17632	2.50374	0.17604	2.50598	
SILT 53.47	5.04375	2.42763	0.11248	1.06285	16.0	0.15306	2.70782	0.14920	2.74470	
CLAY 11.90	5.05297	2.40780	0.11881	1.05965	25.0	0.12211	3.03374	0.12195	3.03560	
MUD 65.37	4.59458	2.28677	-0.06450	0.85328	50.0	0.02832	5.14208	0.02834	5.14124	
S/M 0.53	5.00884	2.26414	-0.05847	0.85939	75.0	0.01267	6.30211	0.01276	6.29211	
		2.42101	-0.47415	0.26165	84.0	0.00643	7.28135	0.00647	7.27298	
		2.41223	-0.47738	0.26105	90.0	0.00232	8.74946	0.00233	8.74343	
				0.51523	95.0	0.00064	10.60678	0.00065	10.59768	
				0.51448						

DATA FOR CONSTN OF BARGRAPHS AND CUM. CURVES

SIZE FRACTION	WT.(GMS)	WT.PCT.	WT.PCT.	MID PHI(LINEAR)	MID PHI(PROB.)	MODE
MM	PHI	UNCR	COR	PHI	MM	MM
0.250000	2.000	0.160	0.160	3.279	3.279	1.751
0.177000	2.458	0.320	0.320	6.557	9.836	2.249
0.125000	3.000	0.720	0.720	14.754	24.590	2.749
0.088000	3.506	0.300	0.300	6.148	30.738	3.253
0.062500	4.000	0.190	0.190	3.893	34.631	3.753
0.044000	4.506	0.400	0.400	8.197	42.828	4.253
0.031000	5.012	0.180	0.180	3.689	46.516	4.759
0.022000	5.506	0.644	0.644	13.206	59.722	5.259
0.015600	6.002	0.516	0.516	10.565	70.287	5.754
0.011000	6.506	0.387	0.387	7.923	76.210	6.254
0.007900	7.002	0.193	0.193	3.962	82.172	6.754
0.005500	7.506	0.161	0.161	3.301	89.473	7.254
0.003700	8.002	0.129	0.129	2.641	88.115	7.754
0.002700	8.533	0.064	0.064	1.321	89.436	8.268
0.001900	9.040	0.064	0.064	1.321	50.756	8.786
0.001300	9.501	0.064	0.064	1.321	92.077	9.270
0.000900	9.955	0.064	0.064	1.321	93.398	9.748
0.000600	10.501	0.064	0.064	1.320	94.717	10.248
0.000400	10.955	0.064	0.064	1.321	96.038	10.748
0.000300	11.522	0.064	0.064	1.321	97.359	11.259
0.000200	14.000	0.129	0.129	2.641	100.000	12.741

TOTALS 4.880 4.880 100.0

Pl++ 15 0 0.0 0 0.0 0

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 \*\*\*\* MULTIMODAL SAMPLE \*\*\*\*  
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WET WT	DPY WT	SALT	ORGANIC	MOISTURE	WEIGHT LOSS DUE TO HANDLING	0.0
1000.0000	6.3300	0.0	0.0	0.0 (GRAMS)	GRAVEL CORRECTION FACTOR	1.000
100.0000	100.0000	0.0	0.0	0.0 (PCT WET WT)	SIZES ELIMINATED (%.01%)	NONE
					TRASK SORTING COEFFICIENT	2.124
					USING PROBABILITY EXTRAP.	2.113
					MEAN CUBED DEVIATION	19.308
					USING PROBABILITY EXTRAP.	15.238

PERCENTAGE COMPOSITION	TABLE OF STATISTICAL DATA IN PHI UNITS					PERCENTILES		LINEAR EXTRAP.		PROBABILITY EXTRAP.	
	MEAN	STD DEV	SKEWNESS	KURTOSIS		MM.	PHI UNITS	MM.	PHI UNITS		
GRAVEL 0.0	MOMENT 5.06196	2.23041	1.74020	6.21881	5.0	0.15332	2.70542	0.14483	2.78756		
SAND 36.97	P-MOMENT 5.04539	2.12064	1.59785	5.48084	10.0	0.12387	3.01307	0.12344	3.01810		
SILT 53.83	FGLK 4.72209	1.94749	0.38863	1.41123	18.0	0.10664	3.22915	0.10395	3.26599		
CLAY 9.20	P-FCLK 4.73492	1.92434	0.40346	1.40403	25.0	0.08509	3.55482	0.08479	3.55991		
MUD 63.03	INMAN 4.85614	1.62699	0.24532	1.30008	50.0	0.04553	4.45700	0.04551	4.45780		
S/M 0.59	P-INMAN 4.87347	1.60748	0.25858	1.30047	75.0	0.01886	5.72838	0.01899	5.71878		
	KRUMH. 1.61004	0.18460	0.22709	0.22709	84.0	0.01118	6.48313	0.01120	6.48096		
	P-KRUM. 1.59916	0.18154	0.22619	0.22619	90.0	0.00449	7.79884	0.00452	7.79026		
	FCLK (TRANSFORMED)		0.58527	0.58527	95.0	0.00086	10.18982	0.00086	10.18350		
	P-FCLK (TRANSFORMED)		0.58403	0.58403							

DATA FOR CONSTN OF BARGRAPHS AND CUM. CURVES

SIZE FRACTION	WT.(GMS)		WT.PCT.		MID PHI(LINEAR)		MID PHI(PROB.)		MCDE	
MM	PHI	UNCOR	COR	COR	CUMUL.	PHI	MM	PHI	MM	
0.250000	2.000	0.020	0.020	0.316	0.316	1.751	0.29707	1.894	0.26915	0
0.177000	2.498	0.090	0.090	1.422	1.738	2.249	0.21036	2.333	0.19845	0
0.125000	3.000	0.500	0.500	7.899	9.637	2.749	0.14875	2.827	0.14094	0
0.088000	3.506	0.890	0.890	14.060	23.697	3.253	0.10498	3.289	0.10229	1
0.062500	4.000	0.840	0.840	13.270	36.967	3.753	0.07416	3.765	0.07353	0
0.044000	4.506	0.914	0.914	14.440	51.407	4.253	0.05244	4.257	0.05232	1*
0.031000	5.012	0.416	0.416	6.571	57.978	4.759	0.03693	4.758	0.03696	0
0.022000	5.506	0.873	0.873	13.788	71.766	5.259	0.02612	5.250	0.02528	1
0.015600	6.002	0.457	0.457	7.223	78.989	5.754	0.01853	5.744	0.01865	0
0.011000	6.506	0.333	0.333	5.253	84.242	6.254	0.01310	6.243	0.01320	0
0.007800	7.002	0.166	0.166	2.626	86.868	6.754	0.00926	6.747	0.00931	0
0.005500	7.506	0.125	0.125	1.970	88.838	7.254	0.00655	7.247	0.00658	0
0.003900	8.002	0.125	0.125	1.970	90.808	7.754	0.00463	7.746	0.00466	1
0.002700	8.503	0.083	0.083	1.313	92.121	8.268	0.00325	8.260	0.00326	0
0.001900	9.004	0.042	0.042	0.656	92.777	8.786	0.00227	8.782	0.00227	0
0.001300	9.501	0.083	0.083	1.314	94.091	9.270	0.00162	9.261	0.00163	1
0.000980	9.995	0.042	0.042	0.656	94.747	9.748	0.00116	9.742	0.00117	0
0.000650	10.501	0.042	0.042	0.656	95.404	10.248	0.00082	10.241	0.00083	0
0.000490	10.995	0.042	0.042	0.657	96.061	10.748	0.00058	10.740	0.00058	1
0.000340	11.522	0.042	0.042	0.656	96.717	11.259	0.00041	11.249	0.00041	0
0.000061	14.000	0.208	0.208	3.283	100.000	12.761	0.00014	11.908	0.00026	0

TOTALS 6.330 6.330 100.0

PITT17

SIEVE, SH. PIP., SEDIGRAPH SAMPLE WT.= 4.8300

PHI PCT. CUMPCT.

1.50	0.21	
2.00	0.41	0.21
2.50	0.83	0.62
3.00	1.65	1.45
3.50	3.31	3.10
4.00	5.73	6.41
4.50	14.32	12.14
5.00	18.14	20.47
5.50	14.32	44.61
6.00	10.50	58.54
6.50	5.73	69.44
7.00	5.73	75.17
7.50	4.77	80.90
8.00	3.82	85.68
8.50	1.91	89.50
9.00	1.91	91.41
9.50	1.91	93.32
10.00	4.77	95.23
12.00		100.00

MEAN ST.DEV. SKEWNESS KURTOSIS

✓ 5.87 1.47 0.27 0.26 KRUMHEIN+PETTIIJOHN(1938) MOMENT MEASURES FOR SIZE RANGE 2.0 TO 10.0 PHI

6.05 1.73 0.36 1.37 FOLK GRAPHIC STATISTICAL PARAMETERS FOLK AND WARD,1957

PERCENTILES MEDIAN 5.69 5TH 3.79 16TH 4.63 25TH 4.95 75TH 6.99 84TH 7.82 95TH 9.94

PER CENT GRAVEL 0.0 SAND 6.41 SILT 79.63 ( 79.26 ) CLAY 13.96 ( 14.32 )

GRAVEL + SAND 6.41 SILT/(SILT+CLAY) 84.69PCT GRAV+SAND/SILT+CLAY 0.07



PI+ 18 C 0.0 0 0.0 0

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 \*\*\*\*  
 \*\*\* MULTIMODAL SAMPLE \*\*\*  
 \*\*\*\*  
 \*\*\*\*\*

WET WT DRY WT SALT ORGANIC MOISTURE  
 1000.0000 3.5400 0.0 0.0 0.0 (GRAMS)  
 100.0000 100.0000 0.0 0.0 0.0 (PCT WET WT)

WEIGHT LOSS DUE TO HANDLING 0.0  
 GRAVEL CORRECTION FACTOR 1.000  
 SIZES ELIMINATED (<0.01%) NONE  
 TRASK SORTING COEFFICIENT 2.320  
 USING PROBABILITY EXTRAP. 2.306  
 MEAN CUBED DEVIATION 13.558  
 USING PROBABILITY EXTRAP. 10.015

PERCENTAGE COMPOSITION

TABLE OF STATISTICAL DATA IN PHI UNITS

PERCENTILES LINEAR EXTRAP.

PROBABILITY EXTRAP.

	MEAN	STD DEV	SKEWNESS	KURTOSIS	MM.	PHI UNITS	MM.	PHI UNITS	
GRAVEL 0.0	6.40609	2.33263	1.06816	3.75840	5.0	0.08893	3.49115	0.08869	3.49505
SAND 10.73	6.37418	2.21769	0.91829	3.25227	10.0	0.06534	3.93581	0.06474	3.94914
SILT 67.21	6.43950	2.26371	0.43590	1.31216	16.0	0.04123	4.59598	0.04071	4.61856
CLAY 20.06	6.44436	2.25597	0.45869	1.31897	25.0	0.03274	4.93280	0.03247	4.94473
MUD 89.27	6.77205	2.17206	0.45931	0.78923	50.0	0.01827	5.77440	0.01827	5.77460
S/M 0.12	6.77924	2.16068	0.46496	0.79554	75.0	0.00609	7.36049	0.00611	7.35565
	KPUMPEIN	1.79829	0.37225	0.20021	84.0	0.00203	8.94411	0.00204	8.93992
	P-KPUM.	1.78589	0.37558	0.19929	90.0	0.00098	9.49855	0.00098	9.99815
	FOLK. (TRANSFORMED)			0.56750	95.0	0.00041	11.26381	0.00041	11.25423
	P-FOLK (TRANSFORMED)			0.56877					

DATA FOR CONSTN OF BARGRAPHS AND CUM. CURVES

SIZE FRACTION	WT.(GMS)	WT.PCT.	WT.PCT.	MID PHI(LINEAR)	MID PHI(PROB.)	MODE
MM	PHI	UNCOR	COR	PHI	MM	MM
0.250000	2.000	0.010	0.010	0.282	0.282	1.751
0.177000	2.498	0.020	0.020	0.565	0.847	2.249
0.125000	3.000	0.050	0.050	1.412	2.260	2.749
0.088000	3.506	0.100	0.100	2.825	3.085	3.255
0.062500	4.000	0.200	0.200	5.650	10.734	3.753
0.044000	4.506	0.097	0.097	2.733	13.468	4.253
0.021000	5.012	0.484	0.484	13.662	27.130	4.759
0.022000	5.506	0.548	0.548	15.484	42.614	5.259
0.015600	6.002	0.484	0.484	13.664	56.278	5.754
0.011000	6.506	0.355	0.355	10.320	66.298	6.254
0.007800	7.002	0.193	0.193	5.465	71.763	6.754
0.005900	7.506	0.161	0.161	4.555	76.318	7.254
0.003900	8.002	0.129	0.129	3.643	79.961	7.754
0.002700	8.533	0.064	0.064	1.822	81.783	8.268
0.001900	9.040	0.097	0.097	2.733	84.516	8.786
0.001380	9.501	0.097	0.097	2.732	87.247	9.270
0.000980	9.995	0.097	0.097	2.733	89.580	9.748
0.000690	10.501	0.097	0.097	2.733	92.713	10.248
0.000490	10.995	0.065	0.065	1.822	94.535	10.748
0.000340	11.522	0.032	0.032	0.911	95.446	11.259
0.000061	14.000	0.161	0.161	4.554	100.000	12.761

TOTALS 3.540 3.540 100.0

PITT19

SIEVE, SH. PIP., SEIGRAPH SAMPLE WT.= 4.0100

PHI PCT. CUMPT.

1.50	0.25		
2.00	0.25	0.25	
2.50	0.25	0.50	
3.00	0.25	0.75	
3.50	3.50	4.24	***
4.00	6.49	10.74	*****
4.50	9.92		*****
4.50	11.72	20.65	*****
5.00	15.33	32.38	*****
5.50	11.72	47.70	*****
6.00	7.21	59.43	*****
6.50	4.51	66.64	*****
7.00	4.51	71.15	*****
7.50	2.70	75.66	***
8.00	2.70	78.36	***
8.50	3.61	81.07	****
9.00	1.80	84.67	**
9.50	1.80	86.48	**
10.00	1.80	88.28	**
10.50	1.80	90.08	**
11.00	1.80	91.89	**
11.50	1.80	93.69	**
12.00	4.51	95.49	*****
12.00	100.00		

MEAN ST.DEV. SKEWNESS KURTOSIS

✓ 6.07 2.08 0.50 0.41 KRUMBEIN+PETTICORN (1938) MOMENT MEASURES FOR SIZE RANGE 2.0 TO 12.0 PHI

6.26 2.42 0.47 1.00 FOLK GRAPHIC STATISTICAL PARAMETERS FOLK AND WARD, 1957

PERCENTILES MEDIAN 5.60 5TH 3.56 16TH 4.27 25TH 4.69

PITT20

SIEVE, SH. PIP., SEDIGRAPH SAMPLE WT.= 3.2600

PHI PCT. COMPCT.

1.50			
2.00	0.31	0.31	
2.50	0.92	1.23	*
	1.23		*
3.00	2.46	2.46	**
3.50	3.69	4.92	****
4.00	3.73	8.60	****
4.50	11.19	12.33	*****
5.00	15.85	23.52	*****
5.50	13.99	39.38	*****
6.00	9.33	53.37	*****
6.50	6.53	62.69	*****
7.00	4.66	69.22	*****
7.50	3.73	73.89	****
8.00	3.73	77.62	****
8.50	2.80	81.35	***
9.00	2.80	84.15	***
9.50	2.80	86.94	***
10.00	1.87	89.74	**
10.50	1.57	91.61	**
11.00	1.87	93.47	**
11.50	0.93	95.34	*
12.00	3.73	96.27	****
12.00		100.00	

MEAN ST.DEV. SKEWNESS KUPTOSIS

✓ 6.29	2.01	0.37	0.20	KRUMBEIN+PETTIJOHN(1938) MOMENT MEASURES FOR SIZE RANGE 2.0 TO 12.0 PHI
6.51	2.27	0.42	1.57	FOLK GRAPHIC STATISTICAL PARAMETERS FOLK AND WARD,1957

PERCENTILES MEDIAN 5.88 5TH 3.91 16TH 4.66 29TH 5.05

PITT21A

SIEVE, SH. PIP., SEDIGRAPH SAMPLE WT.= 5.1100

PHI PCT. CUMPT.

1.50	0.20		
2.00	0.59	0.20	*
2.50	1.17	0.78	*
3.00	2.74	1.56	***
3.50	4.31	4.70	****
4.00	4.64	9.00	*****
4.50	11.14	13.64	*****
5.00	17.64	24.79	*****
5.50	14.86	42.43	*****
6.00	12.07	57.29	*****
6.50	7.43	69.36	*****
7.00	6.50	76.79	*****
7.50	3.71	83.29	****
8.00	2.79	87.00	***
8.50	2.79	89.79	***
9.00	1.86	92.57	**
9.50	1.86	94.43	**
10.00	3.71	96.29	****
12.00		100.00	

MEAN ST.DEV. SKEWNESS KURTOSIS

✓ 5.87 1.49 0.20 0.25 KRUMBEIN+PETTICORN(1938) MOMENT MEASURES FOR SIZE RANGE 2.0 TO 10.0 PHI

5.99 1.67 0.25 1.42 FOLK GRAPHIC STATISTICAL PARAMETERS FOLK AND WARD,1957

PERCENTILES MEDIAN 5.75 5TH 3.54 16TH 4.61 25TH 5.01  
75TH 6.88 84TH 7.60 95TH 9.65

PER CENT GRAVEL 0.0 SAND 9.00 SILT 78.28 ( 78.00) CLAY 12.72 ( 13.00)

GRAVEL + SAND 9.00 SILT/(SILT+CLAY) 85.71PCT GRAV+SAND/SILT+CLAY 0.10

PITT218

SIEVE, SH. PIP., SEDIGRAPH SAMPLE WT.= 3.5900

PHI PCT. CUMPT.

3.00	1.67	**
3.50	1.67	***
4.00	4.46	**
4.50	1.93	**
5.00	6.39	*****
5.50	12.18	*****
6.00	13.51	*****
6.50	25.69	*****
7.00	12.55	*****
7.50	38.24	*****
8.00	10.62	*****
8.50	48.85	*****
9.00	5.79	*****
9.50	54.64	*****
10.00	7.72	*****
10.50	62.36	*****
11.00	4.83	*****
11.50	67.19	*****
12.00	5.79	*****
	72.98	*****
	3.86	*****
	76.54	*****
	4.83	*****
	81.66	*****
	4.83	*****
	86.49	*****
	3.86	*****
	90.55	*****
	3.86	*****
	94.21	*****
	1.93	**
	96.14	*****
	3.86	*****
	100.00	

MEAN ST.DEV. SKEWNESS KURTOSIS

6.96 1.99 0.22 -0.74 KUMREIN+PETTIJOHN(1938) MOMENT MEASURES  
FOR SIZE RANGE 3.5 TO 11.5 PHI

7.16 2.22 0.34 1.23 FOLK GRAPHIC STATISTICAL PARAMETERS  
FOLK AND WARD,1957

PERCENTILES MEDIAN 6.60 5TH 4.14 16TH 5.14 25TH 5.47  
75TH 8.76 84TH 9.74 95TH 11.20

PER CENT GRAVEL 0.0 SAND 4.46 SILT 63.46 ( 62.73) CLAY 32.08 ( 32.81)

GRAVEL + SAND 4.46 SILT/(SILT+CLAY) 65.66PCT GRAV+SAND/SILT+CLAY 0.05

PITT22A

SIEVE, SH. PIP., SEDIGRAPH SAMPLE WT. = 4.0000

PHI PCT. CUMFCT.

1.50	0.25		
2.00	0.75	0.25	*
2.50	1.00	1.00	**
3.00	3.25	2.50	***
3.50	6.75	5.75	*****
4.00	7.95	12.50	*****
4.50	5.30	20.45	*****
5.00	12.37	25.76	*****
5.50	7.95	38.13	*****
6.00	7.07	46.09	*****
6.50	5.30	53.16	*****
7.00	6.19	58.46	*****
7.50	5.30	64.65	*****
8.00	6.19	69.95	*****
8.50	6.19	76.14	*****
9.00	4.42	82.32	****
9.50	4.42	86.74	****
10.00	2.65	91.16	***
10.50	2.65	93.81	***
11.00	3.54	96.46	****
12.00		100.00	

MEAN ST. DEV. SKEWNESS KUPTOSIS

✓ 6.45 2.12 0.11 -0.90 KRUMBEIN+PETTIDJOHN(1938) MOMENT MEASURES  
FOR SIZE RANGE 2.0 TO 11.0 PHI

6.56 2.35 0.19 1.24 FOLK GRAPHIC STATISTICAL PARAMETERS  
FOLK AND WARD, 1957

PERCENTILES MEDIAN 6.28 5TH 3.38 16TH 4.22 25TH 4.93  
75TH 8.41 84TH 9.19 95TH 10.72

PITT228

SIEVF, SH. PIP., SEDIGRAPH SAMPLE WT.= 3.9600

PHI	PCT. COMPCT.			
1.50	0.25			
2.00	0.51	0.25	*	
2.50	1.01	0.76	*	
3.00	1.77			
	2.02		**	
3.50	3.74			
	4.04		****	
4.00	7.83			
	4.66		*****	
4.50	12.48			
	5.59		*****	
5.00	18.07			
	14.90		*****	
5.50	32.97			
	13.03		*****	
6.00	46.00			
	6.52		*****	
6.50	52.52			
	7.45		*****	
7.00	59.97			
	5.59		*****	
7.50	65.55			
	4.66		*****	
8.00	70.21			
	4.66		*****	
8.50	74.86			
	4.66		*****	
9.00	79.52			
	4.66		*****	
9.50	84.17			
	3.72		****	
10.00	87.90			
	3.72		****	
10.50	91.62			
	3.72		****	
11.00	95.34			
	0.93		*	
11.50	96.28			
	3.72		****	
12.00	100.00			
MEAN	ST.DEV.	SKEWNESS	KURTOSIS	
6.65	2.07	0.19	-0.65	KRUMREIN+PETTICHOHN(1938) MOMENT MEASURES FOR SIZE RANGE 2.0 TO 11.5 PHI
6.87	2.27	0.32	1.28	FOLK GRAPHIC STATISTICAL PARAMETERS FOLK AND WARD, 1957
PERCENTILES	MEDIAN	6.31	5TH	3.65
			16TH	4.81
			25TH	5.23

75TH 8.51      84TH 9.48      95TH 10.95

PITT22C

SIEVE, SH. PIP., SEDIGRAPH SAMPLE WT.= 4.0000

PHI	PCT. CUMPT.	
2.50	0.25	
3.00	0.75	*
3.50	1.00	**
4.00	2.74	**
4.50	4.69	*****
5.00	9.55	*****
5.50	22.19	*****
6.00	34.84	*****
6.50	44.56	*****
7.00	53.32	*****
7.50	61.10	*****
8.00	66.93	*****
8.50	73.74	*****
9.00	80.55	*****
9.50	85.41	*****
10.00	90.27	***
10.50	93.19	***
11.00	96.11	***
12.00	100.00	

MEAN ST.DEV. SKEWNESS KURTOSIS

✓ 6.98 1.78 0.15 -0.73 KRUMBEIN+PETTITJOHN(1938) MOMENT MEASURES FOR SIZE RANGE 3.0 TO 11.0 PHI

7.14 1.98 0.26 1.16 FOLK GRAPHIC STATISTICAL PARAMETERS FOLK AND WARD, 1957

PERCENTILES MEDIAN 6.81 5TH 4.53 16TH 5.26 25TH 5.61

75TH 8.59 84TH 9.35 95TH 10.81

PER. CENT GRAVEL 0.0 SAND 2.74 SILT 64.21 ( 64.19) CLAY 33.04 ( 33.07)

GRAVEL + SAND 2.74 SILT/(SILT+CLAY) 66.00PCT GRAV+SAND/SILT+CLAY 0.03



PITT23A

SIEVE, SH. PIP., SEDIGRAPH SAMPLE WT.= 2.5600

PHI PCT. CUMFCT.

3.50	1.56	**
4.00	0.98	*
4.50	2.54	****
5.00	3.94	*****
5.50	5.91	*****
6.00	10.63	*****
6.50	23.22	*****
7.00	32.08	*****
7.50	38.97	*****
8.00	45.86	*****
8.50	53.73	*****
9.00	60.62	*****
9.50	66.53	*****
10.00	73.42	*****
10.50	78.34	*****
11.00	82.28	*****
11.50	87.20	*****
12.00	93.11	*****
12.00	97.05	*****
12.00	100.00	*****

MEAN ST.DEV. SKEWNESS KURTOSIS

✓ 7.84 2.10 0.10 -0.98 KRUMBEIN+PETT(1938) MOMENT MEASURES FOR SIZE RANGE 4.0 TO 12.0 PHI

8.03 2.30 0.16 1.15 FOLK GRAPHIC STATISTICAL PARAMETERS FOLK AND WARD, 1957

PERCENTILES MEDIAN 7.76 5TH 4.81 16TH 5.67 25TH 6.10  
75TH 9.66 84TH 10.67 95TH 11.74

PER CENT GRAVEL 0.0 SAND 1.56 SILT 52.63 ( 52.17) CLAY 45.81 ( 46.27)

GRAVEL + SAND 1.56 SILT/(SILT+CLAY) 53.00PCT GRAV+SAND/SILT+CLAY 0.02

PITT238

SIEVE, SH. PIP., SEDIGRAPH SAMPLE WT.= 2.7900

PHI PCT. CUMPT.

3.50	2.15	**
4.00	2.15	**
4.50	1.96	**
	4.11	***
5.00	2.94	***
	7.05	*****
5.50	6.85	*****
	13.90	*****
6.00	6.85	*****
	20.75	*****
6.50	8.81	*****
	29.55	*****
7.00	4.89	*****
	34.44	*****
7.50	4.89	*****
	39.34	*****
8.00	6.85	*****
	46.18	*****
8.50	7.83	*****
	54.01	*****
9.00	6.85	*****
	60.86	*****
9.50	5.87	*****
	66.73	*****
10.00	4.89	*****
	71.62	*****
10.50	5.87	*****
	77.50	*****
11.00	4.89	*****
	82.39	*****
11.50	6.85	*****
	89.24	*****
12.00	4.89	*****
	94.13	*****
12.00	5.87	*****
	100.00	

MEAN ST.DEV. SKEWNESS KURTOSIS

✓ 8.03 2.21 0.00 -1.07 KRUMBEIN+PETTICORN(1938) MOMENT MEASURES FOR SIZE RANGE 4.0 TO 12.0 PHI

8.34 2.48 0.04 1.13 FOLK GRAPHIC STATISTICAL PARAMETERS FOLK AND WARD,1957

PERCENTILES MEDIAN 6.24 5TH 4.65 16TH 5.65 25TH 6.24  
75TH 10.29 84TH 11.12 95TH 12.00

PER CENT GRAVEL 0.0 SAND 2.15 SILT 43.99 ( 44.03) CLAY 53.86 ( 53.82)

PITT23C

## SEDIGRAPH ANALYSIS

PHI PCT. CUMPT.

4.00

0.0

4.50

0.0

5.00

1.00

1.00

5.50

1.00

2.00

6.00

3.00

5.00

6.50

6.00

11.00

7.00

9.00

20.00

7.50

12.00

32.00

8.00

13.00

45.00

8.50

11.00

56.00

9.00

9.00

65.00

9.50

8.00

73.00

10.00

7.00

80.00

10.50

5.00

85.00

11.00

4.00

89.00

11.50

4.00

93.00

12.00

4.00

97.00

12.00

3.00

100.00

MEAN ST.DEV. SKEWNESS KUPTOSIS

8.36

1.62

0.14

-0.55

KFUMBEIN+PETTIJOHN(1938) MOMENT MEASURES  
FOR SIZE RANGE 4.5 TO 12.0 PHI

8.47

1.78

0.21

1.18

FOLK GRAPHIC STATISTICAL PARAMETERS  
FOLK AND WARD, 1957

PERCENTILES

MEDIAN

8.23

5TH

6.00

16TH

6.78

25TH

7.21

75TH

9.64

84TH

10.40

95TH

11.75

PER CENT GRAVEL

0.00

SAND 0.0

SILT 0.0

(.56.00)

CLAY 0.0

(.44.00)

GRAVEL + SAND

0.00

SILT/(SILT+CLAY)

56.00PCT

GRAV+SAND/SILT+CLAY

0.00

LABELS SHEPARD -CLAYEY SILT FOLKIGMS)-MUD

(SCS)-MUD

PITT24A

SIEVE, SH. PIP., SEDIGRAPH SAMPLE WT.= 3.8500

PHI PCT. CUMPT.

3.50			**
4.00	1.82	1.82	***
4.50	2.95	4.77	***
5.00	2.95	7.71	***
5.50	5.89	13.60	*****
6.00	4.91	18.51	*****
6.50	8.84	27.35	*****
7.00	6.87	34.22	*****
7.50	7.85	42.07	*****
8.00	8.84	50.91	*****
8.50	4.91	55.82	*****
9.00	7.85	63.67	*****
9.50	6.87	70.55	*****
10.00	5.89	76.44	*****
10.50	3.93	80.36	****
11.00	2.95	83.31	***
11.50	4.91	88.22	****
12.00	3.93	92.15	****
12.50	3.93	96.07	****
12.00	100.00		

MEAN ST.DEV. SKEWNESS KURTOSIS

8.03 2.21 0.07 -0.84

KRUMBEIN+PETTIJOHN(1938) MOMENT MEASURES  
FOR SIZE RANGE 4.0 TO 12.5 PHI

8.25 2.52 0.15 1.31

FOLK GRAPHIC STATISTICAL PARAMETERS  
FOLK AND WARD,1957

PERCENTILES	MEDIAN	7.95	5TH	4.54	16TH	5.74	25TH	6.37
			75TH	9.88	84TH	11.07	95TH	12.36

PER CENT GRAVEL 0.0 SAND 1.82 SILT 49.42 ( 49.09) CLAY 48.76 ( 49.09)

PITT24B

SIEVE, SH. PIP., SEDIGRAPH SAMPLE WT.= 3.7900

PHI PCT. CUMPCT.

3.50			
4.00	1.06	1.06	*
4.50	2.97	4.02	***
5.00	5.94	9.96	*****
5.50	7.92	17.88	*****
6.00	6.93	24.80	*****
6.50	8.91	33.71	*****
7.00	4.95	38.65	*****
7.50	8.91	47.56	*****
8.00	6.93	54.49	*****
8.50	6.93	61.41	*****
9.00	6.93	68.34	*****
9.50	3.96	75.26	****
10.00	4.95	79.22	****
10.50	2.97	84.17	***
11.00	3.96	87.14	****
11.50	3.96	91.10	****
12.00	4.95	95.05	****
12.00		100.00	

MEAN ST.DEV. SKEWNESS KURTOSIS

✓ 7.65 2.10 0.11 -0.91 KRUMBEIN+PETTIJOHN(1938) MOMENT MEASURES FOR SIZE RANGE 4.0 TO 12.0 PHI

7.85 2.40 0.13 1.25 FOLK GRAPHIC STATISTICAL PARAMETERS FOLK AND WARD,1957

PERCENTILES MEDIAN 7.68 5TH 4.58 16TH 5.38 25TH 6.01

75TH 9.48 84TH 10.48 95TH 11.99

PER CENT GRAVEL 0.0 SAND 1.06 SILT 53.43 ( 53.43) CLAY 45.51 ( 45.51)

GRAVEL + SAND 1.06 SILT/(SILT+CLAY) 54.00PCT GRAV+SAND/SILT+CLAY 0.01



PITT25A

SIEVE, SH. PIP., SEDIGRAPH SAMPLE WT.= 3.6400

PHI PCT. CUMPT.

3.50	0.55	*
4.00	0.99	0.55
4.50	0.99	1.54
5.00	1.99	2.54
5.50	0.99	4.53
6.00	4.97	5.52
6.50	5.97	10.49
7.00	12.93	16.46
7.50	10.94	29.39
8.00	9.95	40.33
8.50	9.95	50.27
9.00	6.96	60.22
9.50	5.97	67.18
10.00	6.96	73.15
10.50	4.97	80.11
11.00	6.96	85.08
11.50	6.96	92.04
12.00	0.99	99.01
12.50	100.00	

MEAN ST.DEV. SKEWNESS KURTOSIS

8.62 1.82 -0.02 -0.55 KRUMBEIN+PETTICORN(1938) MOMENT MEASURES FOR SIZE RANGE 4.0 TO 12.0 PHI

8.78 1.89 0.15 1.14 FOLK GRAPHIC STATISTICAL PARAMETERS FOLK AND WARD, 1957

PERCENTILES MEDIAN 8.49 5TH 5.74 16TH 6.96 25TH 7.33

75TH 10.13 84TH 10.89 95TH 11.71

PER CENT GRAVEL 0.0 SAND 0.55 SILT 39.78 ( 39.78) CLAY 59.67 ( 59.67)

GRAVEL + SAND 0.55 SILT/(SILT+CLAY) 40.00PCT GRAV+SAND/SILT+CLAY 0.01

PITT25B

SEDIGRAPH ANALYSIS

PHI PCT. CUMPT.

4.00			
4.50	0.0	0.0	
5.00	0.0	0.0	
5.50	2.00		**
6.00	1.00		*
6.50	3.00		***
7.00	8.00		*****
7.50	11.00		*****
8.00	15.00		*****
8.50	12.00		*****
9.00	50.00		*****
9.50	7.00		*****
10.00	7.00		*****
10.50	6.00		*****
11.00	8.00		*****
11.50	6.00		*****
12.00	8.00		*****
12.00	2.00		**
12.00	100.00		

MEAN ST.DEV. SKEWNESS KURTOSIS

8.81 1.72 0.08 -0.97 KRUMBEIN+PETTIJOHN(1938) MOMENT MEASURES  
FOR SIZE RANGE 4.5 TO 12.0 PHI

8.86 1.81 0.24 1.02 FGLK GRAPHIC STATISTICAL PARAMETERS  
FOLK AND WARD,1957

PERCENTILES MEDIAN 8.50 5TH 6.33 16TH 7.09 25TH 7.50  
75TH 10.42 84TH 11.00 95TH 11.81

PER CENT GRAVEL 0.00 SAND 0.0 SILT 0.0 ( 50.00) CLAY 0.0 ( 50.00)

GRAVEL + SAND 0.00 SILT/(SILT+CLAY) 50.00PCT GRAV+SAND/SILT+CLAY 0.00

LABELS SHEPARD -CLAYEY SILT FOLK(GMS)-MUD

(SCS)-MUD



PITT25C

SIEVE, SH. PIP., SEDIGRAPH SAMPLE WT.= 4.6200

PHI PCT. CUMPT.

3.50				
	0.87		*	
4.00		0.87		
	0.99		*	
4.50		1.86		
	0.99		*	
5.00		2.85		
	0.99		*	
5.50		3.84		
	1.98		**	
6.00		5.82		
	5.95		*****	
6.50		11.77		
	8.92		*****	
7.00		20.69		
	11.90		*****	
7.50		32.59		
	12.89		*****	
8.00		45.48		
	10.90		*****	
8.50		56.38		
	8.92		*****	
9.00		65.30		
	7.93		*****	
9.50		73.23		
	6.94		*****	
10.00		80.17		
	4.96		*****	
10.50		85.13		
	3.97		****	
11.00		89.10		
	3.97		****	
11.50		93.06		
	3.97		****	
12.00		97.03		
	2.97		***	
12.00		100.00		

MEAN ST.DEV. SKEWNESS KURTOSIS

8.31 1.70 0.03 -0.22 KRUMBEIN+PETTICHOHN(1938) MOMENT MEASURES  
FOR SIZE RANGE 4.0 TO 12.0 PHI

8.44 1.81 0.19 1.22 FOLK GRAPHIC STATISTICAL PARAMETERS  
FOLK AND WARD, 1957

PERCENTILES MEDIAN 8.21 5TH 5.79 16TH 6.74 25TH 7.18

75TH 9.63 84TH 10.39 95TH 11.74

PER CENT GRAVEL 0.0 SAND 0.87 SILT 44.42 ( 44.61) CLAY 54.71 ( 54.52)

GRAVEL + SAND 0.87 SILT/(SILT+CLAY) 45.00PCT GRAV+SAND/SILT+CLAY 0.31

PITT26A

SEDIGRAPH ANALYSIS

PHI PCT. CUMPCT.

4.00	1.00	*
4.50	1.00	
	0.0	
5.00	1.00	**
	2.00	
5.50	3.00	**
	2.00	
6.00	5.00	*****
	5.00	
6.50	10.00	*****
	5.00	
7.00	15.00	*****
	10.00	
7.50	25.00	*****
	11.00	
8.00	36.00	*****
	11.00	
8.50	47.00	*****
	10.00	
9.00	57.00	*****
	8.00	
9.50	65.00	*****
	5.00	
10.00	70.00	*****
	5.00	
10.50	75.00	*****
	5.00	
11.00	80.00	**
	2.00	
11.50	82.00	*****
	9.00	
12.00	91.00	*****
	5.00	
12.50	96.00	****
	4.00	
12.00	100.00	

MEAN ST.DEV. SKEWNESS KURTOSIS

8.80 1.89 0.08 -0.67

KRUMBEIN+PETTITJOHN(1938) MOMENT MEASURES  
FOR SIZE RANGE 4.5 TO 12.5 PHI

9.10 2.11 0.24 1.18

FOLK GRAPHIC STATISTICAL PARAMETERS  
FOLK AND WARD,1957

PERCENTILES MEDIAN 8.65 5TH 6.00 16TH 7.05 25TH 7.50

75TH 10.50 84TH 11.61 95TH 12.40

PER CENT GRAVEL 0.00 SAND 1.00 SILT 0.0 ( 46.00) CLAY 0.0 ( 53.00)



PITT26C

SEDIGRAPH ANALYSIS

PHI PCT. CUMPCT.

4.00			
4.50	1.00	1.00	*
5.00	2.00	3.00	**
5.50	3.00	6.00	***
6.00	5.00	11.00	****
6.50	6.00	17.00	*****
7.00	9.00	26.00	*****
7.50	11.00	37.00	*****
8.00	12.00	49.00	*****
8.50	14.00	63.00	*****
9.00	8.00	71.00	*****
9.50	8.00	79.00	*****
10.00	6.00	85.00	*****
10.50	5.00	90.00	*****
11.00	6.00	96.00	*****
11.50	4.00	100.00	****
12.00			

MEAN ST. DEV. SKEWNESS KURTOSIS

8.16	1.70	0.01	-0.65	KRUMBEIN+PETTICORN(1938) MOMENT MEASURES FOR SIZE RANGE 4.5 TO 11.5 PHI
8.37	1.89	0.12	1.20	FOLK GRAPHIC STATISTICAL PARAMETERS FOLK AND WARD, 1957

PERCENTILES	MEDIAN	8.15	5TH	5.33	16TH	6.50	25TH	7.05
			75TH	9.67	84TH	10.42	95TH	11.42

PER CENT GRAVEL 0.00 SAND 1.00 SILT 0.0 (56.00) CLAY 0.0 (43.00)

GRAVEL + SAND 1.00 SILT/(SILT+CLAY) 56.37PCT GRAV+SAND/SILT+CLAY 0.01

LABELS SHEPARD -CLAYY SILT FOLK(GMS)-MUD (SCS)-MUD

PITT27A

## SEDIGRAPH ANALYSIS

PHI	PCT. CUMPT.			
4.00	0.0			
4.50	2.00	0.0	**	
5.00	3.00	2.00	***	
5.50	4.00	5.00	****	
6.00	6.00	9.00	*****	
6.50	7.00	15.00	*****	
7.00	9.00	22.00	*****	
7.50	11.00	31.00	*****	
8.00	8.00	42.00	*****	
8.50	9.00	50.00	*****	
9.00	8.00	59.00	*****	
9.50	5.00	67.00	*****	
10.00	6.00	72.00	*****	
10.50	5.00	78.00	*****	
11.00	5.00	83.00	*****	
11.50	6.00	88.00	*****	
12.00	6.00	94.00	*****	
12.00	100.00			
MEAN	ST.DEV.	SKWNESS	KUPTOSIS	
8.44	1.85	0.05	-0.83	KRUMBEIN+PETT (JOHN) (1938) MOMENT MEASURES FOR SIZE RANGE 4.5 TO 12.0 PHI
8.72	2.12	0.11	1.10	FOLK GRAPHIC STATISTICAL PARAMETERS FOLK AND WARD, 1957
PERCENTILES	MEDIAN	2.50	5TH 5.50	16TH 6.57
			75TH 10.25	25TH 7.17
			84TH 11.10	95TH 12.00
PER CENT GRAVEL	0.00	SAND	0.0	SILT 0.0 ( 50.00)
				CLAY 0.0 ( 50.00)
GRAVEL + SAND	0.00	SILT/(SILT+CLAY)	50.00PCT	GRAV+SAND/SILT+CLAY 0.00

LABELS SHEPARD -CLAYEY SILT FOLK (GMS)-MUD

(SCS)-MUD

PITT27B

## SEDIGRAPH ANALYSIS

PHI	PCT.	CUMPT.		
4.00				
4.50	0.0	0.0		
5.00	3.00	3.00	***	
5.50	4.00	7.00	****	
6.00	5.00	12.00	*****	
6.50	6.00	18.00	*****	
7.00	7.00	25.00	*****	
7.50	9.00	34.00	*****	
8.00	9.00	43.00	*****	
8.50	9.00	52.00	*****	
9.00	8.00	60.00	*****	
9.50	5.00	65.00	*****	
10.00	6.00	71.00	*****	
10.50	5.00	77.00	*****	
11.00	5.00	82.00	*****	
11.50	6.00	87.00	*****	
12.00	5.00	93.00	*****	
12.50	2.00	98.00	**	
12.00		100.00		
MEAN	ST.DEV.	SKEWNESS	KURTOSIS	
8.53	2.07	0.06	-0.96	KRUMBEIN+PETTICORN(1938) MOMENT MEASURES FOR SIZE RANGE 4.5 TO 12.5 PHI
8.64	2.27	0.13	1.20	FOLK GRAPHIC STATISTICAL PARAMETERS FOLK AND WARD, 1957
PERCENTILES	MEDIAN	8.39	5TH 5.25	16TH 6.33
			75TH 10.33	84TH 11.20
				95TH 12.20
PER CENT	GRAVEL	0.00	SAND	0.0
			SILT	0.0 ( 52.00)
			CLAY	0.0 ( 48.00)

GRAVEL + SAND 0.00 SILT/(SILT+CLAY) 52.00PCT GRAV+SAND/(SILT+CLAY) 0.00

PL++ 29 0 0.0 0 0.0 0

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 \*\*\* MULTIMODAL SAMPLE \*\*\*  
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WET WT	DRY WT	SALT	ORGANIC	MOISTURE	WEIGHT LOSS DUE TO HANDLING	0.0
1000.000	5.7300	0.0	0.0	0.0 (GRAMS)	GRAVEL CORRECTION FACTOR	1.000
99.9999	100.0000	0.0	0.0	0.0 (PCT WET WT)	SIZES ELIMINATED (KJ. J13)	NONE
					TRASK SORTING COEFFICIENT	2.233
					USING PROBABILITY EXTRAP.	2.200
					MEAN CUBED DEVIATION	11.488
					USING PROBABILITY EXTRAP.	9.666

PERCENTAGE COMPOSITION		TABLE OF STATISTICAL DATA IN PHI UNITS				PERCENTILES		LINEAR EXTRAP.		PROBABILITY EXTRAP.	
		MEAN	STD DEV	SKEWNESS	KURTOSIS	MM.	PHI UNITS	MM.	PHI UNITS		
GRAVEL	0.0	MOMENT 4.72744	1.96908	1.50475	5.33991	5.0	0.15522	2.68760	0.14373	2.79854	
SAND	47.62	MOMENT 4.73245	1.90676	1.42318	4.75920	10.0	0.13147	2.98722	0.12826	2.96284	
SILT	44.15	MEAN 4.51920	1.77215	0.47820	1.11145	10.0	0.11675	3.09049	0.11428	3.12458	
CLAY	7.99	MEAN 4.52651	1.74455	0.49838	1.11090	25.0	0.10179	3.29052	0.09835	3.33138	
MJD	52.18	MEAN 4.73787	1.63937	0.40016	0.91726	50.0	0.05905	4.08186	0.05909	4.08090	
S/M	0.92	MEAN 4.74924	1.61591	0.41257	0.90392	75.0	0.02041	5.61431	0.02052	5.60701	
		KURTOSIS 1.71703	0.37345	0.25866		84.0	0.01203	6.37724	0.01210	6.38920	
		P-KURT. 1.68565	0.38824	0.25031		90.0	0.00589	7.40800	0.00591	7.40204	
		POK (TRANSFORMED)		0.52639		95.0	0.00199	8.97383	0.00200	8.96883	
		P-POK (TRANSFORMED)		0.52627							

DATA FOR CONSTN OF PARAGRAPHS AND CUM. CURVES

SIZE FRACTION	WT.(GMS)	WT.PCT.	WT.PCT.	MID PHI(LINEAR)	MID PHI(PROB.)	MODE
MM	PHI	UNCOR	COR	PHI	MM	
0.250000	2.000	0.020	0.020	0.349	0.29707	0
0.177000	2.468	0.040	0.040	0.658	0.21036	0
0.125000	3.000	0.600	0.600	10.471	0.14875	0
0.091000	3.500	1.320	1.320	23.037	0.10488	1
0.067000	4.000	0.760	0.760	13.264	0.07416	0
0.044000	4.500	0.773	0.773	13.491	0.05244	1
0.021000	5.012	0.020	0.020	0.353	0.03693	0
0.022000	5.506	0.671	0.671	11.715	0.02612	1
0.015000	6.002	0.427	0.427	7.455	0.01853	0
0.011000	6.506	0.244	0.244	4.259	0.01310	0
0.007000	7.002	0.183	0.183	3.195	0.00926	0
0.005000	7.506	0.122	0.122	2.129	0.00655	0
0.003000	8.002	0.092	0.092	1.598	0.00463	0
0.002700	8.503	0.092	0.092	1.598	0.00325	1
0.001800	9.000	0.051	0.051	1.597	0.00227	0
0.001300	9.501	0.061	0.061	1.065	0.00162	0
0.000900	9.995	0.061	0.061	1.065	0.00116	0
0.000600	10.501	0.061	0.061	1.065	0.00082	0
0.000400	10.995	0.031	0.031	0.533	0.00058	0
0.000001	14.000	0.061	0.061	1.065	0.00017	0
TOTALS		5.730	5.730	100.0		

PI\*\* 30 0 0.0 0 0.0 0

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 \*\*\* MULTIMODAL SAMPLE \*\*\*  
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WET WT	DRY WT	SALT	ORGANIC	MOISTURE	WEIGHT LOSS DUE TO HANDLING	0.0
100.0000	5.8000	0.0	0.0	0.0 (GRAMS)	GRAVEL CORRECTION FACTOR	1.000
100.0000	106.0000	0.0	0.0	0.0 (PCT WET WT)	SIZES ELIMINATED (<0.01%)	NONE
					TRASK SORTING COEFFICIENT	2.001
					USING PROBABILITY EXTRAP.	1.988
					MEAN CUBED DEVIATION	11.522
					USING PROBABILITY EXTRAP.	6.508

PERCENTAGE COMPOSITION		TABLE OF STATISTICAL DATA IN PHI UNITS				PERCENTILES		LINEAR EXTRAP.		PROBABILITY EXTRAP.	
		MEAN	STD	COV	SKEWNESS	KURTOSIS		MM.	PHI UNITS	MM.	PHI UNITS
GRAVEL	0.0	4.88812	1.88910	1.70917	6.52770		5.0	0.13433	2.84616	0.13042	2.93874
SAND	38.28	4.85164	1.70458	1.31409	4.59443		10.0	0.11450	3.12857	0.11062	3.17834
SILT	54.79	4.65156	1.59984	0.39850	1.19719		16.0	0.10026	3.31811	0.09715	3.36862
CLAY	6.93	4.62290	1.57862	0.41214	1.19851		25.0	0.08248	3.54987	0.08164	3.61897
MUD	01.72	4.80498	1.48688	0.30955	0.90071		50.0	0.04922	4.34471	0.04917	4.34598
SYM	0.62	4.82146	1.45783	0.32615	0.92342		75.0	0.02059	5.60169	0.02069	5.59489
			1.48283	0.25607	0.24474		84.0	0.01276	6.29186	0.01287	6.27925
			1.46957	0.25695	0.24642		90.0	0.00672	7.21628	0.00679	7.20185
					0.53043		95.0	0.00267	8.54840	0.00267	8.54830
					0.53672						

DATA FOR CONSTN OF BARGRAPHS AND LIM. CURVES

SIZE FRACTION	WT. (GMS)	WT. PCT.	WT. PCT.	MID PHI (LINEAR)	MID PHI (PROB.)	MODE				
MM	PHI	UNCOR	CCR	CCR	CUMUL.	PHI	MM	PHI	MM	
0.250000	2.000	0.030	0.030	0.517	0.517	1.751	0.29707	1.903	0.26745	0
0.177000	2.498	0.030	0.030	0.517	1.034	2.249	0.21036	2.286	0.20489	0
0.125000	3.000	0.290	0.290	5.000	6.034	2.749	0.14875	2.832	0.14048	0
0.087500	3.500	0.920	0.920	15.802	21.837	3.253	0.10488	3.307	0.10107	0
0.062500	4.000	0.950	0.950	16.379	28.776	3.753	0.07416	3.769	0.07337	0
0.045000	4.500	0.999	0.999	17.221	59.457	4.253	0.05244	4.255	0.05230	1*
0.032500	5.012	0.280	0.280	4.873	68.330	4.759	0.03693	4.757	0.03687	0
0.022500	5.500	0.767	0.767	13.227	73.547	5.259	0.02612	5.249	0.02630	1
0.015000	6.000	0.438	0.438	7.999	81.195	5.754	0.01853	5.743	0.01868	0
0.010000	6.500	0.292	0.292	5.959	86.144	6.254	0.01310	6.242	0.01322	0
0.007500	7.000	0.146	0.146	2.919	88.663	6.754	0.00926	6.746	0.00932	0
0.005000	7.500	0.185	0.185	3.149	91.812	7.254	0.00655	7.239	0.00662	1
0.003500	8.000	0.073	0.073	1.259	93.072	7.754	0.00463	7.746	0.00466	0
0.002700	8.500	0.110	0.110	1.650	94.561	8.268	0.00325	8.251	0.00328	1
0.001900	9.000	0.073	0.073	1.259	96.221	8.786	0.00227	8.772	0.00229	0
0.001375	9.500	0.037	0.037	0.630	98.851	9.270	0.00162	9.262	0.00163	0
0.001000	14.000	0.183	0.183	3.149	100.000	11.751	0.00029	10.203	0.00085	0
TOTAL		5.800	5.800	100.0						
0.250000	0.320000									
0.177000	0.630000									
0.125000	1.570000									



P1++ 31A 0 0.0 0 0.0 0

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 \*\*\* MULTIMODAL SAMPLE \*\*\*  
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WET WT	DRY WT	SALT	ORGANIC	MOISTURE	WEIGHT LOSS DUE TO HANDLING	0.0
1000.0000	4.5200	0.0	0.0	0.0 (GRAMS)	GRAVEL CORRECTION FACTOR	1.000
100.0000	100.0000	0.0	0.0	0.0 (PCT WET WT)	SIZES ELIMINATED (<0.01%)	NONE
					TRASK SORTING COEFFICIENT	1.250
					USING PROBABILITY EXTRAP.	1.216
					MEAN CUBED DEVIATION	8.121
					USING PROBABILITY EXTRAP.	7.353

PERCENTAGE COMPOSITION		TABLE OF STATISTICAL DATA IN PHI UNITS				PERCENTILES		LINEAR EXTRAP.		PROBABILITY EXTRAP.	
		MEAN	STD DEV	SKWENESS	KURTOSIS		MM.	PHI UNITS	MM.	PHI UNITS	
GRAVEL	0.0	3.43493	1.24395	4.21908	24.84883	5.0	0.17023	2.55442	0.15758	2.66584	
SAND	90.93	3.46090	1.19926	4.26338	24.36111	10.0	0.16192	2.62666	0.14757	2.76052	
SILT	7.06	3.21719	0.70759	0.34727	1.87162	16.0	0.19248	2.71334	0.14011	2.83535	
CLAY	2.01	3.24288	0.65056	0.44671	2.05238	25.0	0.13933	2.84337	0.13224	2.91873	
MUD	9.07	3.23773	0.52439	0.11751	1.80293	50.0	0.11064	3.17611	0.11118	3.18898	
S/M	10.02	3.27983	0.44448	0.24938	2.18001	75.0	0.08918	3.48707	0.08942	3.48324	
			0.47682	-0.01089	0.23993	84.0	0.07370	3.76212	0.07566	3.72431	
			0.41815	0.03200	0.23615	90.0	0.06390	3.96808	0.06445	3.95575	
					0.65176	95.0	0.02219	5.49407	0.02221	5.49277	
					0.67239						

DATA FOR CONSTN OF BARGRAPHS AND CUM. CURVES

SIZE FRACTION	WT.(GMS)	WT.PCT.	WT.PCT.	MID PHI(LINEAR)	MID PHI(PROB.)	MODE				
MM	PHI	UNCOR	COR	COR	CUMUL.	PHI	MM	PHI	MM	
0.250000	2.000	0.020	0.020	0.442	0.442	1.751	0.29707	1.900	0.26794	0
0.177300	2.498	0.030	0.030	0.664	1.106	2.249	0.21036	2.298	0.20337	0
0.125000	3.000	1.570	1.570	34.735	35.841	2.749	0.14875	2.061	0.13768	0
0.082000	3.506	1.840	1.840	40.708	76.549	3.253	0.10488	3.242	0.10572	1
0.062500	4.000	0.650	0.650	14.381	90.929	3.753	0.07416	3.716	0.07611	0
0.044000	4.506	0.052	0.052	1.146	92.075	4.253	0.05244	4.247	0.05267	0
0.031000	5.012	0.069	0.069	1.925	93.603	4.759	0.03693	4.749	0.03720	1
0.022000	5.506	0.065	0.065	1.435	95.036	5.259	0.02612	5.247	0.02534	0
0.015600	6.002	0.043	0.043	0.955	95.990	5.754	0.01853	5.744	0.01866	0
0.011900	6.500	0.030	0.030	0.668	96.858	6.254	0.01310	6.245	0.01319	0
0.007800	7.002	0.026	0.026	0.573	97.231	6.754	0.00926	6.745	0.00933	0
0.005500	7.506	0.017	0.017	0.382	97.613	7.254	0.00655	7.246	0.00659	0
0.003900	8.002	0.017	0.017	0.382	97.995	7.754	0.00463	7.745	0.00466	0
0.002700	8.503	0.017	0.017	0.383	98.377	8.268	0.00325	8.256	0.00327	1
0.001900	9.040	0.009	0.009	0.190	98.568	8.786	0.00227	8.779	0.00228	0
0.001300	9.501	0.013	0.013	0.287	98.854	9.270	0.00162	9.259	0.00163	1
0.000980	9.995	0.009	0.009	0.191	99.045	9.748	0.00116	9.738	0.00117	0
0.000650	10.501	0.009	0.009	0.190	99.236	10.248	0.00082	10.236	0.00083	0
0.000490	10.995	0.009	0.009	0.191	99.427	10.748	0.00058	10.732	0.00059	1
0.000340	11.522	0.009	0.009	0.191	99.618	11.259	0.00041	11.235	0.00041	1
0.000061	14.000	0.017	0.017	0.382	100.000	12.761	0.00014	12.034	0.00024	0

TOTALS 4.520 4.520 100.0

PI\*\* 318 0 0.0 0 0.0 0

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 \*\*\* MULTIMODAL SAMPLE \*\*\*  
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WET WT	DRY WT	SALT	ORGANIC	MOISTURE	WEIGHT LOSS DUE TO HANDLING	0.0
1000.0000	3.8200	0.0	0.0	0.0 (GRAMS)	GRAVEL CORRECTION FACTOR	1.000
100.0001	100.0000	0.0	0.0	0.0 (PCT WET WT)	SIZES ELIMINATED (<0.01%)	NONE
					TRASK SORTING COEFFICIENT	2.305
					USING PROBABILITY EXTRAP.	2.286
					MEAN CURVED DEVIATION	21.826
					USING PROBABILITY EXTRAP.	18.351

PERCENTAGE COMPOSITION TABLE OF STATISTICAL DATA IN PHI UNITS PERCENTILES LINEAR EXTRAP. PROBABILITY EXTRAP.

PERCENTAGE COMPOSITION		TABLE OF STATISTICAL DATA IN PHI UNITS				PERCENTILES		LINEAR EXTRAP.		PROBABILITY EXTRAP.	
		MEAN	STD DEV	SKEWNESS	KUPTOSIS		MM.	PHI UNITS	MM.	PHI UNITS	
GRAVEL	0.0	5.09407	2.36776	1.64424	5.70868	5.0	0.15981	2.64558	0.14829	2.75345	
SAND	37.70	5.08708	2.27659	1.55528	5.22502	10.0	0.13915	2.84526	0.13270	2.91571	
SILT	51.91	4.80978	2.17330	0.42492	1.36110	18.0	0.11846	3.07756	0.11716	3.09348	
CLAY	10.40	4.81427	2.15129	0.43737	1.35515	25.0	0.09434	3.40602	0.09340	3.42055	
MUD	62.30	4.99939	1.92183	0.29598	1.08180	50.0	0.04637	4.43057	0.04634	4.43158	
S/M	0.61	5.00561	1.91213	0.30021	1.00275	75.0	0.01776	5.81540	0.01787	5.80005	
			1.78472	0.18014	0.22896	84.0	0.00825	6.92122	0.00827	6.91774	
			1.76719	0.18163	0.22997	90.0	0.00363	8.10677	0.00364	8.10060	
					0.57647	95.0	0.00062	10.64733	0.00063	10.64193	
					0.57540						

DATA FOR CONSTN OF BARGRAPHS AND CUM. CURVES

SIZE FRACTION	WT.(GMS)	WT.PCT.	WT.PCT.	MID PHI(LINEAR)	MID PHI(PROB.)	MODE
MM	PHI	UNCOR	COR	PHI	MM	PHI
0.250000	2.000	0.010	0.010	0.262	0.262	0
0.177000	2.498	0.040	0.040	1.047	1.309	0
0.125000	3.000	0.480	0.480	12.565	13.874	0
0.081500	3.500	0.530	0.530	13.874	27.749	1
0.062500	4.000	0.380	0.380	9.948	37.696	0
0.044000	4.500	0.553	0.553	14.469	52.105	1*
0.021000	5.012	0.216	0.216	5.651	57.816	0
0.022000	5.506	0.471	0.471	12.331	70.147	0
0.015600	6.002	0.297	0.297	7.788	77.935	0
0.011000	6.586	0.149	0.149	3.894	81.829	0
0.007800	7.002	0.099	0.099	2.596	84.424	0
0.005500	7.566	0.099	0.099	2.596	87.020	0
0.003900	8.002	0.099	0.099	2.597	89.617	1
0.002700	8.533	0.074	0.074	1.946	91.563	0
0.001900	9.040	0.050	0.050	1.298	92.861	0
0.001300	9.501	0.025	0.025	0.649	95.511	0
0.000980	9.995	0.025	0.025	0.649	94.160	1
0.000690	10.501	0.025	0.025	0.648	94.808	0
0.000490	10.995	0.025	0.025	0.649	95.457	0
0.000340	11.522	0.025	0.025	0.649	96.106	0
0.000240	12.025	0.025	0.025	0.649	96.755	0

0.000061 14.000 0.124 0.124 3.245 100.000 13.012 0.00012 12.332 0.00015 0  
 TOTALS 3.820 3.820 100.0

PITT 32 0 0.0 0 0.0 0

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 MULTIMODAL SAMPLE  
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WET WT	DPY WT	SALT	ORGANIC	MOISTURE	WEIGHT LOSS DUE TO HANDLING	0.0
1000.0000	4.4500	0.0	0.0	0.0 (GRAMS)	GRAVEL CORRECTION FACTOR	1.000
100.0000	100.0000	0.0	0.0	0.0 (PCT WET WT)	SIZES ELIMINATED (<0.01%)	NONE
					TRASK SORTING COEFFICIENT	2.460
					USING PROBABILITY EXTRAP.	2.453
					MEAN CUBED DEVIATION	18.075
					USING PROBABILITY EXTRAP.	15.011

PERCENTAGE COMPOSITION	TABLE OF STATISTICAL DATA IN PHI UNITS					PERCENTILES	LINEAR EXTRAP.	PROBABILITY EXTRAP.	
	MEAN	STD DEV	SKWNESS	KURTOSIS		MM.	PHI UNITS	MM.	PHI UNITS
GRAVEL 0.0	5.62304	2.41749	1.27933	3.93355	5.0	0.11540	3.11422	0.11086	3.17312
SAND 27.64	5.60987	2.32965	1.16720	3.50748	10.0	0.09546	3.38901	0.09297	3.42713
SILT 55.37	5.62875	2.31720	0.45063	1.21012	16.0	0.08081	3.62939	0.07935	3.65563
CLAY 16.99	5.63546	2.29816	0.45967	1.20571	25.0	0.06625	3.91592	0.06559	3.93047
MUD 72.36	5.93345	2.30406	0.39674	0.66882	50.0	0.03083	5.01934	0.03064	5.01921
S/M 0.38	5.64359	2.28796	0.40402	0.66472	75.0	0.01089	6.52036	0.01090	6.51979
	KPUMFEIN	1.92921	0.19879	0.21047	84.0	0.00331	8.23751	0.00333	8.23154
	P-KFUM.	1.91802	0.20592	0.21073	90.0	0.00131	9.57623	0.00131	9.57084
	FOLK (TRANSFORMED)			0.54754	95.0	0.00056	10.80435	0.00056	10.79072
	P-FOLK (TRANSFORMED)			0.54663					

DATA FOR CONSTN OF BARGRAPHS AND CUM. CURVES

SIZE FRACTION	WT.(GMS)	WT.PCT.	WT.PCT.	MID PHI(LINEAR)	MID PHI(PROB.)	MODE
MM	PHI	UNCOR	COR	PHI	MM	PHI
0.250000	2.000	0.010	0.010	0.225	0.225	1.751
0.177000	2.498	0.020	0.020	0.449	0.674	2.249
0.125000	3.000	0.100	0.100	2.247	2.921	2.749
0.098000	3.506	0.410	0.410	9.213	12.135	3.253
0.075000	4.000	0.690	0.690	15.506	27.640	3.753
0.044000	4.506	0.873	0.873	19.615	47.255	4.253
0.031000	5.012	0.113	0.113	2.536	49.791	4.759
0.022000	5.506	0.591	0.591	13.291	63.082	5.259
0.015600	6.002	0.329	0.329	7.383	70.465	5.754
0.011000	6.506	0.197	0.197	4.430	74.896	6.254
0.007800	7.002	0.164	0.164	3.692	78.588	6.754
0.005500	7.506	0.099	0.099	2.215	80.802	7.254
0.003900	8.002	0.095	0.095	2.216	85.018	7.754
0.002700	8.533	0.095	0.095	2.215	85.233	8.268
0.001900	9.040	0.099	0.099	2.216	87.448	8.785
0.001300	9.501	0.099	0.099	2.215	89.663	9.270
0.000900	9.995	0.099	0.099	2.215	91.878	9.748
0.000600	10.501	0.099	0.099	2.216	94.093	10.248
0.000400	10.995	0.066	0.066	1.476	95.570	10.748
0.000340	11.522	0.066	0.066	1.476	97.046	11.259
0.000261	14.000	0.131	0.131	2.954	100.000	12.761

TOTALS 4.450 4.450 100.0

PI++ 33 0 0.0 0 0.0 0

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 \*\*\* MULTIMODAL SAMPLE \*\*\*  
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WET WT	DRY WT	SALT	ORGANIC	MOISTURE	WEIGHT LOSS DUE TO HANDLING	0.0
1000.0000	4.6700	0.0	0.0	0.0 (GRAMS)	GRAVEL CORRECTION FACTOR	1.000
100.0000	100.0000	0.0	0.0	0.0 (PCT WET WT)	SIZES ELIMINATED (NO. SIZES)	NONE
					TRASK SORTING COEFFICIENT	2.118
					USING PROBABILITY EXTRAP.	2.118
					MEAN CUBED DEVIATION	14.358
					USING PROBABILITY EXTRAP.	10.698

PERCENTAGE COMPOSITION	TABLE OF STATISTICAL DATA IN PHI UNITS				PERCENTILES		LINEAR EXTRAP.		PROBABILITY EXTRAP.	
	MEAN	STD DEV	SKEWNESS	KURTOSIS	MM.	PHI UNITS	MM.	PHI UNITS		
GRAVEL 0.0	5.28558	2.09413	1.56290	5.58731	5.0	0.11956	3.06415	0.11990	3.10900	
SAND 30.84	5.26826	1.97827	1.38194	4.66799	10.0	0.10381	3.26890	0.09923	3.33314	
SILT 59.16	5.11205	1.88119	0.34786	1.26772	16.0	0.08769	3.51141	0.08762	3.51261	
CLAY 10.10	5.11207	1.87162	0.35223	1.26986	25.0	0.07141	3.80781	0.07040	3.87833	
MUD 69.16	5.24395	1.73253	0.22839	0.93315	50.0	0.03472	4.84825	0.03471	4.84848	
S/M 0.43	5.24386	1.73125	0.22838	0.91755	75.0	0.01592	5.97336	0.01594	5.97118	
		1.60411	0.04234	0.22769	84.0	0.00794	6.97648	0.00795	6.97511	
		1.58730	0.05127	0.22851	90.0	0.00384	8.02358	0.00385	8.02184	
				0.55903	95.0	0.00115	9.76269	0.00116	9.74993	
				0.55944						

DATA FOR CONSTN OF BARGRAPHS AND CUM. CURVES

SIZE FRACTION	WT.(GMS)		WT.PCT.		MID PHI(LINEAR)		MID PHI(PROB.)		MODE	
	MM	PHI	UNCOR	COR	PHI	MM	PHI	MM		
0.250000	2.500	0.010	0.010	0.214	0.214	1.751	0.29707	1.885	0.27579	0
0.177500	2.498	0.010	0.010	0.214	0.428	2.249	0.21036	2.287	0.20487	0
0.125000	3.000	0.140	0.140	2.998	3.426	2.749	0.14875	2.846	0.13906	0
0.088000	3.506	0.580	0.580	12.420	15.846	3.253	0.10488	3.320	0.10012	0
0.062500	4.000	0.700	0.700	14.989	30.835	3.753	0.07416	3.776	0.07301	1*
0.344000	4.506	0.655	0.655	14.336	44.872	4.253	0.05244	4.260	0.05218	0
0.250000	5.012	0.354	0.354	7.978	52.490	4.759	0.03693	4.759	0.03692	0
0.224000	5.500	0.673	0.673	14.499	66.859	5.259	0.02612	5.253	0.02522	1
0.018000	6.002	0.404	0.404	8.846	75.504	5.754	0.01853	5.745	0.01864	0
0.011000	6.500	0.265	0.265	5.763	81.268	6.254	0.01310	6.245	0.01319	0
0.007800	7.002	0.135	0.135	2.882	84.150	6.754	0.00926	6.748	0.00921	0
0.005000	7.500	0.135	0.135	2.882	87.032	7.254	0.00659	7.246	0.00659	0
0.003000	8.002	0.135	0.135	2.881	89.913	7.754	0.00463	7.743	0.00467	0
0.002000	8.503	0.101	0.101	2.162	92.075	8.268	0.00325	8.256	0.00327	0
0.001000	9.000	0.034	0.034	0.721	92.796	8.786	0.00227	8.782	0.00227	0
0.001000	9.501	0.067	0.067	1.441	94.237	9.270	0.00162	9.260	0.00163	1
0.000800	9.995	0.067	0.067	1.441	95.678	9.748	0.00116	9.734	0.00117	1
0.000400	10.501	0.034	0.034	0.719	96.397	10.248	0.00082	10.239	0.00083	0
0.000400	10.995	0.034	0.034	0.721	97.118	10.748	0.00058	10.737	0.00059	0
0.000001	14.000	0.135	0.135	2.882	100.000	12.497	0.00017	11.467	0.00035	0
TOTALS		4.670		4.670	100.00					

Pl++ 35 0 0.0 0 0.0 0

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 \*\*\* MULTIMODAL SAMPLE \*\*\*  
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WET WT DRY WT SALT ORGANIC MOISTURE  
 1000.0000 3.8600 0.0 0.0 0.0 (GRAMS)  
 100.0000 100.0000 0.0 0.0 0.0 (PCT WET WT)

WEIGHT LOSS DUE TO HANDLING 0.0  
 GRAVEL CORRECTION FACTOR 1.000  
 SIZES ELIMINATED (<0.01%) NONE  
 TRASK SORTING COEFFICIENT 2.294  
 USING PROBABILITY EXTRAP. 2.281  
 MEAN CUBED DEVIATION 14.690  
 USING PROBABILITY EXTRAP. 10.240

PERCENTAGE COMPOSITION	TABLE OF STATISTICAL DATA IN PHI UNITS					PERCENTILES LINEAR EXTRAP.		PROBABILITY EXTRAP.	
	MEAN	STD DEV	SKEWNESS	KURTOSIS		MM.	PHI UNITS	MM.	PHI UNITS
GRAVEL 0.0	5.26064	2.19625	1.38670	4.72712	5.0	0.13101	2.93224	0.12768	2.96714
SAND 33.16	5.25327	2.05477	1.18032	3.79626	10.0	0.11305	3.14491	0.10897	3.19759
SILT 54.66	5.10409	2.02668	0.38567	1.19081	16.0	0.09827	3.34710	0.09551	3.38813
CLAY 12.16	5.11484	2.00770	0.39520	1.19153	25.0	0.07824	3.67603	0.07749	3.68991
MUD 66.84	5.29069	1.94359	0.28802	0.79108	50.0	0.03760	4.73089	0.03766	4.73283
S/M 0.50	5.30685	1.91872	0.50021	0.80304	75.0	0.01486	6.07219	0.01490	6.06896
		1.77494	0.14322	0.22139	84.0	0.00664	7.23428	0.00663	7.22557
		1.76226	0.14860	0.22208	90.0	0.00266	8.55661	0.00266	8.55420
				0.54355	95.0	0.00105	9.89451	0.00106	9.88617
				0.54378					

DATA FOR CONSTN OF BARGRAPHS AND CUM. CURVES

SIZE FRACTION MM	PHI	WT.(GMS) UNCOR	WT.(GMS) COR	WT.PCT. COR	WT.PCT. CUMUL.	MID PHI(LINEAR) PHI	MID PHI(LINEAR) MM	MID PHI(PKCB.) PHI	MID PHI(PKCB.) MM	MODE
0.250000	2.000	0.010	0.010	0.259	0.259	1.751	0.29707	1.889	0.26955	0
0.177000	2.458	0.010	0.010	0.259	0.518	2.249	0.21036	2.287	0.20489	0
0.125000	3.000	0.200	0.200	5.181	5.699	2.749	0.14875	2.855	0.13024	0
0.088000	3.500	0.580	0.580	15.026	20.725	3.253	0.10488	3.307	0.10101	1
0.062500	4.000	0.480	0.480	12.435	33.161	3.753	0.07416	3.768	0.07342	0
0.044000	4.506	0.545	0.545	14.108	47.268	4.253	0.05244	4.259	0.05223	1
0.031000	5.012	0.237	0.237	6.146	53.415	4.759	0.03623	4.759	0.03594	0
0.022000	5.506	0.495	0.495	12.828	66.242	5.259	0.02612	5.254	0.02521	1
0.015600	6.002	0.313	0.313	8.102	74.345	5.754	0.01853	5.747	0.01863	0
0.011000	6.506	0.182	0.182	4.725	79.070	6.254	0.01310	6.247	0.01316	0
0.007800	7.002	0.130	0.130	3.376	82.446	6.754	0.00926	6.748	0.00921	0
0.005500	7.506	0.130	0.130	3.377	85.823	7.254	0.00655	7.245	0.00659	1
0.003900	8.002	0.078	0.078	2.025	87.847	7.754	0.00463	7.748	0.00465	0
0.002700	8.533	0.078	0.078	2.026	89.873	8.268	0.00325	8.259	0.00326	0
0.001900	9.040	0.104	0.104	2.701	92.574	8.786	0.00227	8.772	0.00229	1
0.001300	9.561	0.052	0.052	1.350	93.924	9.270	0.00162	9.261	0.00163	0
0.000980	9.995	0.052	0.052	1.351	95.275	9.748	0.00116	9.736	0.00117	1
0.000690	10.501	0.052	0.052	1.350	96.624	10.248	0.00082	10.231	0.00083	0
0.000001	14.000	0.130	0.130	3.376	100.000	12.251	0.00021	11.044	0.00047	0
TOTALS		3.860	3.860	100.0						
0.250000	0.010000									

P1++ 36 0 0.0 0 0.0 0

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 \*\*\*\* MULTIMODAL SAMPLE \*\*\*\*  
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WET WT	OPY WT	SALT	ORGANIC	MOISTURE	WEIGHT LOSS DUE TO HANDLING	0.0
1000.0000	3.9100	0.0	0.0	0.0 (GRAMS)	GRAVEL CORRECTION FACTOR	1.000
100.0001	100.0000	0.0	0.0	0.0 (PCT WET WT)	SIZES ELIMINATED (<0.01%)	NONE
					TRASK SORTING COEFFICIENT	2.714
					USING PROBABILITY EXTRAP.	2.698
					MEAN CUBED DEVIATION	20.675
					USING PROBABILITY EXTRAP.	18.217

PERCENTAGE COMPOSITION	TABLE OF STATISTICAL DATA IN PHI UNITS					PERCENTILES		LINEAR EXTRAP.		PROBABILITY EXTRAP.	
	MEAN	STD	DEV	SKEWNESS	KURTOSIS	MM.	PHI UNITS	MM.	PHI UNITS		
GRAVEL 0.0	6.04913	2.57011	1.22959	3.95281	5.0	0.10952	3.19077	0.10439	3.25989		
SAND 20.46	4.02790	2.49830	1.16822	3.68918	10.0	0.08654	3.53044	0.08609	3.53795		
SILT 59.85	5.95107	2.54515	0.41997	1.24959	16.0	0.07180	3.79977	0.07038	3.82368		
CLAY 19.69	5.96001	2.52622	0.42927	1.24683	25.0	0.05545	4.17272	0.05487	4.16784		
MUD 79.54	6.22810	2.42833	0.34224	0.80875	50.0	0.02373	5.39733	0.02371	5.39813		
S/M 0.26	6.24095	2.41228	0.34939	0.80588	75.0	0.00753	7.05383	0.00754	7.05169		
		2.13415	0.21625	0.22452	84.0	0.00248	8.65642	0.00248	8.65323		
		2.12137	0.22163	0.22352	90.0	0.00101	9.94670	0.00102	9.94418		
				0.55547	95.0	0.00025	11.97526	0.00025	11.97245		
				0.55493							

DATA FOR CONSTN OF BARGRAPHS AND CUM. CURVES

SIZE FRACTION	WT.(GMS)	WT.PCT.	WT.PCT.	MID PHI(LINEAR)	MID PHI(PROB.)	MODE
MM	PHI	UNCOR	COR	PHI	MM	MM
0.250000	2.000	0.010	0.010	0.256	0.256	1.751
0.177000	2.458	0.020	0.020	0.512	0.767	2.249
0.125000	3.000	0.060	0.060	1.535	2.302	2.749
0.088000	3.500	0.280	0.280	7.161	9.463	3.253
0.062500	4.000	0.430	0.430	10.997	20.460	3.753
0.044000	4.500	0.520	0.520	13.307	33.767	4.253
0.031000	5.012	0.185	0.185	4.733	38.500	4.759
0.022000	5.500	0.577	0.577	14.761	53.261	5.259
0.015600	6.002	0.417	0.417	10.660	63.921	5.754
0.011000	6.566	0.289	0.289	7.380	71.301	6.254
0.007800	7.002	0.128	0.128	3.280	74.581	6.754
0.005500	7.506	0.160	0.160	4.100	78.680	7.254
0.003900	8.002	0.064	0.064	1.639	80.320	7.754
0.002700	8.533	0.128	0.128	3.280	83.600	8.268
0.001900	9.040	0.064	0.064	1.641	85.241	8.766
0.001380	9.501	0.128	0.128	3.280	88.521	9.270
0.000980	9.995	0.064	0.064	1.639	90.160	9.748
0.000650	10.501	0.064	0.064	1.641	91.801	10.248
0.000450	10.995	0.064	0.064	1.639	93.440	10.748
0.000340	11.522	0.032	0.032	0.820	94.260	11.259
0.000240	12.025	0.032	0.032	0.821	95.081	11.773

0.000170	12.522	0.032	0.032	0.820	95.900	12.273	0.00020	12.264	0.00020	0
0.000061	14.000	0.160	0.160	4.100	100.000	13.261	0.00010	12.749	0.00015	0
TOTALS		3.910	3.910	100.0						

PI# 37 0 0.0 0 0.0 0

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 \*\*\* MULTIMODAL SAMPLE \*\*\*  
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WET WT	DRY WT	SALT	ORGANIC	MOISTURE	WEIGHT LOSS DUE TO HANDLING	0.0
1000.0000	4.5900	0.0	0.0	0.0 (GRAMS)	GRAVEL CORRECTION FACTOR	1.000
100.0000	100.0000	0.0	0.0	0.0 (PCT WET WT)	SIZES ELIMINATED (<0.01%)	NONE
					TRASK SORTING COEFFICIENT	2.180
					USING PROBABILITY EXTRAP.	2.168
					MEAN CUBED DEVIATION	6.657
					USING PROBABILITY EXTRAP.	4.737

PERCENTAGE COMPOSITION		TABLE OF STATISTICAL DATA IN PHI UNITS				PERCENTILES		LINEAR EXTRAP.		PROBABILITY EXTRAP.	
		MEAN	STD DEV	SKEWNESS	KURTOSIS		MM.	PHI UNITS	MM.	PHI UNITS	
GRAVEL	0.0	5.57841	1.80635	1.12940	4.85231	5.0	0.10306	3.27848	0.09799	3.35118	
SAND	20.70	5.50605	1.72197	0.92777	3.85024	10.0	0.08309	3.58517	0.08151	3.61694	
SILT	69.58	5.44714	1.71080	0.19269	1.04429	16.0	0.07082	3.81959	0.06917	3.85365	
CLAY	9.73	5.45497	1.68749	0.20393	1.03772	25.0	0.05414	4.20710	0.05364	4.22044	
MUD	79.30	5.50452	1.68492	0.10215	0.70067	50.0	0.02482	5.33239	0.02479	5.33386	
S/M	0.26	5.51552	1.66187	0.10929	0.70087	75.0	0.01129	6.45626	0.01141	6.45313	
			1.66605	-0.00072	0.25742	84.0	0.00665	7.18544	0.00691	7.17738	
			1.65384	0.00290	0.25743	90.0	0.00402	7.95788	0.00403	7.95340	
					0.51083	95.0	0.00194	9.00949	0.00195	9.00443	
					0.50926						

DATA FOR CONSTN OF BARGRAPHS AND CUM. CURVES

SIZE FRACTION	WT.(GMS)		WT.PCT.		MID PHI(LINEAR)		MID PHI(PROB.)		MODE	
	MM	PHI	UNCOR	COR	COR	CUMUL.	PHI	MM		
0.250000	2.000	0.010	0.010	0.218	0.218	1.751	0.29707	1.885	0.27971	0
0.177000	2.498	0.020	0.020	0.436	0.654	2.249	0.21035	2.308	0.20200	0
0.125000	3.000	0.040	0.040	0.871	1.525	2.749	0.14875	2.794	0.14417	0
0.080000	3.506	0.290	0.290	6.518	7.843	3.253	0.10488	3.330	0.09945	0
0.062500	4.000	0.590	0.590	12.854	20.697	3.753	0.07416	3.793	0.07215	1
0.044000	4.506	0.483	0.483	10.520	31.217	4.253	0.05244	4.267	0.05156	0
0.031000	5.012	0.260	0.260	5.665	36.881	4.759	0.03693	4.763	0.03683	0
0.022000	5.506	0.925	0.925	20.231	57.112	5.259	0.02612	5.261	0.02607	1*
0.015600	6.002	0.520	0.520	11.329	68.441	5.754	0.01853	5.748	0.01860	0
0.011000	6.506	0.334	0.334	7.282	75.723	6.254	0.01310	6.246	0.01317	0
0.007500	7.002	0.297	0.297	6.474	82.197	6.754	0.00926	6.743	0.00934	0
0.005500	7.506	0.223	0.223	4.855	87.052	7.254	0.00655	7.241	0.00661	0
0.003900	8.062	0.149	0.149	3.237	90.290	7.754	0.00463	7.742	0.00467	0
0.002700	8.533	0.111	0.111	2.427	92.717	8.268	0.00325	8.253	0.00328	0
0.001900	9.040	0.111	0.111	2.426	95.145	8.786	0.00227	8.766	0.00230	1
0.001350	9.561	0.074	0.074	1.619	96.764	9.270	0.00162	9.262	0.00164	0
0.000980	9.995	0.037	0.037	0.808	97.572	9.748	0.00116	9.733	0.00117	0
0.000690	10.501	0.037	0.037	0.809	98.381	10.248	0.00082	10.226	0.00083	0
0.000061	14.000	0.074	0.074	1.619	100.000	12.251	0.00021	11.083	0.00346	0
TOTALS										
0.250000	0.010000	4.590	4.590	100.0						

PITT38

SIEVE, SH. PIP., SEDIGRAPH SAMPLE WT.= 6.3100

PHI	PCT.	CUMPCT.		
1.50				
2.00	0.48	0.48		
2.50	0.32	0.79		
	1.27		*	
3.00		2.06		
	4.75		*****	
3.50		6.81		
	7.61		*****	
4.00		14.42		
	8.64		*****	
4.50		23.07		
	15.56		*****	
5.00		38.63		
	18.15		*****	
5.50		56.78		
	11.24		*****	
6.00		68.02		
	8.64		*****	
6.50		76.66		
	5.19		*****	
7.00		81.85		
	5.19		*****	
7.50		87.03		
	4.32		****	
8.00		91.36		
	3.46		***	
8.50		94.81		
	3.46		***	
9.00		98.27		
	1.73		**	
12.00		100.00		
MEAN ST. DEV. SKEWNESS KURTOSIS				
5.48	1.44	0.19	-0.21	KRUMBEIN+PETTICORN (1958) MOMENT MEASURES FOR SIZE RANGE 2.0 TO 9.0 PHI
5.54	1.57	0.22	1.22	FOLK GRAPHIC STATISTICAL PARAMETERS FOLK AND WARD, 1957
PERCENTILES				
MEDIAN	5.31	5TH	3.31	16TH 4.09 25TH 4.56
		75TH	6.40	84TH 7.21 95TH 8.53
PER CENT GRAVEL 0.0 SAND 14.42 SILT 77.26 (76.93) CLAY 8.32 (8.64)				
GRAVEL + SAND 14.42 SILT/(SILT+CLAY) 89.90PCT GRAV+SAND/SILT+CLAY 0.17				
LABELS SHEPARD -SILT FOLK (GMS)-SANDY MUD (SCS)-SANDY SILT				



PITT39

SIEVE, SH. PIP., SEDIGRAPH SAMPLE WT.= 4.8000

PHI PCT. CUMPCT.

3.00	0.42		
3.50	1.67	0.42	**
4.00	1.96	2.08	**
4.50	2.94	4.04	***
5.00	7.83	6.98	*****
5.50	8.81	14.81	*****
6.00	10.77	23.63	*****
6.50	6.85	34.40	*****
7.00	6.85	41.25	*****
7.50	7.83	48.10	*****
8.00	4.90	55.94	*****
8.50	2.94	60.83	***
9.00	11.75	63.77	*****
9.50	4.90	75.52	****
10.00	4.90	80.42	****
10.50	4.90	85.31	****
11.00	4.90	90.21	****
11.50	4.90	95.10	****
12.00		100.00	

MEAN ST.DEV. SKEWNESS KUPTOSIS

7.63 2.01 0.06 -1.01 KUMBEIN+PETTITJOHN(1938) MOMENT MEASURES FOR SIZE RANGE 3.5 TO 11.5 PHI

7.85 2.23 0.14 1.17 FOLK GRAPHIC STATISTICAL PARAMETERS FOLK AND WARD, 1957

PERCENTILES MEDIAN 7.62 5TH 4.66 16TH 5.57 25TH 6.06

75TH 9.48 84TH 10.37 95TH 11.49

PER CENT GRAVEL 0.0 SAND 2.08 SILT 54.17 ( 53.85) CLAY 43.75 ( 44.06)

GRAVEL + SAND 2.08 SILT/(SILT+CLAY) 55.00PCT GRAV+SAND/SILT+CLAY 0.02

PITT40A

SIEVE, SH. PIP., SEDIGRAPH SAMPLE WT.= 3.4200

PHI PCT. CUMFCT.

3.50			
4.00	1.17	1.17	*
4.50	1.98	3.15	**
5.00	2.96	6.11	***
5.50	5.93	12.04	*****
6.00	6.92	18.96	*****
6.50	4.94	23.90	*****
7.00	4.44	28.34	*****
7.50	6.92	35.26	*****
8.00	6.92	42.18	*****
8.50	7.91	50.09	*****
9.00	9.88	60.07	*****
9.50	5.93	66.00	*****
10.00	5.93	72.93	*****
10.50	5.93	78.86	*****
11.00	6.92	85.78	*****
11.50	5.93	91.71	*****
12.00	1.98	93.69	**
12.00	6.92	100.00	*****

MEAN ST.DEV. SKEWNESS KURTOSIS

8.11 2.05 -0.06 -0.96

KRUMBEIN+PETTIIJOHN(1938) MOMENT MEASURES  
FOR SIZE RANGE 4.0 TO 12.0 PHI

8.39 2.37 -0.03 1.19

FOLK GRAPHIC STATISTICAL PARAMETERS  
FOLK AND WARD, 1957

PERCENTILES MEDIAN 8.46 5TH 4.81 16TH 5.79 25TH 6.61

75TH 10.23 84TH 10.92 95TH 12.00

PER CENT GRAVEL 0.0 SAND 1.17 SILT 41.73 ( 41.51) CLAY 57.10 ( 57.32)

PITT408

SEDIGRAPH ANALYSIS

PHI	PCT. CUMPCT.		
4.00	0.0		
4.50	2.00	**	
5.00	6.00	*****	
5.50	10.00	*****	
6.00	18.00	*****	
6.50	27.00	*****	
7.00	36.00	*****	
7.50	47.00	*****	
8.00	55.00	*****	
8.50	61.00	*****	
9.00	74.00	*****	
9.50	83.00	***	
10.00	87.00	**	
10.50	90.00	**	
11.00	92.00	*	
11.50	94.00		
12.00	95.00		
12.00	100.00		

MEAN ST.DEV. SKEWNESS KURTOSIS

7.68 1.64 0.14 -0.67 KRUMBEIN+PETTICHOFF (1938) MOMENT MEASURES FOR SIZE RANGE 4.5 TO 12.0 PHI

7.74 1.95 0.16 1.32 FOLK GRAPHIC STATISTICAL PARAMETERS FOLK AND WARD, 1957

PERCENTILES MEDIAN 7.69 5TH 5.25 16TH 5.90 25TH 6.39 75TH 9.06 84TH 9.63 95TH 12.00

PER CENT GRAVEL 0.00 SAND 0.0 SILT 0.0 ( 61.00) CLAY 0.0 ( 39.00)

GRAVEL + SAND 0.00 SILT/(SILT+CLAY) 61.00PCT GRAV+SAND/SILT+CLAY 0.00

LABELS SHEPARD -CLAYEY SILT FOLK(GMS)-MUD

(SCS)-MUD

P1++ 41 0 0.0 0 0.0 0

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 \*\*\* MULTIMODAL SAMPLE \*\*\*  
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WET WT	DRY WT	SALT	ORGANIC	MOISTURE	WEIGHT LOSS DUE TO HANDLING	0.0
1000.0000	5.1800	0.0	0.0	0.0 (GRAMS)	GRAVEL CORRECTION FACTOR	1.000
100.0000	100.0000	0.0	0.0	0.0 (PCT WET WT)	SIZES ELIMINATED (<0.01)	NONE
					TRASK SORTING COEFFICIENT	2.101
					USING PROBABILITY EXTRAP.	2.088
					MEAN CUBED DEVIATION	15.544
					USING PROBABILITY EXTRAP.	13.367

PERCENTAGE COMPOSITION TABLE OF STATISTICAL DATA IN PHI UNITS PERCENTILES LINEAR EXTRAP. PROBABILITY EXTRAP.

	MEAN	STD DEV	SKEWNESS	KURTOSIS	MM.			PHI UNITS		
					MM.	PHI UNITS	MM.	PHI UNITS		
GRAVEL 0.0	5.36141	2.11961	1.63230	5.96058	5.0	0.11645	3.10219	0.11171	3.10221	
SAND 28.19	5.35819	2.05163	1.54784	5.45989	10.0	0.09841	3.34505	0.09496	3.39656	
SILT 61.65	5.18990	1.88250	0.27868	1.32931	16.0	0.08274	3.59532	0.08105	3.61441	
CLAY 10.17	5.19261	1.86668	0.28770	1.32852	25.0	0.06725	3.89420	0.06651	3.91018	
MUD 71.81	5.25513	1.65981	0.11987	1.09276	50.0	0.03006	5.05610	0.03008	5.05516	
S/M 0.39	5.26164	1.64723	0.12535	1.08965	75.0	0.01524	6.03606	0.01526	6.03392	
		1.58657	-0.09103	0.22610	84.0	0.00829	6.91493	0.00832	6.90886	
		1.57314	-0.08311	0.22882	90.0	0.00380	8.04015	0.00381	8.03720	
				0.57069	95.0	0.00094	10.04936	0.00095	10.04647	
				0.57064						

DATA FOR CONSTN OF BARGRAPHS AND CUM. CURVES

SIZE FRACTION	WT.(GMS)		WT.PCT.		MID PHI(LINEAR)		MID PHI(PROB.)		MODE	
	MM	PHI	UNCOR	COR	PHI	MM	PHI	MM		
0.250000	2.000	0.310	0.010	0.193	0.193	1.751	0.29707	1.882	0.27128	0
0.177000	2.458	0.020	0.020	0.386	0.579	2.249	0.21036	2.308	0.20197	0
0.125000	3.000	0.120	0.120	2.317	2.896	2.749	0.14875	2.828	0.14380	0
0.088000	3.506	0.540	0.540	10.425	13.520	3.253	0.10488	3.322	0.10503	0
0.062500	4.000	0.770	0.770	14.865	28.185	3.753	0.07416	3.780	0.07278	0
0.044000	4.506	0.878	0.878	16.948	45.133	4.253	0.05244	4.263	0.05208	1*
0.031000	5.012	0.174	0.174	3.363	48.496	4.759	0.03693	4.759	0.03692	0
0.022000	5.506	0.864	0.864	10.684	65.181	5.259	0.02612	5.254	0.02620	1
0.015600	6.002	0.488	0.488	9.431	74.611	5.754	0.01853	5.745	0.01864	0
0.011000	6.506	0.301	0.301	5.803	80.414	6.254	0.01310	6.245	0.01318	0
0.007800	7.002	0.225	0.225	4.352	84.767	6.754	0.00926	6.744	0.00933	0
0.005900	7.506	0.113	0.113	2.177	86.943	7.254	0.00655	7.248	0.00658	0
0.003900	8.002	0.150	0.150	2.902	89.845	7.754	0.00463	7.743	0.00467	1
0.002700	8.533	0.113	0.113	2.176	92.020	8.268	0.00325	8.256	0.00327	0
0.001900	9.040	0.075	0.075	1.451	93.471	8.786	0.00227	8.777	0.00228	0
0.001380	9.501	0.038	0.038	0.726	94.197	9.270	0.00162	9.265	0.00163	0
0.000960	9.995	0.038	0.038	0.725	94.922	9.748	0.00116	9.741	0.00117	0
0.000690	10.501	0.038	0.038	0.726	95.648	10.248	0.00082	10.240	0.00083	1
0.000450	10.995	0.038	0.038	0.725	96.373	10.748	0.00058	10.739	0.00059	0
0.000340	11.522	0.038	0.038	0.726	97.099	11.259	0.00041	11.246	0.00041	1
0.000240	12.025	0.038	0.038	0.725	97.823	11.773	0.00029	11.758	0.00029	0

PITT45

SIEVE, SH. PIP., SEDIGRAPH SAMPLE WT.= 5.0400

PHI PCT. CUMPT.

3.00			
3.50	1.59		**
	3.57	1.59	****
4.00		5.16	
	6.77		*****
4.50		11.94	
	10.64		*****
5.00		22.58	
	17.42		*****
5.50		40.00	
	16.45		*****
6.00		56.45	
	10.64		*****
6.50		67.10	
	7.74		*****
7.00		74.84	
	5.81		*****
7.50		80.65	
	4.84		*****
8.00		85.48	
	3.87		*****
8.50		89.36	
	1.94		**
9.00		91.29	
	0.97		*
9.50		92.26	
	0.97		*
10.00		93.23	
	0.97		*
10.50		94.19	
	0.97		*
11.00		95.16	
	4.84		*****
12.00		100.00	

MEAN ST. DEV. SKEWNESS KUPTOSIS

5.99	1.47	0.43	0.79
0.11	1.24	0.38	1.58

KRUMBEIN+PETTICORN(1938) MOMENT MEASURES FOR SIZE RANGE 3.5 TO 11.0 PHI

FOLK GRAPHIC STATISTICAL PARAMETERS FOLK AND WARD, 1957

PERCENTILES	MEDIAN	5TH	16TH	25TH
	3.00	3.98	4.69	5.07
		75TH	84TH	95TH
		7.01	7.85	10.92

PER CENT GRAVEL 0.0 SAND 5.16 SILT 80.44 ( 80.32) CLAY 14.40 ( 14.52)

GRAVEL + SAND 5.16 SILT/(SILT+CLAY) 84.65PCT GRAV+SAND/SILT+CLAY 0.05

LABELS SHEPARD -SILT FOLK(KGMS)-MUD (SCS)-SILT

P1++ 42 0 0.0 0 0.0 0

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 \*\*\* MULTIMODAL SAMPLE \*\*\*  
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WET WT	DRY WT	SALT	ORGANIC	MOISTURE	WEIGHT LOSS DUE TO HANDLING	0.0
1000.0000	6.3100	0.0	0.0	0.0 (GRAMS)	GRAVEL CORRECTION FACTOR	1.000
100.0000	100.0000	0.0	0.0	0.0 (PCT WET WT)	SIZES ELIMINATED (K0.01%)	NONE
					TRASK SORTING COEFFICIENT	1.930
					USING PROBABILITY EXTRAP.	1.908
					MEAN CUBED DEVIATION	8.229
					USING PROBABILITY EXTRAP.	3.847

PERCENTAGE COMPOSITION		TABLE OF STATISTICAL DATA IN PHI UNITS				PERCENTILES		LINEAR EXTRAP.		PROBABILITY EXTRAP.	
		MEAN	STD DEV	SKEWNESS	KURTOSIS		MM.	PHI UNITS	MM.	PHI UNITS	
GRAVEL	0.0	5.00619	1.68268	1.72719	7.30730	5.0	0.11629	3.10416	0.11181	3.10087	
SAND	29.64	4.96703	1.48859	1.16629	4.67062	10.0	0.09699	3.36005	0.09406	3.41033	
SILT	66.05	4.84360	1.38834	0.28719	1.02392	16.0	0.08230	3.60304	0.08099	3.62614	
CLAY	4.32	4.84389	1.36578	0.29655	1.02547	25.0	0.08863	3.86504	0.08762	3.88644	
MUD	70.36	4.94371	1.34068	0.22401	0.76732	50.0	0.04001	4.64339	0.04002	4.64298	
S/M	0.42	4.94436	1.31822	0.22865	0.76906	75.0	0.01843	5.76181	0.01858	5.75044	
		KRUMH. INMAN	1.40501	0.17003	0.27529	84.0	0.01283	6.28439	0.01302	6.26258	
		P-INMAN	1.38074	0.17548	0.27529	90.0	0.00891	6.81106	0.00900	6.79588	
		P-KRUMH.			0.50591	95.0	0.00436	7.84298	0.00441	7.82489	
		FDLK (TRANSFORMED)			6.50629						
		P-FDLK (TRANSFORMED)									

DATA FOR CONSTN OF BARGRAPHS AND CUM. CURVES

SIZE FRACTION	WT.(GMS)		WT.PCT.		MID PHI(LINEAR)		MID PHI(PROB.)		MODE	
MM	PHI	UNCOR	COR	COR	PHI	MM	PHI			
0.250000	2.000	0.030	0.030	0.475	0.475	1.751	0.29707	1.901	0.26171	0
0.177000	2.498	0.030	0.030	0.475	0.951	2.249	0.21036	2.286	0.20757	0
0.125000	3.000	0.130	0.130	2.060	3.011	2.749	0.14875	2.608	0.14282	0
0.088600	3.506	0.610	0.610	9.867	12.076	3.253	0.10488	3.318	0.10025	0
0.062500	4.000	1.070	1.070	16.957	29.635	3.753	0.07416	3.784	0.07262	0
0.044900	4.506	1.122	1.122	17.788	47.424	4.253	0.05244	4.262	0.05212	1*
0.031000	5.012	0.599	0.599	9.496	56.920	4.759	0.03693	4.758	0.03695	0
0.022000	5.506	0.861	0.861	13.642	70.502	5.259	0.02612	5.251	0.02626	1
0.015600	6.002	0.544	0.544	8.616	79.178	5.754	0.01853	5.743	0.01867	0
0.011000	6.506	0.544	0.544	8.616	87.794	6.254	0.01310	6.233	0.01330	1
0.007800	7.002	0.227	0.227	3.590	91.384	6.754	0.00926	6.739	0.00936	0
0.005500	7.506	0.136	0.136	2.154	93.538	7.254	0.00655	7.241	0.00661	0
0.003900	8.002	0.136	0.136	2.154	95.692	7.754	0.00463	7.735	0.00470	0
0.002700	8.533	0.045	0.045	0.718	96.410	8.268	0.00325	8.258	0.00327	0
0.001900	9.040	0.045	0.045	0.719	97.128	8.786	0.00227	8.775	0.00228	0
0.000001	14.000	0.181	0.181	2.872	100.000	11.520	0.00034	9.820	0.00111	0
TOTALS		6.310	6.310	100.0						
0.250000	C.040000									
0.177000	C.080000									
0.125000	C.760000									
0.088600	1.020000									

PI+ 43 0 0.0 0 0.0 0

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 MULTIMODAL SAMPLE  
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WET WT	DPY WT	SALT	ORGANIC	MOISTURE	WEIGHT LOSS DUE TO HANDLING	0.0
100.0000	5.7800	0.0	0.0	0.0 (GRAMS)	GRAVEL CORRECTION FACTOR	1.000
100.0000	100.0000	0.0	0.0	0.0 (PCT WET WT)	SIZES ELIMINATED (<0.01%)	NONE
					TRASK SORTING COEFFICIENT	2.326
					USING PROBABILITY EXTRAP.	2.298
					MEAN CURED DEVIATION	13.147
					USING PROBABILITY EXTRAP.	9.634

PERCENTAGE COMPOSITION	TABLE OF STATISTICAL DATA IN PHI UNITS					PERCENTILES		LINEAR EXTRAP.		PROBABILITY EXTRAP.	
	MEAN	STD DEV	SKWNESS	KURTOSIS		MM.	PHI UNITS	MM.	PHI UNITS		
GRAVEL 0.0	4.77598	2.05552	1.51377	5.56451	5.0	0.16383	2.60976	0.15460	2.69336		
SAND 45.50	4.76377	1.94277	1.31380	4.48585	10.0	0.14353	2.80058	0.13644	2.87361		
SILT 47.18	4.55761	1.84208	0.42579	1.08576	15.0	0.12309	3.02223	0.12259	3.02809		
CLAY 7.31	4.55853	1.82703	0.43688	1.08696	25.0	0.10291	3.28046	0.10112	3.30581		
MUD 54.50	4.75091	1.72868	0.33546	0.86647	50.0	0.05551	4.17130	0.05554	4.17031		
S/M 0.83	4.75264	1.72455	0.33767	0.84611	75.0	0.01902	5.71627	0.01915	5.70662		
	KRUMHÖLN	1.80430	0.32736	0.26532	84.0	0.01121	6.47959	0.01122	6.47719		
	P-KRUM.	1.77838	0.33590	0.26408	90.0	0.00582	7.42578	0.00584	7.41914		
	FGLK (TRANSFORMED)			0.52056	95.0	0.00187	9.06283	0.00187	9.06076		
	P-FGLK (TRANSFORMED)			0.52083							

DATA FOR CONSTN OF BARGRAPHS AND CUM. CURVES

SIZE FRACTION	PHI	WT.(GMS)	WT.PCT.	WT.PCT.	MID PHI(LINEAR)	MID PHI(PROB.)	MODE
MM	PHI	UNCOR	COR	CUMUL.	PHI	MM	
0.250000	2.000	0.040	0.040	0.692	0.692	1.751	0.29707
0.177000	2.498	0.380	0.080	1.364	2.076	2.249	0.21036
0.125000	3.000	0.760	0.760	13.149	15.225	2.749	0.14875
0.082500	3.508	1.025	1.025	17.647	32.872	3.253	0.10488
0.062500	4.000	0.730	0.730	12.630	45.502	3.753	0.07416
0.040000	4.506	0.770	0.770	13.318	58.820	4.253	0.05244
0.031000	5.012	0.139	0.139	2.413	61.234	4.759	0.03693
0.022500	5.506	0.617	0.617	10.675	71.903	5.259	0.02612
0.015600	6.002	0.422	0.422	7.304	79.212	5.754	0.01853
0.011300	6.506	0.292	0.292	5.056	84.268	6.254	0.01310
0.007800	7.002	0.195	0.195	3.371	87.639	6.754	0.00926
0.005600	7.506	0.162	0.162	2.810	89.449	7.254	0.00655
0.002900	8.002	0.130	0.130	2.247	92.696	7.754	0.00463
0.002700	8.523	0.065	0.065	1.124	93.820	8.268	0.00325
0.001900	9.040	0.065	0.065	1.124	94.944	8.786	0.00227
0.001380	9.561	0.065	0.065	1.124	96.067	9.270	0.00162
0.000980	9.995	0.065	0.065	1.124	97.191	9.748	0.00116
0.000640	10.501	0.032	0.032	0.561	97.753	10.248	0.00082
0.000061	14.000	0.130	0.130	2.247	100.000	12.251	0.00021
TOTALS		5.780	5.780	100.0			
0.250000	0.160000						

PITT44

SIEVE, SH. PIP., SEDIGRAPH SAMPLE WT.= 4.4900

PHI PCT. CUMPT.

3.50			
4.00	4.68	4.68	*****
	6.88		*****
4.50	11.56		*****
	11.79		*****
5.00	23.35		*****
	17.69		*****
5.50	41.04		*****
	17.69		*****
6.00	58.73		*****
	14.74		*****
6.50	73.47		*****
	8.84		*****
7.00	82.31		*****
	6.88		*****
7.50	89.19		*****
	4.91		*****
8.00	94.10		**
	1.97		**
8.50	96.07		**
	1.97		**
9.00	98.03		**
	1.97		**
12.00	100.00		

MEAN ST.DEV. SKEWNESS KUPTOSIS

5.82 1.14 0.19 -0.21 KRUMBEIN+PETTIJOHN(1938) MOMENT MEASURES  
FOR SIZE RANGE 4.0 TO 9.0 PHI

5.85 1.25 0.15 1.06 FOLK GRAPHIC STATISTICAL PARAMETERS  
FOLK AND WARD,1957

PERCENTILES MEDIAN 5.75 5TH 4.02 16TH 4.69 25TH 5.05  
75TH 6.59 84TH 7.12 95TH 8.23

PER CENT GRAVEL 0.0 SAND 4.68 SILT 89.74 ( 89.42) CLAY 5.57 ( 5.90)

GRAVEL + SAND 4.68 SILT/(SILT+CLAY) 93.81PCT GRAV+SAND/SILT+CLAY 0.05

LABELS SHEPARD -SILT FOLK(GMS)-MUD (SCS)-SILT



PIT146

SIEVE, SH. PIP., SEDIGRAPH SAMPLE WT. = 5.4600

PHI PCT. COMPCT.

1.50	0.37		
2.00	0.55	0.37	*
2.50	0.92		
	1.28		*
3.00	2.20		
	2.38		**
3.50	4.58		
	4.76		*****
4.00	9.34		
	5.44		*****
4.50	14.70		
	12.69		*****
5.00	27.47		
	19.04		*****
5.50	40.51		
	10.88		*****
6.00	57.37		
	7.25		*****
6.50	64.64		
	4.53		*****
7.00	69.18		
	2.72		*****
7.50	71.90		
	2.72		***
8.00	74.62		
	1.81		**
8.50	76.43		
	1.81		**
9.00	78.24		
	1.81		**
9.50	80.05		
	0.91		*
10.00	80.96		
	0.91		*
10.50	81.87		
	0.91		*
11.00	82.77		
	17.23		*****
12.00	100.00		

MEAN ST.DEV. SKEWNESS KURTOSIS

5.87	1.62	0.44	1.10	KRUMBEIN+PETTICORN(1938) MOMENT MEASURES FOR SIZE RANGE 2.0 TO 11.0 PHI
7.29	2.87	0.57	1.45	FOLK GRAPHIC STATISTICAL PARAMETERS FOLK AND WARD, 1957

PERCENTILES	MEDIAN	5.00	5TH	3.54	16TH	4.55	25TH	4.90
			75TH	8.11	84TH	11.07	95TH	11.71

PI++ 48 0 0.0 0 0.0 0

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 \*\*\* MULTIMODAL SAMPLE \*\*\*  
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WET WT	DRY WT	SALT	ORGANIC	MOISTURE	WEIGHT LOSS DUE TO HANDLING	0.0
1000.0000	6.5400	0.0	0.0	0.0 (GRAMS)	GRAVEL CORRECTION FACTOR	1.000
100.0000	100.0000	0.0	0.0	0.0 (PCT WET WT)	SIZES ELIMINATED (<0.01%)	NONE
					TRASK SORTING COEFFICIENT	2.315
					USING PROBABILITY EXTRAP.	2.296
					MEAN CUBED DEVIATION	16.174
					USING PROBABILITY EXTRAP.	11.921

PERCENTAGE COMPOSITION	TABLE OF STATISTICAL DATA IN PHI UNITS				PERCENTILES		LINEAR EXTRAP.		PROBABILITY EXTRAP.	
		MEAN	STD DEV	SKWNESS	KURTOSIS	MM.	PHI UNITS	MM.	PHI UNITS	
GRAVEL 0.0	MOMENT 5.36295	2.33600	1.26879	4.59943	5.0	0.16914	2.56368	0.16659	2.58562	
SAND 29.97	P-MOMENT 5.35456	2.21157	1.10204	3.91924	10.0	0.12410	3.01041	0.12363	3.01356	
SILT 57.67	FOLK 5.16853	2.15329	0.20843	1.34345	16.0	0.10135	3.30260	0.09941	3.33043	
CLAY 12.16	P-FOLK 5.17613	2.14207	0.21428	1.35303	25.0	0.07436	3.74930	0.07370	3.76223	
MUD 70.03	INMAN 5.20367	1.90107	0.05545	1.08783	50.0	0.02919	5.09626	0.02922	5.09691	
S/M 0.43	P-INMAN 5.21574	1.98531	0.06303	1.09943	75.0	0.01388	6.17094	0.01398	6.16006	
	KRUMHOLZ 1.79381	-0.13814	0.20958		84.0	0.00727	7.10474	0.00728	7.10106	
	P-KRUM 1.77617	-0.13577	0.20787		90.0	0.00226	8.78776	0.00227	8.78114	
	FOLK (TRANSFORMED) 0.57328				95.0	0.00069	10.50187	0.00069	10.50178	
	P-FOLK (TRANSFORMED) 0.57502									

DATA FOR CONSTN OF BARGRAPHS AND CUM. CURVES

SIZE FRACTION	WT.(GMS)		WT.PCT.		MID PHI(LINEAR)		MID PHI(Prob.)		MODE	
	MM	PHI	UNCOR	COR	CUMUL.	PHI	MM	PHI		
0.250000	2.000	0.160	0.160	2.446	2.446	1.751	0.29707	1.921	0.26414	1
0.177000	2.456	0.120	0.120	1.835	4.281	2.249	0.21036	2.277	0.20526	0
0.125000	3.000	0.360	0.360	5.305	9.786	2.745	0.14975	2.788	0.14477	0
0.088000	3.506	0.680	0.680	10.358	20.184	3.253	0.10488	3.283	0.10271	1
0.062500	4.000	0.640	0.640	9.786	29.969	3.753	0.07416	3.766	0.07350	0
0.044000	4.506	0.844	0.844	12.901	42.870	4.253	0.05244	4.261	0.05216	1
0.031000	5.012	0.278	0.278	4.250	47.120	4.759	0.03693	4.760	0.03591	0
0.022000	5.506	1.075	1.075	16.436	63.550	5.259	0.02612	5.255	0.02618	1
0.015000	6.002	0.561	0.561	8.575	72.131	5.754	0.01853	5.747	0.01862	0
0.011000	6.506	0.561	0.561	8.575	80.706	6.254	0.01310	6.242	0.01322	1
0.007800	7.002	0.187	0.187	2.859	83.564	6.754	0.00926	6.748	0.00930	0
0.005500	7.506	0.140	0.140	2.144	85.705	7.254	0.00655	7.248	0.00658	0
0.003900	8.002	0.140	0.140	2.144	87.852	7.754	0.00463	7.747	0.00465	1
0.002700	8.533	0.093	0.093	1.430	89.281	8.268	0.00325	8.262	0.00326	0
0.001900	9.040	0.093	0.093	1.429	90.710	8.786	0.00227	8.780	0.00228	0
0.001300	9.501	0.093	0.093	1.429	92.139	9.270	0.00162	9.263	0.00163	0
0.000980	9.995	0.093	0.093	1.430	93.569	9.748	0.00116	9.738	0.00117	1
0.000690	10.501	0.093	0.093	1.429	94.998	10.248	0.00082	10.235	0.00083	0
0.000450	10.995	0.093	0.093	1.430	96.427	10.748	0.00058	10.731	0.00059	0
0.000061	14.000	0.234	0.234	3.573	100.000	12.497	0.00017	11.460	0.00036	0
TOTALS		6.540	6.540	100.0						

PI++ 49 0 0.0 0 0.0 0

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 \*\*\* MULTIMODAL SAMPLE \*\*\*  
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WET WT	OPY WT	SALT	ORGANIC	MOISTURE	WEIGHT LOSS DUE TO HANDLING	0.0
1000.0000	6.3300	0.0	0.0	0.0	GRAVEL CORRECTION FACTOR	1.000
100.0000	100.0000	0.0	0.0	0.0	SIZES ELIMINATED (<0.012)	NONE
					TRASK SORTING COEFFICIENT	2.275
					USING PROBABILITY EXTRAP.	2.255
					MEAN CUBED DEVIATION	10.557
					USING PROBABILITY EXTRAP.	6.177

PERCENTAGE COMPOSITION		TABLE OF STATISTICAL DATA IN PHI UNITS				PERCENTILES	LINEAR EXTRAP.	PROBABILITY EXTRAP.		
		MEAN	STD DEV	SKENNESS	KURTOSIS		MM.	PHI UNITS	MM.	PHI UNITS
GRAVEL	0.0	4.58694	1.92786	1.47344	5.45582	5.0	0.16812	2.57243	0.16074	2.65720
SAND	50.24	4.55945	1.76433	1.12472	3.72803	10.0	0.19043	2.73266	0.14211	2.81467
SILT	43.72	4.39308	1.71206	0.43579	1.09115	16.0	0.13164	2.92537	0.12893	2.95527
CLAY	6.04	4.39878	1.68948	0.44862	0.99818	25.0	0.11036	3.17976	0.10871	3.20142
MUD	49.76	4.59410	1.66872	0.36137	0.75570	50.0	0.06289	3.99106	0.06288	3.99122
S/M	1.01	4.60257	1.64729	0.31112	0.73452	75.0	0.02133	5.59114	0.02138	5.54772
			1.75657	0.57439	0.26894	84.0	0.01302	6.26282	0.01314	6.24986
			1.73799	0.38335	0.27161	90.0	0.00708	7.14166	0.00712	7.15405
					0.50029	95.0	0.00303	8.36522	0.00306	8.35173
					0.45954					

DATA FOR CONSTN OF BARGRAPHS AND CUM. CURVES

SIZE FRACTION	WT.(GMS)		WT.PCT.		MID PHI(LINEAR)		MID PHI(PROB.)		MODE	
	MM	PHI	UNCOR	COR	PHI	MM	PHI	MM		
0.250000	2.000	0.050	0.050	0.790	0.790	1.751	0.29707	1.909	0.26027	0
0.177000	2.498	0.120	0.120	1.896	2.686	2.249	0.21036	2.311	0.20153	0
0.125000	3.000	0.990	0.990	15.640	18.325	2.749	0.14875	2.829	0.14076	0
0.087000	3.506	1.190	1.190	18.799	37.125	3.255	0.10488	3.275	0.10531	1
0.062500	4.000	0.830	0.830	13.112	50.237	3.753	0.07416	3.756	0.07599	0
0.044000	4.506	0.673	0.673	10.625	60.865	4.253	0.05244	4.251	0.05253	0
0.031000	5.012	0.250	0.250	3.949	64.814	4.759	0.03693	4.757	0.03699	0
0.222000	5.506	0.604	0.604	9.550	74.364	5.259	0.02612	5.250	0.02627	1
0.015600	6.002	0.446	0.446	7.038	81.402	5.754	0.01853	5.743	0.01867	0
0.011000	6.506	0.318	0.318	5.026	86.428	6.254	0.01310	6.241	0.01522	0
0.007800	7.002	0.191	0.191	3.916	89.444	6.754	0.00926	6.743	0.00933	0
0.005000	7.506	0.127	0.127	2.011	91.455	7.254	0.00695	7.245	0.00659	0
0.003900	8.002	0.159	0.159	2.913	93.968	7.754	0.00463	7.738	0.00468	1
0.002700	8.533	0.095	0.095	1.508	95.476	8.268	0.00325	8.252	0.00328	0
0.001900	9.040	0.127	0.127	2.010	97.487	8.786	0.00227	8.756	0.00231	0
0.000001	14.000	0.159	0.159	2.913	100.000	11.520	0.00334	9.829	0.00113	0
TOTALS				6.330	6.330	100.0				
0.250000	0.010300									
0.177000	0.010300									
0.125000	0.240000									
0.088000	0.810000									

PI++ 50 0 0.0 0 0.0 0

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 \*\*\*\* MULTIMODAL SAMPLE \*\*\*\*  
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WET WT DRY WT SALT ORGANIC MOISTURE  
 100.0000 6.3500 0.0 0.0 0.0 (GRAMS)  
 100.0000 100.0000 0.0 0.0 0.0 (PCT WET WT)

WEIGHT LOSS DUE TO HANDLING 0.0  
 GRAVEL CORRECTION FACTOR 1.000  
 SIZES ELIMINATED (<0.016) NONE  
 TRASK SORTING COEFFICIENT 2.310  
 USING PROBABILITY EXTRAP. 2.293  
 MEAN CUBED DEVIATION 9.540  
 USING PROBABILITY EXTRAP. 4.822

PERCENTAGE COMPOSITION		TABLE OF STATISTICAL DATA IN PHI UNITS				PERCENTILES		LINEAR EXTRAP.		PROBABILITY EXTRAP.	
		MEAN	STD DEV	SKEWNESS	KURTOSIS		MM.	PHI UNITS	MM.	PHI UNITS	
GRAVEL	0.0	5.39800	1.97154	1.24488	4.90284	5.0	0.12192	3.03593	0.11977	3.06166	
SAND	27.72	5.35234	1.78161	0.85259	3.37179	10.0	0.10625	3.23441	0.10170	3.29758	
SILT	52.78	5.23941	1.81696	0.17620	1.02439	16.0	0.09008	3.47253	0.08937	3.48402	
CLAY	9.50	5.24059	1.80771	0.18198	1.02847	25.0	0.06808	3.87657	0.06752	3.88861	
MUD	72.28	5.27653	1.80395	0.06173	0.67380	50.0	0.02787	5.16516	0.02769	5.16415	
S/M	0.38	5.27850	1.75448	0.06372	0.67433	75.0	0.01276	6.29260	0.01284	6.28320	
			1.78965	-0.08058	0.25963	84.0	0.00739	7.08647	0.00743	7.07299	
			1.77377	-0.07825	0.26126	90.0	0.00422	7.88725	0.00424	7.86037	
					0.50602	95.0	0.00185	9.07461	0.00186	9.07078	
					0.50702						

DATA FOR CONSTN OF BARGRAPHS AND CUM. CURVES

SIZE FFACTION	WT.(GMS)	WT.PCT.	WT.PCT.	MID PHILINEAR)	MID PHI(PROB.)	MODE
MM	PHI	UNCOR	COR	COR CUMUL.	PHI	MM
0.250000	2.000	0.010	0.010	0.157	0.157	1.751
0.177000	2.498	0.010	0.010	0.157	0.315	2.249
0.125000	3.000	0.240	0.240	3.780	4.094	2.749
0.088000	3.506	0.810	0.810	12.756	16.850	3.253
0.062500	4.000	0.690	0.690	10.866	27.717	3.753
0.044000	4.506	0.502	0.502	7.902	35.619	4.253
0.331000	5.012	0.611	0.611	9.021	45.240	4.759
0.322000	5.506	0.974	0.974	15.332	60.572	5.259
0.015600	6.002	0.649	0.649	10.222	70.795	5.754
0.011000	6.506	0.464	0.464	7.302	78.066	6.254
0.007800	7.002	0.325	0.325	5.111	83.207	6.754
0.005500	7.506	0.325	0.325	5.111	88.318	7.254
0.003900	8.002	0.139	0.139	2.150	90.508	7.754
0.002700	8.532	0.185	0.185	2.921	93.429	8.268
0.001900	9.040	0.093	0.093	1.460	96.609	8.766
0.001300	9.501	0.093	0.093	1.461	98.350	9.270
0.000600	14.000	0.232	0.232	3.050	100.000	11.751
TOTALS		6.350	6.350	100.0		
0.250000	0.100000					
0.177000	0.150000					
0.125000	0.860000					

PITTS1

SIEVE, SH. PIP., SEDIGRAPH SAMPLE WT.= 4.9900

PHI PCT. CUMFCT.

2.00			
2.50	0.20	0.20	*
3.00	0.80	1.00	*
	4.01		****
3.50		5.02	
	6.22		*****
4.00		11.23	
	9.76		*****
4.50		21.00	
	15.98		*****
5.00		36.93	
	18.64		*****
5.50		55.62	
	12.43		*****
6.00		68.04	
	7.99		*****
6.50		76.03	
	5.33		****
7.00		81.36	
	6.21		*****
7.50		87.57	
	4.44		****
8.00		92.01	
	2.66		***
8.50		94.67	
	1.78		**
9.00		96.45	
	0.89		*
9.50		97.34	
	2.65		***
12.00		100.00	

MEAN ST.DEV. SKEWNESS KURTOSIS

5.51 1.36 0.26 -0.08 KRUMBEIN+PETTICORN(1938) MOMENT MEASURES  
FOR SIZE RANGE 2.5 TO 9.5 PHI

5.60 1.51 0.26 1.20 FOLK GRAPHIC STATISTICAL PARAMETERS  
FOLK AND WARD,1957

PERCENTILES MEDIAN 5.35 5TH 3.50 16TH 4.24 25TH 4.63  
75TH 6.44 84TH 7.21 95TH 8.59

PER CENT GRAVEL 0.0 SAND 11.23 SILT 80.74 ( 80.78) CLAY 8.02 ( 7.99)

GRAVEL + SAND 11.23 SILT/(SILT+CLAY) 91.00PCT GRAV+SAND/SILT+CLAY 0.13

LABELS SHEPARD -SILT FOLK(GMS)-SANDY MUD (SCS)-SANDY SILT

PARAMETER - NAME UNIT VALUE UNIT

PITT92

SIEVE, SH. PIP., SEDIGRAPH SAMPLE WT.= 5.1400

PHI PCT. CUMPCT.

3.50			*****
4.00	7.01	7.01	*****
4.50	9.30	16.31	*****
	26.04		*****
5.00		42.35	*****
	15.81		*****
5.50		58.15	*****
	6.51		*****
6.00		64.66	*****
	7.44		*****
6.50		72.10	*****
	4.65		*****
7.00		76.75	*****
	4.65		*****
7.50		81.40	***
	2.79		***
8.00		84.19	***
	2.79		***
8.50		86.98	**
	1.86		**
9.00		88.84	****
	3.72		****
9.50		92.56	**
	1.86		**
10.00		94.42	**
	1.86		**
10.50		96.28	****
	3.72		****
12.00		100.00	

MEAN ST.DEV. SKEWNESS KUPTOSIS

5.75 1.62 0.56 0.44 KRUMBEIN+PETTIJOHN(1938) MOMENT MEASURES FOR SIZE RANGE 4.0 TO 10.5 PHI

5.90 1.82 0.56 1.37 FOLK GRAPHIC STATISTICAL PARAMETERS FCLK AND WARD,1957

PERCENTILES MEDIAN 5.24 5TH 3.86 16TH 4.48 25TH 4.67 75TH 6.81 84TH 7.97 95TH 10.16

PER CENT GRAVEL 0.0 SAND 7.01 SILT 76.92 ( 77.18) CLAY 16.07 ( 15.81)

GRAVEL + SAND 7.01 SILT/(SILT+CLAY) 83.00PCT GRAV+SAND/SILT+CLAY 0.08

LABELS SHEPARD -SILT FOLK(IGMS)-MUD (SCSI)-SILT

PITT53

SIEVE, SH. PIP., SEDIGRAPH SAMPLE WT.= 5.0300

PHI PCT. COMPCT.

2.50			*
3.00	0.80	0.80	***
3.50	2.98	3.78	*****
4.00	5.77	9.54	*****
4.50	7.38	16.93	*****
5.00	22.15	39.08	*****
5.50	14.77	53.65	*****
6.00	7.38	61.23	*****
6.50	7.38	68.62	*****
7.00	5.54	74.16	*****
7.50	5.54	79.69	****
8.00	3.69	83.39	****
8.50	4.62	88.00	***
9.00	2.77	90.77	***
9.50	5.69	94.46	**
10.00	1.85	96.31	**
12.00	3.69	100.00	****

MEAN ST.DEV. SKEWNESS KURTOSIS

5.78 1.63 0.35 -0.25 KRUMBEIN+PETTIT(1938) MOMENT MEASURES FOR SIZE RANGE 3.0 TO 10.0 PHI

5.96 1.82 0.45 1.25 FOLK GRAPHIC STATISTICAL PARAMETERS FOLK AND WARD,1957

PERCENTILES MEDIAN 5.37 5TH 3.61 16TH 4.44 25TH 4.68  
75TH 7.08 84TH 8.07 95TH 9.65

PER CENT GRAVEL 0.0 SAND 9.54 SILT 74.55 ( 73.84) CLAY 15.90 ( 16.61)

GRAVEL + SAND 9.54 SILT/(SILT+CLAY) 81.63PCT GRAV+SAND/SILT+CLAY 0.11

LABELS SHEPARD -CLAYEY SILT FOLK(GMS)-MUD (SCS)-SILT

PITTS41

SIEVE, SH. PIP., SEDIGRAPH SAMPLE WT.= 4.5500

PHI PCT. CUMPCT.

3.50	5.29	5.29	****0
4.00	7.73	13.02	*****
4.50	17.40	30.41	*****
5.00	15.46	45.88	*****
5.50	8.70	54.58	*****
6.00	9.66	64.24	*****
6.50	5.80	70.04	*****
7.00	5.80	75.84	*****
7.50	4.83	80.67	****
8.00	3.87	84.54	****
8.50	4.83	89.37	***
9.00	2.90	92.27	***
9.50	2.90	95.17	****
10.00	4.83	100.00	
12.00			

MEAN ST.DEV. SKEWNESS KURTOSIS

5.04 1.59 0.34 -0.49 KRUMBEIN+PETTICORN(1938) MOMENT MEASURES  
FOR SIZE RANGE 4.0 TO 10.0 PHI

6.25 1.87 0.41 1.19 FOLK GRAPHIC STATISTICAL PARAMETERS  
FOLK AND WARD, 1957

PERCENTILES MEDIAN 5.74 5TH 3.97 16TH 4.59 25TH 4.84  
75TH 7.43 84TH 8.43 95TH 9.97

PER CENT GRAVEL 0.0 SAND 5.29 SILT 75.44 ( 75.38) CLAY 19.27 ( 19.33)

GRAVEL + SAND 5.29 SILT/(SILT+CLAY) 79.59PCT GRAV+SAND/SILT+CLAY 0.06

LABELS SHEPARD -SILT FOLK(GMS)-MUD (SCS)-SILT

FORMALINE - MOISTURE RESISTANT PAPER



PITT542

SIEVE, SH. PIP., SEDIGRAPH SAMPLE WT.= 4.6900

PHI PCT. CUMPT.

3.50	3.42	***
4.00	6.76	*****
4.50	10.18	*****
5.00	17.39	*****
5.50	27.56	*****
6.00	44.95	*****
6.50	55.57	*****
7.00	66.20	*****
7.50	72.96	*****
8.00	78.75	****
8.50	82.61	****
9.00	86.48	*****
9.50	91.31	***
10.00	94.20	***
10.50	97.10	***
11.00	100.00	

MEAN ST.DEV. SKEWNESS KURTOSIS

6.07 1.53 0.38 -0.31 KRUMBEIN+PETTICORN (1938) MOMENT MEASURES  
FOR SIZE RANGE 4.0 TO 10.0 PHI

6.19 1.71 0.40 1.18 FOLK GRAPHIC STATISTICAL PARAMETERS  
FOLK AND WARD, 1957

PERCENTILES MEDIAN 5.74 5TH 4.12 16TH 4.67 25TH 4.93  
75TH 7.18 84TH 8.18 95TH 9.64

PER CENT GRAVEL 0.0 SAND 3.41 SILT 78.98 ( 79.20) CLAY 17.61 ( 17.39)

GRAVEL + SAND 3.41 SILT/(SILT+CLAY) 82.00PCT GRAV+SAND/SILT+CLAY 0.04

LABELS SHEPARD -SILT FOLK(GMS)-MUD (SCS)-SILT

PITT55

SIEVE, SH. PIP., SEDIGRAPH SAMPLE WT.= 4.0300

PHI PCT. CUMPT.

2.00	0.99	*
2.50	1.99	**
3.00	3.48	***
3.50	6.46	*****
4.00	12.42	*****
4.50	19.43	*****
5.00	31.69	*****
5.50	50.96	*****
6.00	61.47	*****
6.50	70.22	*****
7.00	77.23	*****
7.50	82.48	****
8.00	86.86	****
8.50	90.37	***
9.00	92.99	**
9.50	95.62	*
12.00	100.00	

MEAN ST.DEV. SKEWNESS KUPTOSIS

5.66 1.53 0.18 -0.19 KRUMBEIN+PETTIJOHN(1938) MOMENT MEASURES FOR SIZE RANGE 2.5 TO 9.5 PHI

5.80 1.78 0.28 1.34 FOLK GRAPHIC STATISTICAL PARAMETERS FOLK AND WARD,1957

PERCENTILES MEDIAN 5.48 5TH 3.29 16TH 4.26 25TH 4.73  
75TH 6.84 84TH 7.67 95TH 9.38

PER CENT GRAVEL 0.0 SAND 12.42 SILT 79.50 ( 74.44) CLAY 8.07 ( 13.14)

GRAVEL + SAND 12.42 SILT/(SILT+CLAY) 85.00PCT GRAV+SAND/SILT+CLAY 0.14

LABELS SHEPAD -CLAYEY SILT FOLK(GMS)-SANDY MUD (SGS)-SANDY SILT

PITT56

SIEVE, SH. PIP., SEDIGRAPH SAMPLE WT.= 4.8900

PHI PCT. CUMPCT.

1.50	0.41		
2.00	0.61	0.41	*
2.50	2.04	1.02	**
3.00	11.45	3.07	*****
3.50	13.91	14.52	*****
4.00	15.75	28.43	*****
4.50	19.33	44.17	*****
5.00	14.31	63.50	*****
5.50	9.30	77.81	*****
6.00	6.44	87.12	*****
6.50	3.58	93.56	****
7.00	2.86	97.14	***
12.00		100.00	

MEAN ST.DEV. SKEWNESS KURTOSIS

4.02 1.01 0.04 -0.47 KRUMBEIN+PETTICORN(1938) MOMENT MEASURES  
FOR SIZE RANGE 2.0 TO 7.0 PHI

4.66 1.12 0.09 0.91 FOLK GRAPHIC STATISTICAL PARAMETERS  
FOLK AND WARD, 1957

PERCENTILES MEDIAN 4.65 5TH 3.08 16TH 3.55 25TH 3.88

75TH 5.40 84TH 5.83 95TH 6.70

PER CENT GRAVEL 0.0 SAND 28.43 SILT 7.67 ( 71.57) CLAY 63.91 ( 0.0 )

GRAVEL + SAND 28.43 SILT/(SILT+CLAY) 100.00PCT GRAV+SAND/SILT+CLAY 0.40

LABELS SHEPARD -SANDY SILT FOLK(GMS)-SANDY MUD (SCS)-SANDY SILT

PITT57

SIEVE, SH. PIP., SEDIGRAPH SAMPLE WT.= 6.0000

PHI PCT. CUMPCT.

1.50	0.17		
2.00	0.17	0.17	
2.50	0.17	0.33	
	3.17		***
3.00	3.50		
	13.83		*****
3.50	17.33		
	15.17		*****
4.00	32.50		
	17.05		*****
4.50	49.55		
	18.41		*****
5.00	67.95		
	15.00		*****
5.50	82.95		
	8.86		*****
6.00	91.82		
	4.77		****
6.50	96.59		
	3.41		***
12.00	100.00		

MEAN ST.DEV. SKEWNESS KURTOSIS

4.46 0.92 0.02 -0.74 KRUMBEIN+PETTIJOHN(1938) MOMENT MEASURES FOR SIZE RANGE 2.0 TO 6.5 PHI

4.51 1.02 0.05 0.84 FOLK GRAPHIC STATISTICAL PARAMETERS FOLK AND WARD,1957

PERCENTILES MEDIAN 4.51 5TH 3.05 16TH 3.45 25TH 3.75 75TH 5.23 84TH 5.56 95TH 6.33

PER CENT GRAVEL 0.0 SAND 32.50 SILT 15.42 ( 67.50 ) CLAY 52.08 ( 0.0 )

GRAVEL + SAND 32.50 SILT/(SILT+CLAY) 100.00PCT GRAV+SAND/SILT+CLAY 0.48

LABELS SHEPARD -SANDY SILT FOLK(GMS)-SANDY MUD (SCS)-SANDY SILT

PITT641

SIEVE, SH. PIP., SEDIGRAPH SAMPLE WT.= 6.0600

PHI PCT. CUM.PCT.

1.50	8.75	*****
2.00	0.99	*
2.50	9.74	***
	2.64	
3.00	12.39	*****
	5.62	
3.50	18.00	*****
	7.27	
4.00	25.27	*****
	8.39	
4.50	33.66	*****
	11.44	
5.00	45.10	*****
	15.25	
5.50	60.35	*****
	12.96	
6.00	73.31	*****
	8.39	
6.50	81.70	*****
	6.10	
7.00	87.80	***
	3.05	
7.50	90.85	****
	3.81	
8.00	94.66	*
	0.76	
8.50	95.42	*****
	4.54	
9.00	99.97	
	0.01	
9.50	99.98	
	0.02	
12.00	100.00	

MEAN ST.DEV. SKEWNESS KURTOSIS

5.06 1.74 -0.02 -0.24 KRUMBEIN+PETTIDJOHN(1938) MOMENT MEASURES  
FOR SIZE RANGE 2.0 TO 9.5 PHI

5.06 1.82 -0.07 1.41 FOLK GRAPHIC STATISTICAL PARAMETERS  
FOLK AND WARD,1957

PERCENTILES MEDIAN 5.16 5TH 1.79 16TH 3.32 25TH 3.98  
75TH 6.10 84TH 6.69 95TH 8.22

PER CENT GRAVEL 0.0 SAND 25.27 SILT 69.36 ( 69.39) CLAY 5.37 ( 5.34)

GRAVEL + SAND 25.27 SILT/(SILT+CLAY) 92.86PCT GRAV+SAND/SILT+CLAY 0.34

LABELS SHEPARD -SANDY SILT FOLK(GMS)-SANDY MUD

(SCS)-SANDY SILT

PITT642

SIEVE, SH. PIP., SEDIGRAPH SAMPLE WT.= 5.4800

PHI PCT. CUMPT.

1.50	6.39	*****
2.00	0.73	*
2.50	2.01	**
3.00	3.47	***
3.50	6.58	*****
4.00	7.42	*****
4.50	14.84	*****
5.00	14.84	*****
5.50	11.55	*****
6.00	9.07	*****
6.50	5.77	*****
7.00	5.77	*****
7.50	3.30	***
8.00	3.30	***
8.50	1.65	**
9.00	0.82	*
9.50	0.82	*
10.00	1.65	**
12.00	100.00	

MEAN ST.DEV. SKEWNESS KURTOSIS

5.30 1.70 -0.01 0.04 KRUMBEIN+PETTICORN(1938) MOMENT MEASURES FOR SIZE RANGE 2.0 TO 10.0 PHI

5.39 1.84 0.03 1.49 FOLK GRAPHIC STATISTICAL PARAMETERS FOLK AND WARD, 1957

PERCENTILES MEDIAN 5.29 5TH 1.89 16TH 3.76 25TH 4.39  
75TH 6.39 84TH 7.11 95TH 8.49

PER CENT GRAVEL 0.0 SAND 19.18 SILT 72.60 ( 72.57) CLAY 8.22 ( 8.25)

PITT65

SIEVE, SH. PIP., SEDIGRAPH SAMPLE WT.= 5.8100

PHI	PCT. CUMPT.		
2.50			
	1.20	*	
3.00	1.72	**	
	2.93	***	
3.50	3.27	***	
4.00	6.20	*****	
	4.69	*****	
4.50	10.89	*****	
	9.38	*****	
5.00	20.27	*****	
	15.01	*****	
5.50	35.28	*****	
	15.01	*****	
6.00	50.28	*****	
	11.26	*****	
6.50	61.54	*****	
	8.44	*****	
7.00	69.98	*****	
	7.50	*****	
7.50	77.49	*****	
	4.69	*****	
8.00	82.18	*****	
	3.75	*****	
8.50	85.93	***	
	2.81	***	
9.00	88.74	**	
	1.88	**	
9.50	90.62	**	
	1.88	**	
10.00	92.50	**	
	1.88	**	
10.50	94.37	**	
	1.88	**	
11.00	96.25	****	
	3.75	****	
12.00	100.00		

MEAN ST.DEV. SKEWNESS KUPTOSIS

6.23 1.67 0.33 0.30 KRUMBEIN+PETTICORN(1938) MOMENT MEASURES FOR SIZE RANGE 3.0 TO 11.0 PHI

6.34 1.91 0.33 1.48 FOLK GRAPHIC STATISTICAL PARAMETERS FOLK AND WARD,1957

PERCENTILES MEDIAN 5.99 5TH 3.82 16TH 4.77 25TH 5.16

75TH 7.33 84TH 8.24 95TH 10.67

PER CENT GRAVEL 0.0 SAND 6.20 SILT 76.16 ( 75.98) CLAY 17.64 ( 17.82)

GRAVEL + SAND 6.20 SILT/(SILT+CLAY) 81.00PCT GRAV+SAND/SILT+CLAY 0.07

PITT82

SIEVE, SH. PIP., SEDIGRAPH SAMPLE WT.= 3.7300

PHI PCT. CUMPT.

3.50			*
4.00	0.20		*
	0.99	0.80	
4.50		1.20	
	7.94		*****
5.00		9.73	
	16.86		*****
5.50		26.60	
	17.86		*****
6.00		44.45	
	14.68		*****
6.50		59.23	
	8.93		*****
7.00		68.26	
	8.93		*****
7.50		77.19	
	3.97		****
8.00		81.15	
	4.96		****
8.50		86.11	
	3.97		****
9.00		90.08	
	2.98		***
9.50		93.06	
	2.98		***
10.00		96.03	
	3.97		****
12.00		100.00	

MEAN ST.DEV. SKEWNESS KURTOSIS

6.43 1.34 0.38 -0.11 KRUMBEIN+PETTICORN(1938) MOMENT MEASURES  
FOR SIZE RANGE 4.0 TO 10.0 PHI

6.55 1.55 0.39 1.17 FOLK GRAPHIC STATISTICAL PARAMETERS  
FOLK AND WARD, 1957

PERCENTILES MEDIAN 6.19 5TH 4.70 16TH 5.19 25TH 5.45  
75TH 7.38 84TH 8.29 95TH 9.83

PER CENT GRAVEL 0.0 SAND 0.80 SILT 80.43 ( 80.35) CLAY 18.77 ( 18.85)

GRAVEL + SAND 0.80 SILT/(SILT+CLAY) 81.0CPCT GRAV+SAND/SILT+CLAY 0.01

LABEL'S SHEPARD -SILT FOLK(GMS)-MUD (SCS)-SILT

FORMALINE - MOISTURE TOL. 1.1



PI++ 951 0 0.0 0 0.0 0

\*\*\*\*\*  
 \*\*\*\* MULTIMODAL SAMPLE \*\*\*\*  
 \*\*\*\*  
 \*\*\*\*\*

WET WT	DRY WT	SALT	ORGANIC	MOISTURE	WEIGHT LOSS DUE TO HANDLING	0.0
1000.0000	6.3900	0.0	0.0	0.0 (GRAMS)	GRAVEL CORRECTION FACTOR	1.000
100.0000	100.0000	0.0	0.0	0.0 (PCT WET WT)	SIZES ELIMINATED (<0.01%)	NONE
					TRASK SORTING COEFFICIENT	2.242
					USING PROBABILITY EXTRAP.	2.224
					MEAN CUBED DEVIATION	9.380
					USING PROBABILITY EXTRAP.	5.372

PERCENTAGE COMPOSITION		TABLE OF STATISTICAL DATA IN PHI UNITS				PERCENTILES		LINEAR EXTRAP.		PROBABILITY EXTRAP.	
		MEAN	STD DEV	SKEWNESS	KURTOSIS	MM.	PHI UNITS	MM.	PHI UNITS		
GRAVEL	0.0	MOMENT 4.74961	1.91004	1.34607	5.67573	5.0	0.17490	2.51538	0.17335	2.52825	
SAND	39.12	P-MOMENT 4.72235	1.76116	0.96339	3.97031	10.0	0.15370	2.70181	0.14729	2.76322	
SILT	55.33	FOLK 4.55532	1.71081	0.21660	1.00573	16.0	0.13162	2.92553	0.12951	2.94891	
CLAY	5.54	P-FOLK 4.55836	1.65731	0.21885	1.01146	25.0	0.10050	3.31470	0.09944	3.32996	
MUD	60.88	INMAN 4.61461	1.68908	0.10531	0.69245	50.0	0.04617	4.43674	0.04615	4.43747	
S/H	0.64	P-INMAN 4.61881	1.66990	0.10859	0.70418	75.0	0.01999	5.64453	0.02011	5.63616	
		KRUMBEIN 1.72580	0.04288	0.27225		84.0	0.01266	6.30369	0.01279	6.28670	
		P-KRUM. 1.70830	0.04559	0.27358		90.0	0.00792	6.98061	0.00793	6.97603	
		FOLK (TRANSFORMED)		0.50143		95.0	0.00332	8.23277	0.00355	8.21986	
		P-FOLK (TRANSFORMED)		0.50285							

DATA FOR CONSTN OF BARGRAPHS AND CUM. CURVES

SIZE FRACTION		WT.(GMS)		WT.PCT.		MID PHI(LINEAR)		MID PHI(PROB.)		MODE
MM	PHI	UNCOR	COR	COR	CUMUL.	PHI	MM	PHI	MM	
0.250000	2.000	0.100	0.100	1.565	1.565	1.751	0.29707	1.917	0.26483	0
0.177000	2.498	0.190	0.190	2.973	4.538	2.249	0.21036	2.302	0.20278	0
0.125000	3.000	0.860	0.860	13.459	17.997	2.749	0.14875	2.808	0.14280	1
0.088000	3.506	0.720	0.720	11.268	29.264	3.253	0.10488	3.270	0.10566	0
0.062500	4.000	0.630	0.630	9.859	39.124	3.753	0.07416	3.760	0.07381	0
0.044000	4.506	0.806	0.806	12.610	51.733	4.253	0.05244	4.255	0.05236	1
0.031000	5.012	0.491	0.491	7.682	59.415	4.759	0.03693	4.757	0.03698	0
0.022000	5.506	0.864	0.864	13.528	72.944	5.259	0.02612	5.249	0.02629	1*
0.015600	6.002	0.472	0.472	7.380	80.323	5.754	0.01853	5.743	0.01867	0
0.011000	6.506	0.393	0.393	6.149	86.472	6.254	0.01310	6.239	0.01324	0
0.007800	7.002	0.236	0.236	3.689	90.161	6.754	0.00926	6.740	0.00935	0
0.005500	7.506	0.157	0.157	2.460	92.621	7.254	0.00655	7.241	0.00661	0
0.003900	8.002	0.118	0.118	1.844	94.466	7.754	0.00463	7.740	0.00468	0
0.002700	8.533	0.079	0.079	1.230	95.696	8.268	0.00325	8.254	0.00328	0
0.001900	9.040	0.079	0.079	1.230	96.926	8.786	0.00227	8.769	0.00229	0
0.001360	9.561	0.039	0.039	0.815	97.541	9.270	0.00162	9.260	0.00163	0
0.000661	14.000	0.157	0.157	2.459	100.000	11.751	0.00029	10.218	0.00084	0
TOTALS		6.390	6.390	100.0						

PI+ 952 0 0.0 0 0.0 0

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 MULTIMODAL SAMPLE  
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WET WT 1000.0000  
 DRY WT 5.7900  
 SALT 0.0  
 ORGANIC 0.0  
 MOISTURE 0.0 (GRAMS)  
 100.0000 100.0000 0.0 0.0 0.0 (PCT WET WT)

WEIGHT LOSS DUE TO HANDLING 0.0  
 GRAVEL CORRECTION FACTOR 1.000  
 SIZES ELIMINATED (<0.01%) NONE  
 TRASK SORTING COEFFICIENT 2.426  
 USING PROBABILITY EXTRAP. 2.421  
 MEAN CUBED DEVIATION 17.675  
 USING PROBABILITY EXTRAP. 13.842

PERCENTAGE COMPOSITION

TABLE OF STATISTICAL DATA IN PHI UNITS

PERCENTILES LINEAR EXTRAP.

PROBABILITY EXTRAP.

		MEAN	STD DEV	SKWENESS	KURTOSIS	MM.	PHI UNITS	MM.	PHI UNITS
GRAVEL 0.0	MOMENT 5.15597	2.33109	1.39538	5.10602	5.0	0.17082	2.54946	0.16682	2.58360
SAND 35.58	P-MOMENT 5.13887	2.22652	1.29405	4.44919	10.0	0.14731	2.76310	0.14130	2.82316
SILT 54.00	FOLK 4.92506	2.15752	0.29696	1.21506	16.0	0.12302	3.02303	0.12269	3.02686
CLAY 10.42	P-FOLK 4.92543	2.14584	0.30026	1.21529	25.0	0.08975	3.47796	0.08954	3.48139
MUD 64.42	INMAN 5.03339	2.01036	0.16166	0.89156	50.0	0.03825	4.70839	0.03825	4.70837
S/M 0.55	P-INMAN 5.03396	2.00710	0.16222	0.88469	75.0	0.01525	6.03483	0.01527	6.03274
	KRUMBEIN 1.88938	0.04800	0.23891		84.0	0.00758	7.04375	0.00759	7.04107
	P-KRUM. 1.88989	0.04809	0.24140		90.0	0.00361	8.11419	0.00363	8.10767
	FOLK (TRANSFORMED) 0.54936				95.0	0.00088	10.15487	0.00088	10.14913
	P-FOLK (TRANSFORMED) 0.54859								

DATA FOR CONSTN OF BARGRAPHS AND CUM. CURVES

SIZE FRACTION	WT.(GMS)	WT.PCT.	WT.PCT.	MID PHI(LINEAR)	MID PHI(PROB.F)	MCDE				
MM	PHI	UNCR	CCR	COR	CUMUL.	PHI	MM	PHI	MM	
0.25000	2.000	0.080	0.080	1.382	1.382	1.751	0.29707	1.916	0.26585	0
0.17700	2.498	0.140	0.140	2.418	3.800	2.249	0.21036	2.300	0.20306	0
0.12500	3.000	0.680	0.680	11.744	15.544	2.749	0.14875	2.811	0.14253	1
0.08800	3.506	0.580	0.580	10.317	25.861	3.253	0.10488	3.272	0.10354	0
0.06250	4.000	0.580	0.580	10.317	35.579	3.753	0.07416	3.762	0.07370	0
0.04400	4.506	0.764	0.764	13.191	48.769	4.253	0.05244	4.257	0.05229	1
0.03100	5.012	0.178	0.178	3.077	51.846	4.759	0.03693	4.759	0.03693	0
0.02200	5.506	0.867	0.867	14.967	66.814	5.259	0.02612	5.253	0.02622	1*
0.01560	6.002	0.452	0.452	7.808	74.622	5.754	0.01853	5.747	0.01863	0
0.01100	6.506	0.339	0.339	5.857	80.478	6.254	0.01310	6.245	0.01319	0
0.00780	7.002	0.188	0.188	3.254	83.732	6.754	0.00926	6.747	0.00931	0
0.00550	7.506	0.188	0.188	3.253	86.985	7.254	0.00655	7.245	0.00659	0
0.00390	8.002	0.151	0.151	2.603	89.588	7.754	0.00463	7.745	0.00466	0
0.00270	8.533	0.113	0.113	1.953	91.541	8.268	0.00325	8.257	0.00327	0
0.00190	9.040	0.075	0.075	1.301	92.842	8.766	0.00227	8.778	0.00228	0
0.00130	9.501	0.075	0.075	1.301	94.143	9.270	0.00162	9.261	0.00165	0
0.00090	9.955	0.038	0.038	0.651	94.794	9.748	0.00116	9.742	0.00117	0
0.00060	10.501	0.038	0.038	0.650	95.445	10.248	0.00082	10.241	0.00083	0
0.00040	10.955	0.038	0.038	0.651	96.096	10.748	0.00058	10.740	0.00058	1
0.00030	11.522	0.038	0.038	0.650	96.746	11.259	0.00041	11.249	0.00041	0
0.00001	14.000	0.188	0.188	3.254	100.000	12.761	0.00014	11.908	0.00026	0

TOTALS 5.790 5.790 100.0



P1++ 98 0 0.0 0 0.0 0

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 \*\*\* MULTIMODAL SAMPLE \*\*\*  
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WET WT	DRY WT	SALT	ORGANIC	MOISTURE	WEIGHT LOSS DUE TO HANDLING	0.0
1000.0000	6.7700	0.0	0.0	0.0 (GRAMS)	GRAVEL CORRECTION FACTOR	1.000
100.0000	100.0000	0.0	0.0	0.0 (PCT WET WT)	SIZES ELIMINATED (<0.01%)	NONE
					TRASK SORTING COEFFICIENT	1.801
					USING PROBABILITY EXTRAP.	1.782
					MEAN CUBED DEVIATION	8.605
					USING PROBABILITY EXTRAP.	4.133

PERCENTAGE COMPOSITION	TABLE OF STATISTICAL DATA IN PHI UNITS				PERCENTILES		LINEAR EXTRAP.		PROBABILITY EXTRAP.	
	MEAN	STD DEV	SKWNESS	KURTOSIS	MM.	PHI UNITS	MM.	PHI UNITS		
GRAVEL 0.0	5.26624	1.73119	1.05843	6.55374	5.0	0.10766	3.21544	0.10213	3.29147	
SAND 19.06	5.22036	1.52912	1.15610	4.27895	10.0	0.08548	3.54833	0.08478	3.56005	
SILT 73.65	5.11119	1.49720	0.26747	1.31726	16.0	0.06946	3.84762	0.06333	3.37139	
CLAY 7.29	5.11869	1.47607	0.28043	1.31773	25.0	0.05608	4.15642	0.05531	4.17234	
MUD 80.94	5.18855	1.34094	0.17309	1.03455	50.0	0.03221	4.95645	0.03219	4.95716	
S/M 0.24	5.19945	1.32806	0.18244	1.01780	75.0	0.01729	5.85407	0.01742	5.84324	
		1.25752	0.04879	0.22412	84.0	0.01082	6.52949	0.01384	6.52751	
		1.23474	0.05263	0.22151	90.0	0.00619	7.33570	0.00625	7.32265	
				0.56846	95.0	0.00245	8.67187	0.00249	8.65097	
				0.56854						

DATA FOR CONSTN OF BARGRAPHS AND CUM. CURVES

SIZE FRACTION	WT.(GMS)	WT.PCT.	WT.PCT.	MID PHI(LINEAR)	MID PHI(PROB.)	MODE
MM	PHI	UNCOR	COR	PHI	MM	MM
0.250000	2.000	0.010	0.010	0.148	0.148	0
0.177000	2.498	0.010	0.010	0.148	0.295	0
0.125000	3.000	0.110	0.110	1.625	1.920	0
0.088000	3.500	0.490	0.490	7.238	9.158	0
0.062500	4.000	0.670	0.670	9.897	19.055	0
0.044000	4.506	1.303	1.303	19.244	38.298	1*
0.031000	5.012	0.885	0.885	13.134	51.433	0
0.022000	5.506	1.096	1.096	16.189	67.622	0
0.015600	6.002	0.712	0.712	10.523	78.145	0
0.011000	6.506	0.384	0.384	5.666	83.811	0
0.007800	7.002	0.274	0.274	4.047	87.858	0
0.005500	7.506	0.219	0.219	3.238	91.096	0
0.003900	8.002	0.110	0.110	1.619	92.715	0
0.002700	8.533	0.110	0.110	1.619	94.334	0
0.001900	9.040	0.164	0.164	2.428	96.762	0
0.000001	14.000	0.219	0.219	3.238	100.000	0
TOTALS		6.770	6.770	100.0		
0.250000	0.020000					
0.177000	0.020000					
0.125000	0.210000					
0.088000	0.670000					

P1+ 99 0 0.0 0 0.0 0

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 \*\*\* MULTIMODAL SAMPLE \*\*\*  
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WET WT	DRY WT	SALT	ORGANIC	MOISTURE	WEIGHT LOSS DUE TO HANDLING	0.0
1000.0000	5.4300	0.0	0.0	0.0 (GRAMS)	GRAVEL CORRECTION FACTOR	1.000
100.0000	100.0000	0.0	0.0	0.0 (PCT WET WT)	SIZES ELIMINATED (<0.01%)	NONE
					TRASK SORTING COEFFICIENT	2.193
					USING PROBABILITY EXTRAP.	2.176
					MEAN CUBED DEVIATION	16.012
					USING PROBABILITY EXTRAP.	11.598

PERCENTAGE COMPOSITION		TABLE OF STATISTICAL DATA IN PHI UNITS				PERCENTILES		LINEAR EXTRAP.		PROBABILITY EXTRAP.	
		MEAN	STD DEV	SKWENESS	KURTOSIS	MM.	PHI UNITS	MM.	PHI UNITS		
GRAVEL	0.0	5.33070	2.19224	1.51979	5.34212	5.0	0.12360	3.01623	0.12263	3.02757	
SAND	31.12	5.30554	2.06007	1.32656	4.44995	10.0	0.10721	3.22142	0.10293	3.28023	
SILT	58.21	5.11276	1.52846	0.31398	1.26067	16.0	0.09039	3.46764	0.08963	3.47589	
CLAY	10.66	5.11580	1.92270	0.31674	1.27099	25.0	0.07245	3.78682	0.07148	3.80624	
MUD	68.88	5.21293	1.74529	0.17218	0.99634	50.0	0.03321	4.91242	0.03320	4.91256	
S/M	0.45	5.21742	1.73753	0.17546	1.00169	75.0	0.01507	6.05220	0.01510	6.04924	
		KRUMBEIN	1.67806	0.00709	0.22545	84.0	0.00804	6.95822	0.00806	6.95495	
		P-KRUM.	1.66148	0.01518	0.22618	90.0	0.00329	8.24550	0.00331	8.23863	
		FOLK (TRANSFORMED)			0.55765	95.0	0.00099	9.98463	0.00099	9.98357	
		P-FOLK (TRANSFORMED)			0.55966						

DATA FOR CONSTN OF BARGRAPHS AND CUM. CURVES

SIZE FRACTION	WT.(GMS)	WT.PCT.	WT.PCT.	MID PHI(LINEAR)	MID PHI(PROB.)	MODE				
MM	PHI	UNCOR	COR	COR	CUMUL.	PHI	MM	PHI	MM	
0.250000	2.000	0.020	0.020	0.368	0.368	1.751	0.29707	1.997	0.26858	0
0.177000	2.498	0.020	0.020	0.368	0.737	2.249	0.21036	2.287	0.20494	0
0.125000	3.000	0.210	0.210	3.867	4.604	2.749	0.14875	2.836	0.14009	0
0.088000	3.506	0.670	0.670	12.335	16.943	3.253	0.10488	3.310	0.10083	0
0.062500	4.000	0.770	0.770	14.180	31.123	3.753	0.07416	3.774	0.07312	0
0.044000	4.506	0.801	0.801	14.758	45.881	4.253	0.05244	4.260	0.05218	1*
0.031000	5.012	0.278	0.278	5.124	51.006	4.759	0.03693	4.759	0.03692	0
0.022000	5.506	0.733	0.733	13.491	64.496	5.259	0.02612	5.255	0.02619	1
0.015600	6.002	0.540	0.540	9.941	74.437	5.754	0.01853	5.745	0.01864	0
0.011000	6.506	0.308	0.308	5.680	80.118	6.254	0.01310	6.245	0.01318	0
0.007800	7.002	0.231	0.231	4.261	84.378	6.754	0.00926	6.745	0.00932	0
0.005500	7.506	0.116	0.116	2.130	86.508	7.254	0.00655	7.248	0.00658	0
0.003900	8.002	0.154	0.154	2.841	89.349	7.754	0.00463	7.744	0.00466	1
0.002700	8.523	0.077	0.077	1.420	90.765	8.268	0.00325	8.261	0.00326	0
0.001900	9.040	0.077	0.077	1.421	92.190	8.786	0.00227	8.778	0.00228	1
0.001300	9.561	0.077	0.077	1.420	93.610	9.270	0.00162	9.262	0.00163	0
0.000900	9.995	0.077	0.077	1.420	95.029	9.748	0.00116	9.736	0.00117	0
0.000600	10.501	0.039	0.039	0.710	95.739	10.248	0.00082	10.240	0.00083	0
0.000400	10.995	0.039	0.039	0.710	96.449	10.748	0.00058	10.739	0.00059	0
0.000001	14.000	0.193	0.193	3.551	100.000	12.497	0.00017	11.460	0.00036	0
TOTALS		5.430	5.430	100.0						

Pl+ 100 0 0.0 0 0.0 0

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 \*\*\* MULTIMODAL SAMPLE \*\*\*  
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WET WT	DRY WT	SALT	ORGANIC	MOISTURE	WEIGHT LOSS DUE TO HANDLING	0.0
1000.0000	4.7200	0.0	0.0	0.0 (GFAMS)	GRAVEL CORRECTION FACTOR	1.000
100.0000	100.0000	0.0	0.0	0.0 (PCT WET WT)	SIZES ELIMINATED (<0.01#)	NONE
					TRASK SORTING COEFFICIENT	2.195
					USING PROBABILITY EXTRAP.	2.182
					MEAN CUBED DEVIATION	12.218
					USING PROBABILITY EXTRAP.	7.380

PERCENTAGE COMPOSITION		TABLE OF STATISTICAL DATA IN PHI UNITS					PERCENTILES		LINEAR EXTRAP.		PROBABILITY EXTRAP.	
		MEAN	STD DEV	SKEWNESS	KURTOSIS		MM.	PHI UNITS	MM.	PHI UNITS		
GRAVEL	0.0	5.09805	2.07450	1.36855	9.37042	5.0	0.16576	2.95280	0.16121	2.63301		
SAND	33.05	5.05563	1.91164	1.05644	4.07106	10.0	0.13111	2.93116	0.12931	2.95103		
SILT	58.82	4.90006	1.87253	0.18781	1.23182	16.0	0.10562	3.24303	0.10364	3.27035		
CLAY	8.12	4.90657	1.85647	0.19445	1.23268	25.0	0.07917	3.65892	0.07850	3.67107		
MUD	66.95	4.92217	1.67914	0.03951	1.03006	50.0	0.03453	4.85583	0.03453	4.85601		
S/M	0.49	4.93186	1.66151	0.04565	1.03721	75.0	0.01643	5.92716	0.01649	5.92163		
		KRUMBEIN	1.68018	-0.06279	0.24599	84.0	0.01030	6.60131	0.01036	6.99336		
		P-KRUM.	1.66723	-0.05956	0.24529	90.0	0.00537	7.54152	0.00538	7.53897		
		P-FOLK (TRANSFORMED)			0.55193	95.0	0.00147	9.41031	0.00148	9.40272		
		P-FOLK (TRANSFORMED)			0.59211							

DATA FOR CONSTN OF BARGRAPHS AND CUM. CURVES

SIZE FRACTION	WT.(GMS)		WT.PCT.		MID PHI(LINEAR)		MID PHI(PROB.)		MODE	
	MM	PHI	UNCOR	COR	PHI	MM	PHI	MM		
0.250000	2.000	0.080	0.080	1.695	1.695	1.751	0.29707	1.918	0.26469	0
0.177000	2.498	0.090	0.090	1.907	3.602	2.249	0.21036	2.288	0.20482	0
0.125000	3.000	0.350	0.350	7.415	11.017	2.749	0.14875	2.801	0.14350	0
0.088000	3.506	0.490	0.490	10.381	21.398	3.253	0.10488	3.280	0.10293	0
0.062500	4.030	0.550	0.550	11.653	33.051	3.753	0.07416	3.766	0.07349	0
0.044000	4.506	0.590	0.590	12.492	45.542	4.253	0.05244	4.259	0.05224	1
0.031000	5.012	0.304	0.304	6.444	51.986	4.759	0.03693	4.759	0.03692	0
0.022000	5.506	0.734	0.734	15.554	67.540	5.259	0.02612	5.253	0.02623	1*
0.015600	6.002	0.415	0.415	8.791	76.332	5.754	0.01853	5.745	0.01865	0
0.011000	6.506	0.319	0.319	6.762	83.853	6.254	0.01310	6.242	0.01322	0
0.007800	7.002	0.223	0.223	4.734	87.827	6.754	0.00926	6.741	0.00935	0
0.005500	7.506	0.096	0.096	2.029	89.856	7.254	0.00655	7.246	0.00654	0
0.003900	8.002	0.096	0.096	2.029	91.889	7.754	0.00463	7.744	0.00466	1
0.002700	8.533	0.032	0.032	0.677	92.562	8.268	0.00325	8.263	0.00325	0
0.001900	9.040	0.064	0.064	1.353	93.914	8.786	0.00227	8.776	0.00228	1
0.001300	9.501	0.064	0.064	1.352	95.266	9.270	0.00152	9.259	0.00163	0
0.000980	9.995	0.064	0.064	1.353	96.619	9.748	0.00116	9.731	0.00118	0
0.000061	14.000	0.160	0.160	3.381	100.000	11.997	0.00024	10.617	0.00064	0
TOTALS		4.720	4.720	100.0						
0.250000	0.010000									
0.177000	0.010000									

PI++ 101 0 0.0 0 0.0 0

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 \*\*\* MULTIMODAL SAMPLE \*\*\*  
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WET WT	DPY WT	SALT	ORGANIC	MOISTURE	WEIGHT LOSS DUE TO HANDLING	0.0
1000.0000	4.8400	0.0	0.0	0.0 (GRAMS)	GRAVEL CORRECTION FACTOR	1.000
100.0000	100.0000	0.0	0.0	0.0 (PCT WET WT)	SIZES ELIMINATED (<0.015)	NONE
					TRASK SORTING COEFFICIENT	2.126
					USING PROBABILITY EXTRAP.	2.111
					MEAN CUBED DEVIATION	10.645
					USING PROBABILITY EXTRAP.	5.890

PERCENTAGE COMPOSITION	TABLE OF STATISTICAL DATA IN PHI UNITS					PERCENTILES	LINEAR EXTRAP.		PROBABILITY EXTRAP.	
	MEAN	STD DEV	SKEWNESS	KURTOSIS			MM.	PHI UNITS	MM.	PHI UNITS
GRAVEL 0.0	MOMENT 5.52242	2.01606	1.32339	5.18020	5.0	0.12375	3.01445	0.12310	3.02204	
SAND 21.69	P-MOMENT 5.47572	1.83114	0.95931	3.76718	10.0	0.10109	3.30621	0.09816	3.34874	
SILT 69.49	FCLK 5.38578	1.87543	0.23600	1.19936	16.0	0.07912	3.65586	0.07319	3.67688	
CLAY 8.81	P-FOLK 5.38791	1.86673	0.23842	1.20819	25.0	0.05576	4.16483	0.05532	4.17596	
MUD 78.31	INMAN 5.48106	1.82120	0.15694	0.74826	50.0	0.02729	5.19524	0.02731	5.19443	
S/M 0.28	P-INMAN 5.48466	1.80779	0.16055	0.75761	75.0	0.01234	6.34061	0.01242	6.33160	
	KRUMBEIN 1.61184	0.05738	0.23710		84.0	0.00634	7.30225	0.00638	7.29245	
	P-KRUM. 1.59677	0.05935	0.23792		90.0	0.00420	7.89491	0.00425	7.87886	
	FOLK (TRANSFORMED) 0.54532				95.0	0.00150	9.38232	0.00150	9.37680	
	P-FOLK (TRANSFORMED) 0.54714									

DATA FOR CONSTN OF BARGRAPHS AND CUM. CURVES

SIZE FRACTION	WT.(GMS)		WT.PCT.		MID PHI(LINEAR)		MID PHI(PROB.)		MODE	
	MM	PHI	UNCOR	COR	PHI	MM	PHI	MM		
0.250000	2.000	0.010	0.010	0.207	0.207	1.751	0.29707	1.884	0.27096	0
0.177000	2.498	0.010	0.010	0.207	0.413	2.249	0.21036	2.287	0.20087	0
0.125000	3.000	0.210	0.210	4.239	4.752	2.749	0.14875	2.857	0.13601	0
0.080000	3.506	0.420	0.420	8.678	13.430	3.753	0.10488	3.301	0.13149	1
0.062500	4.000	0.400	0.400	8.264	21.654	3.753	0.07416	3.772	0.07321	0
0.044000	4.506	0.492	0.492	10.166	31.861	4.253	0.05244	4.265	0.05200	0
0.031000	5.012	0.591	0.591	12.207	44.067	4.759	0.03693	4.765	0.03677	0
0.022000	5.506	0.774	0.774	15.981	60.049	5.259	0.02612	5.258	0.02614	1*
0.015600	6.002	0.464	0.464	9.588	69.636	5.754	0.01853	5.748	0.01861	0
0.011000	6.506	0.387	0.387	7.991	77.627	6.254	0.01310	6.244	0.01319	0
0.007800	7.002	0.193	0.193	3.995	81.622	6.754	0.00926	6.747	0.00931	0
0.005500	7.506	0.193	0.193	3.996	85.618	7.254	0.00655	7.244	0.00660	0
0.003900	8.002	0.271	0.271	5.593	91.211	7.754	0.00463	7.733	0.00470	1
0.002700	8.523	0.077	0.077	1.598	92.809	8.268	0.00325	8.257	0.00327	0
0.001900	9.040	0.077	0.077	1.598	94.407	8.786	0.00227	8.774	0.00228	0
0.001360	9.561	0.039	0.039	0.799	95.206	9.270	0.00162	9.263	0.00163	0
0.000980	9.995	0.039	0.039	0.800	96.005	9.748	0.00116	9.739	0.00117	0
0.00061	14.000	0.193	0.193	3.995	100.000	11.997	0.00024	10.610	0.00064	0
TOTALS		4.840	4.840	100.0						
0.250000	0.020000									
0.177000	0.020000									

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PI++ 102 0 0.0 0 0.0 0

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 \*\*\* MULTIMODAL SAMPLE \*\*\*  
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WET WT	DRY WT	SALT	ORGANIC	MOISTURE	WEIGHT LOSS DUE TO HANDLING	0.0
1000.0000	5.4100	0.0	0.0	0.0 (GRAMS)	GRAVEL CORRECTION FACTOR	1.000
100.0000	100.0000	0.0	0.0	0.0 (PCT WET WT)	SIZES ELIMINATED (<0.01%)	NONE
					TRASK SORTING COEFFICIENT	2.017
					USING PROBABILITY EXTRAP.	2.002
					MEAN CUBED DEVIATION	12.881
					USING PROBABILITY EXTRAP.	7.662

PERCENTAGE COMPOSITION		TABLE OF STATISTICAL DATA IN PHI UNITS				PERCENTILES		LINEAR EXTRAP.		PROBABILITY EXTRAP.	
		MEAN	STD DEV	SKEWNESS	KURTOSIS	MM.	PHI UNITS	MM.	PHI UNITS		
GRAVEL	0.0	MOMENT	5.08636	1.97381	1.67507	6.37854	5.0	0.13293	2.91127	0.12919	2.95247
SAND	30.31	P-MOMENT	5.04853	1.79259	1.33018	4.78206	10.0	0.11359	3.13614	0.10966	3.18889
SILT	61.86	FOLK	4.84776	1.71079	0.26086	1.23885	16.0	0.09668	3.54105	0.09590	3.38230
CLAY	7.83	P-FOLK	4.86036	1.69333	0.27275	1.24351	25.0	0.07580	3.72170	0.07517	3.73370
MUD	69.69	INMAN	4.90792	1.56687	0.11519	0.95312	50.0	0.03775	4.72744	0.03776	4.72710
S/M	0.44	P-INMAN	4.92698	1.54468	0.12940	0.96756	75.0	0.01863	5.74650	0.01875	5.73706
		KPUM&EIN		1.45985	0.00666	0.23910	84.0	0.01124	6.47479	0.01127	6.47167
		P-KPUM.		1.48397	0.00828	0.24001	90.0	0.00604	7.37236	0.00608	7.36245
		FCLK (TRANSFORMED)				0.55334	95.0	0.00191	9.03183	0.00191	9.03099
		P-FOLK (TRANSFORMED)				0.55427					

DATA FOR CONSTN OF BARGRAPHS AND CUM. CURVES

SIZE FRACTION	WT.(GMS)	WT.PCT.	WT.PCT.	MID PHI(LINEAR)	MID PHI(PROB.)	MODE
MM	PHI	UNCOR	COR	COR	CUMUL. PHI	MM
0.250000	2.600	0.020	0.020	0.370	0.370	1
0.177000	2.498	0.020	0.020	0.370	0.739	0
0.125000	3.000	0.280	0.280	5.176	5.915	0
0.084000	3.506	0.810	0.810	14.972	20.887	1
0.062500	4.000	0.510	0.510	9.427	30.314	0
0.044000	4.506	0.726	0.726	13.424	43.738	0
0.031000	5.012	0.774	0.774	14.308	58.046	1
0.022000	5.506	0.731	0.731	13.510	71.556	0
0.015600	6.002	0.385	0.385	7.111	78.667	0
0.011000	6.506	0.308	0.308	5.689	84.356	0
0.007800	7.002	0.192	0.192	3.555	87.911	0
0.005500	7.506	0.154	0.154	2.845	90.756	0
0.003900	8.002	0.077	0.077	1.422	92.178	0
0.002700	8.533	0.077	0.077	1.422	93.601	1
0.001900	9.040	0.077	0.077	1.421	95.022	0
0.001360	9.501	0.038	0.038	0.712	95.734	0
0.000980	9.995	0.038	0.038	0.711	96.445	0
0.000661	14.000	0.192	0.192	3.555	100.000	0
TOTALS		5.410	5.410	100.0	11.997	0.00024
0.250000	0.040000					10.614
0.177000	0.040000					0.00064

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 \*\*\* MULTIMODAL SAMPLE \*\*\*  
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WET WT	DRY WT	SALT	ORGANIC	MOISTURE	WEIGHT LOSS DUE TO HANDLING	0.0
100.0000	5.2300	0.0	0.0	0.0 (GRAMS)	GRAVEL CORRECTION FACTOR	1.000
100.0000	100.0000	0.0	0.0	0.0 (PCT WET WT)	SIZES ELIMINATED (<0.01%)	NONE
					TRASK SORTING COEFFICIENT	2.322
					USING PROBABILITY EXTRAP.	2.303
					MEAN CUBED DEVIATION	13.387
					USING PROBABILITY EXTRAP.	8.913

PERCENTAGE COMPOSITION		TABLE OF STATISTICAL DATA IN PHI UNITS					PERCENTILES	LINEAR EXTRAP.	PROBABILITY EXTRAP.	
		MEAN	STD DEV	SKEWNESS	KURTOSIS		MM.	PHI UNITS	MM.	PHI UNITS
GRAVEL	0.0	5.42505	2.16972	1.27502	4.62785	5.0	0.13451	2.89417	0.13122	2.92494
SAND	28.87	5.39094	2.04531	1.04163	3.67795	10.0	0.11036	3.17974	0.10878	3.22725
SILT	59.62	5.28508	2.01018	0.23695	1.17038	16.0	0.09185	3.44456	0.09082	3.46080
CLAY	11.51	5.28703	1.99569	0.24147	1.17304	25.0	0.07015	3.83338	0.06944	3.84807
MUD	71.13	5.36103	1.91647	0.11889	0.81136	50.0	0.02849	5.13318	0.02852	5.13153
S/M	0.41	5.36458	1.90377	0.12221	0.80932	75.0	0.01301	6.26456	0.01309	6.25496
			1.80088	-0.08421	0.22622	84.0	0.00645	7.27749	0.00649	7.26835
			1.78288	-0.08041	0.22600	90.0	0.00266	8.55334	0.00266	8.55226
					0.53925	95.0	0.00109	9.83695	0.00111	9.81902
					0.53982					

DATA FOR CONSTN OF BARGRAPHS AND CUM. CURVES

SIZE FRACTION	WT.(GMS)	WT.PCT.	WT.PCT.	MID PHI(LINEAR)	MID PHI(PROB.)	MODE
MM	PHI	UNCOR	COR	COR	CUMUL. PHI	MM
0.250000	2.000	0.040	0.040	0.765	0.765	1.751
0.177000	2.498	0.040	0.040	0.765	1.530	2.249
0.125000	3.000	0.230	0.230	4.398	5.927	2.749
0.088000	3.506	0.600	0.600	11.472	17.400	3.253
0.062500	4.000	0.630	0.600	11.472	28.872	3.753
0.044000	4.506	0.658	0.658	12.579	41.451	4.253
0.031000	5.012	0.244	0.244	4.663	46.115	4.755
0.022000	5.506	0.827	0.827	15.807	61.922	5.259
0.015600	6.002	0.488	0.488	9.339	71.261	5.754
0.011000	6.506	0.376	0.376	7.185	78.447	6.254
0.007800	7.002	0.188	0.188	3.592	82.038	6.754
0.005500	7.506	0.188	0.188	3.593	85.631	7.254
0.003900	8.002	0.150	0.150	2.874	88.505	7.754
0.002700	8.533	0.075	0.075	1.437	89.942	8.268
0.001900	9.040	0.075	0.075	1.437	91.379	8.786
0.001300	9.501	0.113	0.113	2.155	93.534	9.270
0.000980	9.995	0.113	0.113	2.156	95.689	9.748
0.000690	10.501	0.038	0.038	0.718	96.407	10.248
0.000001	14.000	0.188	0.188	3.593	100.000	12.251
TOTALS		5.230	5.230	100.0		
0.250000	0.010000					

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PI++ 104 0 0.0 0 0.0 0

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 \*\*\*\* MULTIMODAL SAMPLE \*\*\*\*  
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WET WT	DRY WT	SALT	ORGANIC	MOISTURE	WEIGHT LOSS DUE TO HANDLING	0.0
1000.0000	5.4300	0.0	0.0	0.0 (GRAMS)	GRAVEL CORRECTION FACTOR	1.000
100.0000	100.0000	0.0	0.0	0.0 (PCT WET WT)	SIZES ELIMINATED (K.O.%)	NONE
					TRASK SORTING COEFFICIENT	1.958
					USING PROBABILITY EXTRAP.	1.936
					MEAN CUBED DEVIATION	10.132
					USING PROBABILITY EXTRAP.	4.940

PERCENTAGE COMPOSITION		TABLE OF STATISTICAL DATA IN PHI UNITS				PERCENTILES		LINEAR EXTRAP.		PROBABILITY EXTRAP.	
		MEAN	STD DEV	SKEWNESS	KURTOSIS	MM.	PHI UNITS	MM.	PHI UNITS		
GRAVEL	0.0	4.9899	1.80668	1.71812	6.62580	5.0	0.11947	3.00524	0.11558	3.11305	
SAND	33.52	4.94479	1.59203	1.22423	4.29290	10.0	0.10447	3.25667	0.09961	3.32748	
SILT	60.37	4.78555	1.52050	0.40064	1.10450	16.0	0.08893	3.49122	0.08858	3.49694	
CLAY	6.12	4.78548	1.50650	0.40603	1.10872	25.0	0.07409	3.75449	0.07291	3.77781	
MUD	66.48	4.94883	1.45761	0.33522	0.79239	50.0	0.04543	4.46021	0.04539	4.46143	
S/M	0.50	4.94751	1.45057	0.33509	0.77724	75.0	0.01933	5.69335	0.01945	5.68373	
			1.43620	0.26371	0.24844	84.0	0.01179	6.40644	0.01186	6.39808	
			1.41179	0.26934	0.24931	90.0	0.00699	7.16100	0.00704	7.14987	
					0.52483	95.0	0.00319	8.29045	0.00324	8.26907	
					0.52578						

DATA FOR CONSTN OF BARGRAPHS AND CUM. CURVES

SIZE FRACTION	WT.(GMS)		WT.PCT.		MID PHI(LINEAR)		MID PHI(PROB.)		MODE	
MM	PHI	UNCOR	COR	CUR	CUMUL.	PHI	MM	PHI	MM	
0.250000	2.000	0.010	0.010	0.184	0.184	1.751	0.29707	1.881	0.27151	0
0.177000	2.498	0.010	0.010	0.184	0.368	2.249	0.21036	2.287	0.20485	0
0.125000	3.000	0.160	0.160	2.947	3.315	2.749	0.14875	2.851	0.13865	0
0.088000	3.500	0.710	0.710	15.076	16.390	3.253	0.10488	3.323	0.09996	0
0.062500	4.000	0.930	0.930	17.127	33.518	3.753	0.07416	3.777	0.07297	0
0.044000	4.506	0.985	0.985	18.134	51.652	4.253	0.05244	4.259	0.05224	1*
0.031000	5.012	0.378	0.378	6.966	58.618	4.759	0.03693	4.758	0.03697	0
0.022000	5.506	0.737	0.737	13.968	72.186	5.259	0.02612	5.250	0.02628	1
0.015000	6.002	0.405	0.405	7.462	79.648	5.754	0.01853	5.744	0.01866	0
0.011000	6.506	0.295	0.295	5.427	85.076	6.254	0.01310	6.242	0.01521	0
0.007800	7.002	0.221	0.221	4.070	89.145	6.754	0.00926	6.741	0.00935	0
0.005500	7.506	0.147	0.147	2.714	91.859	7.254	0.00655	7.241	0.00661	0
0.003900	8.002	0.110	0.110	2.035	93.894	7.754	0.00463	7.741	0.00468	0
0.002700	8.533	0.111	0.111	2.036	95.930	8.268	0.00325	8.246	0.00329	1
0.001900	9.040	0.037	0.037	0.678	96.608	8.786	0.00227	8.777	0.00228	0
0.000661	14.000	0.184	0.184	3.392	100.000	11.520	0.00034	9.810	0.00111	0
TOTALS		5.430	5.430	100.0						
0.250000	0.020000									
0.177000	0.020000									
0.125000	0.190000									
0.088000	0.810000									

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PI\*\* 115A 0 0.0 0 0.0 0

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 \*\* MULTIMODAL SAMPLE \*\*  
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WET WT	DRY WT	SALT	ORGANIC	MOISTURE	WEIGHT LOSS DUE TO HANDLING	0.0
1000.0000	4.2400	0.0	0.0	0.0 (GRAMS)	GRAVEL CORRECTION FACTOR	1.000
100.0000	100.0000	0.0	0.0	0.0 (PCT WET WT)	SIZES ELIMINATED (<0.01%)	NONE
					TRASK SORTING COEFFICIENT	1.777
					USING PROBABILITY EXTRAP.	1.769
					MEAN CUBED DEVIATION	11.550
					USING PROBABILITY EXTRAP.	6.598

PERCENTAGE COMPOSITION		TABLE OF STATISTICAL DATA IN PHI UNITS					PERCENTILES		LINEAR EXTRAP.		PROBABILITY EXTRAP.	
		MEAN	STD DEV	SKEWNESS	KURTOSIS			MM.	PHI UNITS	MM.	PHI UNITS	
GRAVEL	0.0	MOMENT	4.58070	1.72858	2.23617	9.26206	5.0	0.12919	2.95245	0.12735	2.97308	
SAND	47.64	P-MOMENT	4.55206	1.54303	1.79597	6.68905	10.0	0.11492	3.12126	0.11042	3.17887	
SILT	47.94	FOLK	4.37085	1.34299	0.44121	1.18163	16.0	0.10293	3.28029	0.09892	3.33764	
CLAY	4.41	P-FOLK	4.38490	1.32036	0.45855	1.18334	25.0	0.08739	3.51641	0.08729	3.51892	
MUD	52.26	INMAN	4.51655	1.23626	0.35357	0.93489	50.0	0.05915	4.07945	0.05920	4.07834	
S/M	0.91	P-INMAN	4.53819	1.20055	0.38303	0.97932	75.0	0.02767	5.17572	0.02789	5.18400	
		KRUMBEIN		1.22912	0.26661	0.25528	84.0	0.01854	5.75282	0.01873	5.73874	
		P-KRUM.		1.21924	0.26267	0.25903	90.0	0.01208	6.37125	0.01221	6.35602	
		FOLK (TRANSFORMED)				0.54163	95.0	0.00469	7.73652	0.00472	7.72562	
		P-FOLK (TRANSFORMED)				0.54199						

DATA FOR CONSTN OF BARGRAPHS AND CUM. CURVES

SIZE FRACTION	WT.(GMS)	WT.PCT.	WT.PCT.	MID PHI(LINEAR)	MID PHI(PROB.)	MODE
MM	PHI	UNCOR	COR	COR	CUMUL. PHI	MM
0.250000	2.000	0.020	0.020	0.472	0.472	1.751
0.177000	2.498	0.020	0.020	0.472	0.943	2.249
0.125000	3.000	0.190	0.190	4.481	5.425	2.749
0.080000	3.500	0.810	0.810	19.104	24.528	3.253
0.062500	4.000	0.980	0.980	23.113	47.642	3.753
0.040000	4.500	0.637	0.637	15.027	62.669	4.253
0.031000	5.012	0.391	0.391	9.223	71.892	4.759
0.022000	5.500	0.397	0.397	9.369	81.261	5.259
0.015600	6.002	0.234	0.234	5.912	86.772	5.754
0.011000	6.506	0.187	0.187	4.409	91.182	6.254
0.007800	7.002	0.070	0.070	1.653	92.835	6.754
0.005500	7.506	0.070	0.070	1.653	94.488	7.254
0.003900	8.002	0.047	0.047	1.103	95.591	7.754
0.002700	8.533	0.023	0.023	0.551	96.142	8.260
0.001900	9.040	0.023	0.023	0.552	96.693	8.786
0.001380	9.501	0.023	0.023	0.551	97.244	9.270
0.000061	14.000	0.117	0.117	2.756	100.000	11.751
TOTALS		4.240	4.240	100.0		
0.250000	0.050000					
0.177000	0.020000					
0.125000	0.190000					

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P1++ 1158 0 0.0 0 0.0 0

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 \*\*\* MULTIMODAL SAMPLE \*\*\*  
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WET WT	DRY WT	SALT	ORGANIC	MOISTURE	WEIGHT LOSS DUE TO HANDLING	0.0
100.0000	6.2900	0.0	0.0	0.0 (GRAMS)	GRAVEL CORRECTION FACTOR	1.000
100.0000	100.0000	0.0	0.0	0.0 (PCT WET WT)	SIZES ELIMINATED (<0.01%)	NONE
					TRASK SORTING COEFFICIENT	1.920
					USING PROBABILITY EXTRAP.	1.913
					MEAN CUBED DEVIATION	10.794
					USING PROBABILITY EXTRAP.	5.238

PERCENTAGE COMPOSITION		TABLE OF STATISTICAL DATA IN PHI UNITS				PERCENTILES		LINEAR EXTRAP.		PROBABILITY EXTRAP.	
		MEAN	STD DEV	SKEWNESS	KURTOSIS		MM.	PHI UNITS	MM.	PHI UNITS	
GRAVEL	0.0	5.21379	1.86293	1.66949	6.79074	5.0	0.12088	3.04840	0.11874	3.07415	
SAND	26.23	5.16084	1.64495	1.17674	4.74734	10.0	0.09959	3.32778	0.09661	3.37172	
SILT	67.48	5.02099	1.59659	0.19652	1.25864	16.0	0.08176	3.61253	0.08064	3.63230	
CLAY	6.29	5.02698	1.58596	0.20184	1.26323	29.0	0.06455	3.93333	0.06423	3.92669	
MUD	73.77	5.04721	1.43468	0.05481	1.02242	50.0	0.03194	4.96857	0.03192	4.96945	
S/M	0.36	5.05575	1.42345	0.06063	1.02675	75.0	0.01742	5.84290	0.01755	5.83266	
			1.39968	-0.07046	0.24649	84.0	0.01119	6.48188	0.01121	6.47920	
			1.38665	-0.07277	0.24788	90.0	0.00699	7.16068	0.00705	7.14774	
					0.55726	95.0	0.00216	8.85144	0.00218	8.84409	
					0.55815						

DATA FOR CONSTN OF BARGRAPHS AND CUM. CURVES

SIZE FRACTION	WT.(GMS)	WT.PCT.	WT.PCT.	MID PHI(LINEAR)	MID PHI(PROB.)	MODE
MM	PHI	UNCOR	COR	PHI	MM	PHI
0.25000	2.000	0.050	0.050	0.795	0.795	1.751
0.17700	2.458	0.020	0.020	0.318	1.112	2.249
0.12500	3.000	0.190	0.190	3.021	4.154	2.749
0.08800	3.506	0.570	0.570	9.062	13.196	3.253
0.06250	4.000	0.820	0.820	13.037	26.232	3.753
0.04400	4.506	0.586	0.586	9.309	35.541	4.253
0.03100	5.012	0.494	0.494	15.804	51.345	4.759
0.02200	5.506	1.086	1.086	17.265	68.610	5.259
0.01560	6.002	0.592	0.592	9.417	78.026	5.754
0.01100	6.506	0.395	0.395	6.278	84.304	6.254
0.00780	7.002	0.296	0.296	4.709	89.014	6.754
0.00550	7.506	0.197	0.197	3.159	92.153	7.254
0.00390	8.002	0.099	0.099	1.569	93.722	7.754
0.00270	8.533	0.049	0.049	0.785	94.506	8.268
0.00190	9.046	0.049	0.049	0.785	95.292	8.786
0.00130	9.501	0.049	0.049	0.785	96.076	9.270
0.00061	14.000	0.247	0.247	3.924	100.000	11.751
TOTALS		6.290	6.290	100.0		

P1++ 116A 0 0.0 0 0.0 0

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 \*\*\* MULTIMODAL SAMPLE \*\*\*  
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WET WT	DRY WT	SALT	ORGANIC	MOISTURE	WEIGHT LOSS DUE TO HANDLING	0.0
1000.0000	5.9300	0.0	0.0	0.0 (GRAMS)	GRAVEL CORRECTION FACTOR	1.000
99.9999	100.0000	0.0	0.0	0.0 (PCT WET WT)	SIZES ELIMINATED (<0.01%)	NONE
					TRASK SORTING COEFFICIENT	1.848
					USING PROBABILITY EXTRAP.	1.835
					MEAN CUBED DEVIATION	10.817
					USING PROBABILITY EXTRAP.	5.243

PERCENTAGE COMPOSITION	TABLE OF STATISTICAL DATA IN PHI UNITS				PERCENTILES		LINEAR EXTRAP.		PROBABILITY EXTRAP.	
	MEAN	STD DEV	SKEWNESS	KURTOSIS	MM.	PHI UNITS	MM.	PHI UNITS		
GRAVEL 0.0	MOMENT 5.15673	1.80248	1.84723	7.73735	5.0	0.11391	3.13405	0.10968	3.18857	
SAND 25.63	P-MOMENT 5.10501	1.57916	1.33131	5.52828	10.0	0.08992	3.47526	0.08928	3.48548	
SILT 68.23	FOLK 4.95639	1.49148	0.18272	1.30527	16.0	0.07766	3.68668	0.07583	3.72107	
CLAY 6.14	P-FOLK 4.96211	1.46894	0.19179	1.30543	25.0	0.06340	3.97941	0.06321	3.98375	
MUD 74.37	INMAN 4.96015	1.27347	0.00884	1.21497	50.0	0.03238	4.94888	0.03236	4.94971	
S/M 0.34	P-INMAN 4.96830	1.24723	0.01491	1.23660	75.0	0.01857	5.75073	0.01877	5.73530	
	KRUMHFIN 1.31208	-0.08381		0.27039	84.0	0.01329	6.23361	0.01346	6.21554	
	P-KRUM. 1.29744	-0.09019		0.26996	90.0	0.00929	6.75071	0.00942	6.72560	
	FOLK (TRANSFORMED) 0.56621			0.56624	95.0	0.00228	8.77542	0.00229	8.76768	
	P-FOLK (TRANSFORMED) 0.56624									

DATA FOR CONSTN OF HARGRAPHS AND CUM. CURVES

SIZE FRACTION	WT.(GMS)	WT.PCT.	WT.PCT.	MID PHI(LINEAR)	MID PHI(PRC.)	MODE				
MM	PHI	UNCOR	CCR	COR	CUMUL.	PHI	MM	PHI	MM	
0.250000	2.000	0.070	0.070	1.180	1.180	1.751	0.29707	1.914	0.26536	1
0.177000	2.498	0.030	0.030	0.506	1.686	2.249	0.21036	2.268	0.20760	0
0.125000	3.000	0.080	0.080	1.349	3.035	2.749	0.14875	2.780	0.14362	0
0.098000	3.506	0.440	0.440	7.420	10.455	3.253	0.10488	3.311	0.10076	0
0.0862500	4.000	0.900	0.900	15.177	25.632	3.753	0.07416	3.787	0.07442	0
0.0744000	4.506	0.734	0.734	12.373	38.005	4.253	0.05244	4.264	0.05206	0
0.031000	5.012	0.812	0.812	13.694	51.699	4.759	0.03693	4.762	0.03686	0
0.022000	5.506	1.048	1.048	17.634	69.333	5.259	0.02612	5.251	0.02626	1*
0.015600	6.002	0.682	0.682	11.500	80.833	5.754	0.01853	5.739	0.01873	0
0.011000	6.506	0.409	0.409	6.901	87.734	6.254	0.01310	6.236	0.01327	0
0.007800	7.002	0.273	0.273	4.599	92.333	6.754	0.00926	6.733	0.00940	0
0.005500	7.506	0.048	0.048	0.787	93.100	7.254	0.00655	7.249	0.00657	0
0.003900	8.002	0.045	0.045	0.766	93.867	7.754	0.00463	7.749	0.00465	0
0.002700	8.533	0.045	0.045	0.766	94.633	8.268	0.00325	8.261	0.00326	0
0.001900	9.040	0.045	0.045	0.766	95.400	8.786	0.00227	8.778	0.00228	0
0.001380	9.501	0.045	0.045	0.767	96.127	9.270	0.00162	9.262	0.00163	0
0.000061	14.000	0.227	0.227	3.833	100.000	11.751	0.00029	10.193	0.00085	0
TOTALS		5.930	5.930	100.0						

P1++ 116B 0 0.0 0 0.0 0

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 \*\*\*\* MULTIMODAL SAMPLE \*\*\*\*  
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WET WT	DPY WT	SALT	ORGANIC	MOISTURE	WEIGHT LOSS DUE TO HANDLING	0.0
1000.0000	4.8900	0.0	0.0	0.0 (GRAMS)	GRAVEL CORRECTION FACTOR	1.000
99.9999	100.0000	0.0	0.0	0.0 (PCT WET WT)	SIZES ELIMINATED (<0.01%)	NONE
					TRASK SORTING COEFFICIENT	1.957
					USING PROBABILITY EXTRAP.	1.945
					MEAN CUBED DEVIATION	13.643
					USING PROBABILITY EXTRAP.	9.070

PERCENTAGE COMPOSITION TABLE OF STATISTICAL DATA IN PHI UNITS PERCENTILES LINEAR EXTRAP. PROBABILITY EXTRAP.

PERCENTAGE COMPOSITION		MOMENT	MEAN	STD DEV	SKEWNESS	KURTOSIS	PERCENTILES		LINEAR EXTRAP.		PROBABILITY EXTRAP.	
							MM.	PHI UNITS	MM.	PHI UNITS		
GRAVEL	0.0		5.84548	2.13343	1.40491	5.23066	5.0	0.09685	3.36806	0.09532	3.39106	
SAND	11.86	P-MOMENT	5.85612	1.98350	1.16222	4.31919	10.0	0.06934	3.85024	0.06811	3.87592	
SILT	74.77	FOLK	5.70610	1.93011	0.37507	1.54871	16.0	0.05334	4.22859	0.05248	4.25214	
CLAY	13.37	P-FOLK	5.71438	1.91940	0.38101	1.55866	25.0	0.04028	4.63364	0.03989	4.64765	
MUD	88.14	INMAN	5.86983	1.64124	0.25928	1.23982	50.0	0.02404	5.37665	0.02401	5.38021	
S/M	0.13	P-INMAN	5.88146	1.62933	0.30764	1.23750	75.0	0.01051	6.57143	0.01054	6.56733	
		KRUMHEIN	1.43540	0.22389	0.19866		84.0	0.00548	7.51107	0.00548	7.51079	
		P-KRUM.	1.42195	0.22730	0.19817		90.0	0.00236	8.72731	0.00237	8.71941	
		FOLK (TRANSFORMED)			0.60764		95.0	0.00061	10.65068	0.00061	10.68230	
		P-FOLK (TRANSFORMED)			0.60886							

DATA FOR CONSTN OF BARGRAPHS AND CUM. CURVES

SIZE FRACTION	WT.(GMS)		WT.PCT.		MID PHI(LINEAR)		MID PHI(PROB.)		MODE	
	MM	PHI	UNCOR	COR	PHI	CUMUL.	PHI	MM		
0.250000	2.000	0.040	0.040	0.818	0.818	1.751	0.29707	1.910	0.26618	1
0.177000	2.496	0.040	0.040	0.818	1.636	2.249	0.21036	2.286	0.20507	0
0.125000	3.000	0.070	0.070	1.431	3.067	2.749	0.14875	2.782	0.14541	0
0.098000	3.506	0.130	0.130	2.658	5.726	3.253	0.10488	3.285	0.11262	0
0.062500	4.000	0.300	0.300	6.135	11.861	3.753	0.07416	3.786	0.07248	0
0.044000	4.506	0.448	0.448	9.168	21.029	4.253	0.05244	4.276	0.05160	0
0.031000	5.012	0.771	0.771	15.761	36.789	4.759	0.03693	4.776	0.03551	0
0.022000	5.506	0.871	0.871	17.306	54.595	5.259	0.02612	5.262	0.02506	1
0.015000	6.002	0.522	0.522	10.683	65.278	5.754	0.01853	5.750	0.01858	0
0.011000	6.506	0.435	0.435	8.904	74.182	6.254	0.01310	6.246	0.01313	0
0.007800	7.002	0.305	0.305	6.251	80.413	6.754	0.00926	6.745	0.00933	0
0.005500	7.506	0.174	0.174	3.561	83.974	7.254	0.00655	7.246	0.00659	0
0.003900	8.002	0.131	0.131	2.671	86.645	7.754	0.00463	7.747	0.00466	0
0.002700	8.523	0.131	0.131	2.672	89.317	8.268	0.00325	8.257	0.00327	1
0.001900	9.040	0.087	0.087	1.780	91.097	8.786	0.00227	8.778	0.00228	0
0.001360	9.501	0.087	0.087	1.780	92.877	9.270	0.00162	9.261	0.00163	1
0.000980	9.995	0.044	0.044	0.891	93.768	9.748	0.00116	9.742	0.00117	0
0.000690	10.501	0.044	0.044	0.891	94.658	10.248	0.00082	10.240	0.00083	1
0.000490	10.995	0.044	0.044	0.890	95.548	10.748	0.00058	10.739	0.00059	0
0.000061	14.000	0.218	0.218	4.452	100.000	12.497	0.00017	11.453	0.00016	0
TOTALS		4.890	4.890	100.0						

333

Pl++ 118 0 0.0 0 0.0 0

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 \*\*\* MULTIMOAL SAMPLE \*\*\*  
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WET WT DRY WT SALT ORGANIC MOISTURE  
 1000.0000 4.8300 0.0 0.0 0.0 (GRAMS)  
 100.0000 100.0000 0.0 0.0 0.0 (PCT WET WT)

WEIGHT LOSS DUE TO HANDLING 0.0  
 GRAVEL CORRECTION FACTOR 1.000  
 SIZES ELIMINATED (<0.015) NONE  
 TRASK SORTING COEFFICIENT 1.443  
 USING PROBABILITY EXTRAP. 1.428  
 MEAN CUBED DEVIATION 7.686  
 USING PROBABILITY EXTRAP. 5.293

PERCENTAGE TABLE OF STATISTICAL DATA IN PHI UNITS PERCENTILES LINEAR EXTRAP. PROBABILITY EXTRAP.

GRAVEL	0.0	MOMENT	STATISTICAL DATA				PERCENTILES		LINEAR EXTRAP.		PROBABILITY EXTRAP.	
			MEAN	STD DEV	SKWNESS	KURTOSIS	MM.	PHI UNITS	MM.	PHI UNITS		
SAND	75.57	P-MOMENT	3.82359	1.48994	2.32373	10.20919	5.0	0.17297	2.53142	0.16799	2.57357	
SILT	22.06	FCLK.	3.76923	1.25574	0.54434	1.65215	10.0	0.16155	2.62995	0.15216	2.71635	
CLAY	2.57	P-FOLK	3.79157	1.22255	0.57257	1.68106	16.0	0.14884	2.74618	0.14071	2.82919	
MUD	24.43	INMAN	3.96596	1.21778	0.48439	0.75285	25.0	0.13162	2.92553	0.12896	2.95454	
S/M	3.09	P-INMAN	3.99714	1.16796	0.52803	0.80426	50.0	0.09632	3.37608	0.09603	3.38043	
		KRUMBEIN		0.78446	0.07696	0.17496	75.0	0.06317	3.98456	0.06326	3.98244	
		P-KPUM.		0.76111	0.08826	0.17556	84.0	0.02751	5.18375	0.02787	5.16510	
		FOLK (TRANSFORMED)				0.62295	90.0	0.01983	5.65636	0.02002	5.64271	
		P-FOLK (TRANSFORMED)				0.62701	95.0	0.00897	6.80060	0.00905	6.76817	

DATA FOR CONSTN OF BARGRAPHS AND CUM. CURVES

SIZE FRACTION	WT.(GMS)	WT.PCT.	WT.PCT.	MID PHI(LINEAR)	MID PHI(PROB.)	MODE
MM	PHI	UNCOR	COR	CUMUL.	PHI	MM
0.250000	2.000	0.080	0.080	1.656	1.656	1.751
0.177000	2.498	0.080	0.080	1.656	3.313	2.249
0.125000	3.000	1.230	1.230	25.466	28.778	2.749
0.088000	3.506	1.380	1.380	28.571	57.350	3.253
0.062500	4.000	0.880	0.880	18.219	75.569	3.753
0.044000	4.506	0.210	0.210	4.348	79.917	4.253
0.031000	5.012	0.069	0.069	1.432	81.349	4.759
0.022000	5.506	0.368	0.368	7.618	88.967	5.259
0.015600	6.002	0.165	0.165	3.415	92.382	5.754
0.011000	6.506	0.089	0.089	1.839	94.221	6.254
0.007800	7.002	0.063	0.063	1.314	95.534	6.754
0.005500	7.506	0.051	0.051	1.051	96.585	7.254
0.003900	8.002	0.051	0.051	1.051	97.636	7.754
0.002700	8.533	0.038	0.038	0.788	98.423	8.268
0.001900	9.040	0.025	0.025	0.526	98.949	8.786
0.000661	14.000	0.051	0.051	1.051	100.000	11.520
TOTALS		4.830	4.830	100.0		

35334

PITT119

SIEVE, SH. PIP., SEDIGRAPH SAMPLE WT.= 4.8800

PHI PCT. CUMFCT.

3.50	2.05	**
4.00	2.05	**
4.50	4.05	**
	9.99	*****
5.00	14.05	*****
	17.99	*****
5.50	22.04	*****
	17.99	*****
6.00	50.03	*****
	14.99	*****
6.50	65.02	*****
	9.00	*****
7.00	74.01	*****
	6.00	*****
7.50	80.01	*****
	6.00	*****
8.00	86.01	*****
	4.00	*****
8.50	90.01	**
	2.00	**
9.00	92.00	**
	2.00	**
9.50	94.00	*
	1.00	*
10.00	95.00	*****
	5.00	*****
12.00	100.00	

MEAN ST.DEV. SKEWNESS KURTOSIS

6.15	1.24	0.35	0.21	KRUMBEIN+PETTICORN (1938) MOMENT MEASURES FOR SIZE RANGE 4.0 TO 10.0 PHI
6.30	1.52	0.39	1.29	FOLK GRAPHIC STATISTICAL PARAMETERS FOLK AND WARD, 1957

PERCENTILES	MEDIAN	6.00	5TH	4.55	16TH	5.05	25TH	5.30
			75TH	7.08	84TH	7.83	95TH	10.00

PER CENT GRAVEL 0.0 SAND 2.05 SILT 84.10 ( 83.96) CLAY 13.85 ( 13.99)

GRAVEL + SAND 2.05 SILT/(SILT+CLAY) 85.71PCT GRAV+SAND/SILT+CLAY 0.02

LABELS SHEPARD -SILT FOLK(GMS)-MUD (SCS)-SILT

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PITT120

SIEVF, SH. PIP., SEDIGRAPH SAMPLE WT.= 4.7100

PHI PCT. CUMPCT.

3.50	0.21		
4.00	2.99	0.21	***
4.50	7.98	3.21	*****
5.00	19.96	11.19	*****
5.50	14.97	30.15	*****
6.00	12.97	45.12	*****
6.50	6.99	58.09	*****
7.00	4.99	65.07	*****
7.50	3.99	70.06	***
8.00	2.99	74.06	***
8.50	2.99	77.05	***
9.00	3.99	80.04	****
9.50	2.99	84.03	***
10.00	2.99	87.03	***
10.50	2.00	90.02	**
11.00	3.99	92.02	****
11.50	3.99	96.01	****
12.00		100.00	

MEAN ST.DEV. SKEWNESS KURTOSIS

6.73 1.88 0.49 -0.09 KRUMREIN+PETTIJOHN(1938) MOMENT MEASURES  
FOR SIZE RANGE 4.0 TO 11.5 PHI

6.94 2.12 0.52 1.24 FOLK GRAPHIC STATISTICAL PARAMETERS  
FOLK AND WARD,1957

PERCENTILES MEDIAN 6.19 5TH 4.61 16TH 5.13 25TH 5.36  
75TH 8.16 84TH 9.50 95TH 11.37

PER CENT GRAVEL 0.0 SAND 0.21 SILT 74.31 ( 73.84) CLAY 25.48 ( 25.94)

GRAVEL + SAND 0.21 SILT/(SILT+CLAY) 74.00PCT GRAV+SAND/SILT+CLAY 0.00

LABELS SHEPARD -CLAYEY SILT FOLK(GMS)-MUD

(SCS)-SILT

336

P1++ 122A 0 0.0 0 0.0 0

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 \*\*\*\* MULTIMODAL SAMPLE \*\*\*\*  
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WET WT	DPY WT	SALT	ORGANIC	MOISTURE	WEIGHT LOSS DUE TO HANDLING	0.0
1000.0000	3.5400	0.0	0.0	0.0 (GRAMS)	GRAVEL CORRECTION FACTOR	1.000
100.0000	100.0000	0.0	0.0	0.0 (PCT WET WT)	SIZES ELIMINATED (<0.01%)	NONE
					TRASK SORTING COEFFICIENT	1.962
					USING PROBABILITY EXTRAP.	1.957
					MEAN CUBED DEVIATION	8.923
					USING PROBABILITY EXTRAP.	3.927

PERCENTAGE COMPOSITION TABLE OF STATISTICAL DATA IN PHI UNITS PERCENTILES LINEAR EXTRAP. PROBABILITY EXTRAP.

PERCENTAGE COMPOSITION		TABLE OF STATISTICAL DATA IN PHI UNITS				PERCENTILES LINEAR EXTRAP.		PROBABILITY EXTRAP.	
		MEAN	STD DEV	SKEWNESS	KURTOSIS	MM.	PHI UNITS	MM.	PHI UNITS
GRAVEL	0.0	4.79367	1.74082	1.69138	6.77620	5.0	0.13068	2.93586	0.12778
SAND	41.53	P-MOMENT 4.74921	1.51900	1.12054	4.06657	10.0	0.11503	3.11995	0.11074
SILT	54.11	FOLK 4.64034	1.45677	0.26156	1.03185	16.0	0.10256	3.28541	0.09875
CLAY	4.36	P-FOLK 4.65495	1.43295	0.27466	1.02509	25.0	0.08632	3.53420	0.08510
MUD	58.47	INMAN 4.71567	1.43025	0.15800	0.71117	50.0	0.04451	4.48968	0.04451
S/M	0.71	P-INMAN 4.73752	1.39740	0.17727	0.73395	75.0	0.02243	5.47835	0.02248
		KRUMBEIN 1.44011	0.01660	0.25746		84.0	0.01412	6.14592	0.01423
		P-KRUM. 1.43517	0.01684	0.26100		90.0	0.00840	6.89556	0.00845
		FOLK (TRANSFORMED)		0.50784		95.0	0.00439	7.83069	0.00444
		P-FOLK (TRANSFORMED)		0.50619					7.81431

DATA FOR CONSTN OF BARGRAPHS AND CUM. CURVES

SIZE FRACTION	WT.(GMS)	WT.PCT.	WT.PCT.	MID PHI(LINEAR)	MID PHI(PROB.)	MODE
MM	PHI	UNCOR	COR	PHI	MM	MM
0.250000	2.000	0.010	0.010	0.282	0.282	1.751
0.177000	2.498	0.010	0.010	0.282	0.565	2.249
0.125000	3.000	0.180	0.180	5.085	5.650	2.749
0.088000	3.506	0.650	0.650	18.362	24.011	3.253
0.062500	4.009	0.620	0.620	17.514	41.525	3.753
0.044000	4.506	0.310	0.310	8.763	50.288	4.253
0.031000	5.012	0.438	0.438	12.387	62.675	4.759
0.022000	5.506	0.462	0.462	13.064	75.739	5.259
0.015600	6.002	0.242	0.242	6.843	82.582	5.754
0.011000	6.506	0.176	0.176	4.976	87.558	6.254
0.007800	7.002	0.110	0.110	3.112	90.670	6.754
0.005500	7.506	0.110	0.110	3.110	95.780	7.254
0.003900	8.002	0.066	0.066	1.866	95.646	7.754
0.002700	8.533	0.044	0.044	1.244	96.890	8.268
0.000001	14.000	0.110	0.110	3.110	100.000	11.266
TOTALS		3.540	3.540	100.0		
0.250000	0.070000					
0.177000	0.030000					
0.125000	0.150000					
0.088000	0.810000					
0.062500	1.230000					

337

PITT1228

SIEVE, SH. PIP., SEDIGRAPH SAMPLE WT.= 4.8500

PHI PCT. CUMFCT.

2.00			*
2.50	0.82	0.82	*
	1.44		*
3.00		2.27	
	3.09		***
3.50		5.36	
	5.98		*****
4.00		11.34	
	8.14		*****
4.50		19.48	
	14.48		*****
5.00		33.96	
	9.95		*****
5.50		43.91	
	21.71		*****
6.00		65.62	
	9.05		*****
6.50		74.07	
	5.43		*****
7.00		80.10	
	6.33		*****
7.50		86.43	
	3.62		****
8.00		90.05	
	1.81		**
8.50		91.86	
	2.71		***
9.00		94.57	
	0.90		*
9.50		95.48	
	4.52		*****
12.00		100.00	

MEAN ST.DEV. SKEWNESS KURTOSIS

5.58	1.38	0.15	0.04	KRUMBEIN+PETTICORN(1938) MOMENT MEASURES FOR SIZE RANGE 2.5 TO 9.5 PHI
5.74	1.63	0.17	1.35	FOLK GRAPHIC STATISTICAL PARAMETERS FOLK AND WARD,1957

PERCENTILES	MEDIAN	5.64	5TH	3.44	16TH	4.29	25TH	4.69
			75TH	6.53	84TH	7.31	95TH	9.24

PER CENT GRAVEL 0.0 SAND 11.34 SILT 78.87 ( 78.71) CLAY 9.79 ( 9.95)

GRAVEL + SAND 11.34 SILT/(SILT+CLAY) 88.78PCT GRAV+SAND/SILT+CLAY 0.13

LABELS SHEPARD -SILT FOLK(GMS)-SANDY MUD (SCS)-SANDY SILT

REPRODUCED FROM ORIGINAL RECORDS

338

PIT121

SIEVE, SH. PIP., SEDIGRAPH SAMPLE WT.= 3.4600

PHI PCT. CUMPT.

3.50	3.76	****
4.00	3.76	****
	6.80	*****
4.50	10.57	*****
	20.41	*****
5.00	30.98	*****
	19.44	*****
5.50	50.42	*****
	13.61	*****
6.00	64.03	*****
	7.78	*****
6.50	71.81	*****
	5.83	*****
7.00	77.64	*****
	5.83	*****
7.50	83.47	****
	3.89	****
8.00	87.36	**
	1.94	**
8.50	89.31	**
	1.94	**
9.00	91.25	**
	1.94	**
9.50	93.20	**
	1.94	**
10.00	95.14	*****
	4.86	*****
12.00	100.00	

MEAN ST.DEV. SKEWNESS KURTOSIS

5.79 1.36 0.52 0.65 Krumbein+Peterson (1938) Moment Measures  
for size range 4.0 to 10.0 phi

5.90 1.62 0.47 1.35 Folk Graphic Statistical Parameters  
Folk and Ward, 1957

PERCENTILES MEDIAN 5.49 5TH 4.09 16TH 4.63 25TH 4.85  
75TH 6.77 84TH 7.57 95TH 9.96

PER CENT GRAVEL 0.0 SAND 3.76 SILT 83.94 (83.60) CLAY 12.30 (12.64)

GRAVEL + SAND 3.76 SILT/(SILT+CLAY) 86.87PCT GRAV+SAND/SILT+CLAY 0.04

LABELS SHEPARD -SILT FOLK(GMS)-MUD (SCS)-SILT

339

PITT123A

SIEVE, SH. PIP., SEDIGRAPH SAMPLE WT.= 4.9000

PHI PCT. CUMPCT.

3.50	0.41		
4.00	1.00	0.41	*
4.50	1.99	1.40	**
5.00	3.40		
5.50	5.39		
6.00	10.37		*****
6.50	15.35		
7.00	22.32		*****
7.50	33.27		*****
8.00	45.22		*****
8.50	55.18		*****
9.00	66.14		*****
9.50	75.10		*****
10.00	81.08		*****
10.50	86.06		****
11.00	90.04		****
11.50	94.02		**
12.00	96.02		****
12.00	100.00		

MEAN ST.DEV. SKEWNESS KURTOSIS

6.18	1.70	-0.01	-0.38	KRUMBEIN+PETTIJOHN(1938) MOMENT MEASURES FOR SIZE RANGE 4.0 TO 12.0 PHI
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8.36	1.90	0.10	1.32	FOLK GRAPHIC STATISTICAL PARAMETERS FOLK AND WARD, 1957
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PERCENTILES	MEDIAN	8.24	5TH	5.40	16TH	6.55	25TH	7.12
			75TH	9.49	84TH	10.29	95TH	11.74

PER CENT GRAVEL	0.0	SAND	0.41	SILT	44.94 ( 44.82)	CLAY	54.65 ( 54.78)
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GRAVEL + SAND	0.41	SILT/(SILT+CLAY)	45.00PCT	GRAV+SAND/SILT+CLAY	0.00
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PITT1238

SIEVE, SH. PIP., SEDIGRAPH SAMPLE WT.= 4.2600

PHI PCT. CUMPT.

3.50	0.71	*
4.00	0.71	*
4.50	1.70	***
5.00	4.68	*****
5.50	9.64	*****
6.00	15.00	*****
6.50	25.53	*****
7.00	33.47	*****
7.50	47.37	*****
8.00	58.30	*****
8.50	68.23	*****
9.00	76.17	*****
9.50	83.12	*****
10.00	89.08	***
10.50	92.06	***
11.00	95.04	*****
12.00	100.00	

MEAN ST.DEV. SKEWNESS KURTOSIS

7.56	1.56	0.00	-0.56	KRUMBEIN+PETTITJOHN(1938) MOMENT MEASURES FOR SIZE RANGE 4.0 TO 11.0 PHI
7.74	1.79	0.12	1.22	FOLK GRAPHIC STATISTICAL PARAMETERS FOLK AND WARD,1957

PERCENTILES	MEDIAN	7.62	5TH	5.03	16TH	6.02	25TH	6.47
			75TH	8.93	84TH	9.57	95TH	10.99

PER CENT GRAVEL 0.0 SAND 0.70 SILT 57.58 ( 57.59) CLAY 41.72 ( 41.70)

GRAVEL + SAND 0.70 SILT/((SILT+CLAY) 58.00PCT GRAV+SAND/SILT+CLAY 0.01

LABELS SHEPARD -CLAYEY SILT FOLKIGMSI-MUD (SCS)-MUD

341

PITT1258

SIEVE, SH. PIP., SEDIGRAPH SAMPLE WT.= 5.2300

PHI PCT. CUMPT.

2.00	0.58	*
2.50	1.15	*
3.00	1.73	**
3.50	2.30	**
4.00	2.90	****
4.50	3.50	****
5.00	4.10	*****
5.50	4.70	*****
6.00	5.30	*****
6.50	5.90	*****
7.00	6.50	*****
7.50	7.10	*****
8.00	7.70	*****
8.50	8.30	*****
9.00	8.90	*****
9.50	9.50	*****
10.00	10.10	*****
10.50	10.70	*****
11.00	11.30	*****
11.50	11.90	*****
12.00	12.50	*****

MEAN ST.DEV. SKEWNESS KURTOSIS

6.09 1.71 0.26 -0.16 KRUMBEIN+PETTIIJOHN(1938) MOMENT MEASURES FOR SIZE RANGE 2.5 TO 10.5 PHI

6.33 2.00 0.34 1.39 FOLK GRAPHIC STATISTICAL PARAMETERS FOLK AND WARD,1957

PERCENTILES MEDIAN 5.87 5TH 3.61 16TH 4.62 25TH 4.99  
75TH 7.44 84TH 8.48 95TH 10.41

PER CENT GRAVEL 0.0 SAND 8.44 SILT 72.39 ( 71.94) CLAY 19.18 ( 19.62)

GRAVEL + SAND 8.44 SILT/(SILT+CLAY) 78.57PCT GRAV+SAND/SILT+CLAY 0.09

PITT125C

SIEVE, SH. PIP., SEDIGRAPH SAMPLE WT.= 4.8300

PHI PCT. CUMPCT.

3.00	2.07	**
3.50	4.15	****
4.00	6.22	*****
4.50	11.00	*****
5.00	16.27	*****
5.50	23.44	*****
6.00	39.71	*****
6.50	52.15	*****
7.00	63.84	*****
7.50	71.29	*****
8.00	76.08	*****
8.50	82.77	****
9.00	86.60	***
9.50	89.47	**
10.00	92.34	**
10.50	94.26	**
11.00	96.17	**
11.50	98.08	**
12.00	100.00	****

MEAN ST.DEV. SKEWNESS KURTOSIS

6.14	1.60	0.32	-0.11	KRUMBEIN+PETTICHOHN(1938) MOMENT MEASURES FOR SIZE RANGE 3.5 TO 10.5 PHI
6.26	1.85	0.32	1.33	FOLK GRAPHIC STATISTICAL PARAMETERS FOLK AND WARD,1957

PERCENTILES	MEDIAN	5.91	5TH	3.85	16TH	4.70	25TH	5.05
			75TH	7.39	84TH	8.16	95TH	10.19

PER CENT GRAVEL 0.0 SAND 6.22 SILT 76.68 ( 76.56) CLAY 17.10 ( 17.23)

GRAVEL + SAND 6.22 SILT/(SILT+CLAY) 81.63PCT GRAV+SAND/SILT+CLAY 0.07

LABELS SHEPARD -SILT FOLK(GMS)-MUD (SCS)-SILT

343



PITT127A

SIEVE, SH. PIP., SEDIGRAPH SAMPLE WT.= 5.3000

PHI PCT. CUMPT.

2.00				
2.50	0.76		*	
	1.32	0.76	*	
3.00		2.08		
	2.64		***	
3.50		4.72		
	5.10		*****	
4.00		9.82		
	8.45		*****	
4.50		18.27		
	17.85		*****	
5.00		36.12		
	16.91		*****	
5.50		53.03		
	11.27		*****	
6.00		64.30		
	6.58		*****	
6.50		70.88		
	6.58		*****	
7.00		77.46		
	5.64		*****	
7.50		83.09		
	4.70		*****	
8.00		87.79		
	2.82		***	
8.50		90.61		
	3.76		***	
9.00		94.36		
	0.94		*	
9.50		95.30		
	4.70		*****	
12.00		100.00		

MEAN ST.DEV. SKEWNESS KURTOSIS

5.61 1.45 0.23 -0.18 KRUMBEIN+PETTICORN(1936) MOMENT MEASURES  
FOR SIZE RANGE 2.5 TO 9.5 PHI

5.79 1.69 0.35 1.27 FOLK GRAPHIC STATISTICAL PARAMETERS  
FOLK AND WARD,1957

PERCENTILES MEDIAN 5.41 5TH 3.53 16TH 4.37 25TH 4.69  
75TH 6.81 84TH 7.60 95TH 9.34

PER CENT GRAVEL 0.0 SAND 9.82 SILT 78.38 ( 77.57) CLAY 11.80 ( 12.21)

GRAVEL + SAND 9.82 SILT/(SILT+CLAY) 86.46PCT GRAV+SAND/SILT+CLAY 0.11

LABELS SHEPARD -SILT FOLKIGMS)-MUD (SCS)-SILT

344

PITT1278

SIEVE, SH. PIP., SEDICRAPH SAMPLE WT.= 4.1100

PHI PCT. CUMPT.

2.00	0.73		*
2.50	1.95	0.73	**
3.00	2.92	2.68	***
3.50	5.60	5.60	*****
4.00	8.33	11.19	*****
4.50	17.58	19.52	*****
5.00	18.50	37.09	*****
5.50	11.10	55.60	*****
6.00	10.18	66.70	*****
6.50	4.63	76.67	*****
7.00	5.55	81.50	*****
7.50	3.70	87.05	****
8.00	3.70	90.75	****
8.50	2.78	94.45	***
9.00	2.78	97.22	***
12.00		100.00	

MEAN ST.DEV. SKEWNESS KURTOSIS

5.51 1.36 0.19 -0.05 KRUMBEIN+PETTIJOHN(1938) MOMENT MEASURES  
FOR SIZE RANGE 2.5 TO 9.0 PHI

5.62 1.52 0.26 1.24 FOLK GRAPHIC STATISTICAL PARAMETERS  
FOLK AND WARD,1957

PERCENTILES MEDIAN 5.35 5TH 3.40 16TH 4.29 25TH 4.66  
75TH 6.41 84TH 7.23 95TH 8.60

PER CENT GRAVEL 0.0 SAND 11.19 SILT 79.68 ( 79.56) CLAY 9.12 ( 9.25)

GRAVEL + SAND 11.19 SILT/(SILT+CLAY) 89.58PCT GRAV+SAND/SILT+CLAY 0.13

LABELS SHEPARD -SILT FOLK(GMS)-SANDY MUD (SCS)-SANDY SILT

345

PITT127C

SIEVE, SH. PIP., SEDIGRAPH SAMPLE WT.= 5.8000

PHI PCT. CUMPCT.

2.00			
2.50	0.86		*
	1.90	0.86	**
3.00		2.76	
	3.63		****
3.50		6.39	
	6.39		*****
4.00		12.78	
	8.09		*****
4.50		20.87	
	13.49		*****
5.00		34.36	
	14.39		*****
5.50		48.75	
	17.08		*****
6.00		65.83	
	9.89		*****
6.50		75.72	
	7.19		*****
7.00		82.92	
	6.29		*****
7.50		89.21	
	3.60		****
8.00		92.81	
	3.60		****
8.50		96.40	
	1.80		**
9.00		98.20	
	1.80		**
12.00		100.00	

MEAN ST.DEV. SKEWNESS KURTOSIS

5.54 1.37 0.08 -0.24 KRUMBEIN+PETTICORN(1938) MOMENT MEASURES  
FOR SIZE RANGE 2.5 TO 9.0 PHI

5.61 1.48 0.09 1.18 FOLK GRAPHIC STATISTICAL PARAMETERS  
FOLK AND WARD, 1957

PERCENTILES MEDIAN 5.54 5TH 3.31 16TH 4.20 25TH 4.65  
75TH 6.46 84TH 7.09 95TH 8.30

PER CENT GRAVEL 0.0 SAND 12.78 SILT 80.31 ( 80.03) CLAY 6.91 ( 7.19)

GRAVEL + SAND 12.78 SILT/(SILT+CLAY) 91.75PCT GRAV+SAND/SILT+CLAY 0.15

LABELS SHEPARD -SILT FOLK(GMS)-SANDY MUD (SCS)-SANDY SILT

346

PITT130A

SIEVE, SH. PIP., SEDIGRAPH SAMPLE WT. = 4.2500

PHI PCT. CUMPT.

2.50	0.47		
3.00	3.53	0.47	****
3.50	5.89	4.00	*****
4.00	9.10	9.89	*****
4.50	17.29	19.00	*****
5.00	18.20	36.29	*****
5.50	10.01	54.49	*****
6.00	8.19	64.50	*****
6.50	4.55	72.70	*****
7.00	4.55	77.25	*****
7.50	4.55	81.80	*****
8.00	4.55	86.35	*****
8.50	1.82	90.90	**
9.00	3.64	92.72	****
9.50	3.64	96.36	****
12.00		100.00	

MEAN ST.DEV. SKEWNESS KURTOSIS

5.67 1.50 0.34 -0.17 KRUMREIN+PETTIJOHN(1938) MOMENT MEASURES  
FOR SIZE RANGE 3.0 TO 9.5 PHI

5.82 1.72 0.38 1.27 FOLK GRAPHIC STATISTICAL PARAMETERS  
FOLK AND WARD, 1957

PERCENTILES MEDIAN 5.38 5TH 3.58 16TH 4.34 25TH 4.67  
75TH 6.75 84TH 7.74 95TH 9.31

PER CENT GRAVEL 0.0 SAND 9.89 SILT 77.15 ( 76.45) CLAY 12.96 ( 13.65)

GRAVEL + SAND 9.89 SILT/(SILT+CLAY) 84.85PCT GRAV+SAND/SILT+CLAY 0.11

LABELS SHEPARD -SILT FOLK(GMS)-MUD (SCS)-SILT

347

PITT1308

SIEVE, SH. PIP., SEDIGRAPH SAMPLE WT.= 4.6700

PHI PCT. CUMPCT.

2.50	0.43		
3.00	4.07	0.43	****
3.50	9.22	4.50	*****
4.00	13.21	13.72	*****
4.50	18.49	26.93	*****
5.00	16.73	45.41	*****
5.50	9.68	62.14	*****
6.00	7.92	71.83	*****
6.50	4.40	79.75	****
7.00	4.40	84.15	****
7.50	3.52	88.55	****
8.00	2.64	92.08	***
8.50	1.76	94.72	**
9.00	3.52	96.48	****
12.00		100.00	

MEAN ST.DEV. SKEWNESS KURTOSIS

(5.31) 1.30 0.35 0.01 KRUMBEIN+PETTIGORN(1938) MOMENT MEASURES  
FOR SIZE RANGE 3.0 TO 9.0 PHI

5.40 1.49 0.32 1.20 FOLK GRAPHIC STATISTICAL PARAMETERS  
FOLK AND WARD,1957

PERCENTILES MEDIAN 5.14 5TH 3.53 16TH 4.09 25TH 4.43  
75TH 6.20 84TH 6.98 95TH 8.58

PER CENT GRAVEL 0.0 SAND 13.72 SILT 78.24 ( 78.36) CLAY 8.04 ( 7.92)

GRAVEL + SAND 13.72 SILT/(SILT+CLAY) 90.82PCT GRAV+SAND/SILT+CLAY 0.16

LABELS SHEPARD -SILT FOLK(GMS)-SANDY MUD (SCS)-SANDY SILT

PITT130C

SIEVE, SH. PIP., SEDIGRAPH SAMPLE WT.= 4.3800

PHI PCT. CUMPCT.

1.50	0.23		
2.00	0.23	0.23	
2.50	0.91	0.46	*
3.00	5.02	1.27	*****
3.50	6.85	6.39	*****
4.00	5.31	13.24	*****
4.50	15.05	18.55	*****
5.00	15.54	33.60	*****
5.50	12.39	49.54	*****
6.00	9.74	61.93	*****
6.50	6.20	71.67	*****
7.00	6.20	77.87	*****
7.50	5.31	84.06	*****
8.00	3.54	89.38	*****
8.50	2.56	92.92	*****
9.00	4.43	95.57	*****
12.00		100.00	

MEAN ST.DEV. SKEWNESS KURTOSIS

5.00	1.42	0.12	-0.40	KRUMBEIN+PETTICORN(1938) MOMENT MEASURES FOR SIZE RANGE 2.0 TO 9.0 PHI
5.76	1.65	0.22	1.23	FOLK GRAPHIC STATISTICAL PARAMETERS FOLK AND WARD, 1957

PERCENTILES	MEDIAN	5.52	5TH	3.36	16TH	4.26	25TH	4.71
			75TH	6.77	84TH	7.49	95TH	8.89

PER CENT GRAVEL 0.0 SAND 13.24 SILT 76.48 ( 76.13) CLAY 10.27 ( 10.62)

GRAVEL + SAND 13.24 SILT/(SILT+CLAY) 87.76PCT GRAV+SAND/SILT+CLAY 0.15

LABELS SHEPARD -SILT FOLK(GMS)-SANDY MUD (SCS)-SANDY SILT

PITT131A

SIEVE, SH. PIP., SEDIGRAPH SAMPLE WT.= 4.7800

PHI PCT. CUMPCT.

1.50	0.63	*
2.00	0.21	0.63
2.50	0.63	0.84
3.00	1.40	0.84
3.50	6.07	7.53
4.00	10.88	18.41
4.50	12.62	31.03
5.00	21.87	52.90
5.50	15.98	68.88
6.00	9.25	78.13
6.50	6.73	84.86
7.00	2.52	87.38
7.50	2.52	89.91
8.00	2.52	92.43
8.50	0.84	93.27
9.00	1.68	94.95
9.50	0.84	95.79
10.00	0.84	96.64
10.50	0.84	97.48
12.00	2.52	100.00

MEAN ST.DEV. SKEWNESS KURTOSIS

5.15 1.43 0.57 1.87 KRUMBEIN+PETTITJOHN(1938) MOMENT MEASURES  
FOR SIZE RANGE 2.0 TO 10.5 PHI

5.09 1.51 0.30 1.43 FOLK GRAPHIC STATISTICAL PARAMETERS  
FOLK AND WARD,1957

PERCENTILES MEDIAN 4.93 5TH 3.29 16TH 3.89 25TH 4.26  
75TH 5.83 84TH 6.44 95TH 9.03

PER CENT GRAVEL 0.0 SAND 18.41 SILT 74.27 ( 74.02) CLAY 7.32 ( 7.57)

GRAVEL + SAND 18.41 SILT/(SILT+CLAY) 90.72PCT GRAV+SAND/SILT+CLAY 0.23

PITT131B

SIEVE, SH. PIP., SEDIGRAPH SAMPLE WT.= 3.9400

PHI PCT. CUMPCT.

1.50	0.25		
2.00	0.76	1.02	*
2.50	1.52	1.02	**
3.00	2.61	2.54	*****
3.50	7.62	9.15	*****
4.00	8.67	16.77	*****
4.50	19.07	25.44	*****
5.00	15.61	44.52	*****
5.50	12.14	60.12	*****
6.00	6.94	72.26	*****
6.50	5.20	75.19	*****
7.00	4.33	84.39	****
7.50	2.60	88.73	***
8.00	1.73	91.33	**
8.50	1.73	93.06	**
9.00	1.73	94.80	**
9.50	0.37	96.53	*
10.00	2.60	97.40	***
12.00		100.00	

MEAN ST.DEV. SKEWNESS KURTOSIS

5.33 1.48 0.34 0.51 KRUMBEIN+PETT(1938) MOMENT MEASURES  
FOR SIZE RANGE 2.0 TO 10.0 PHI

5.36 1.64 0.25 1.41 FOLK GRAPHIC STATISTICAL PARAMETERS  
FOLK AND WARD, 1957

PERCENTILES MEDIAN 5.18 5TH 3.19 16TH 3.95 25TH 4.47  
75TH 6.20 84TH 6.96 95TH 9.06

PER CENT GRAVEL 0.0 SAND 16.77 SILT 74.97 ( 74.56) CLAY 8.26 ( 8.67)

GRAVEL + SAND 16.77 SILT/(SILT+CLAY) 89.58PCT GRAV+SAND/SILT+CLAY 0.20



PITT131C

SIEVE, SH. PIP., SEDIGRAPH SAMPLE WT.= 4.7100

PHI PCT. CUMPCT.

2.00	0.21		
2.50	1.28	0.21	*
3.00	5.95	1.49	*****
3.50	7.01	7.44	*****
4.00	7.06	14.45	*****
4.50	17.64	21.51	*****
5.00	18.52	39.15	*****
5.50	12.35	57.67	*****
6.00	7.94	70.01	*****
6.50	5.29	77.95	*****
7.00	4.41	83.24	****
7.50	3.53	87.65	****
8.00	1.76	91.18	**
8.50	1.76	92.94	**
9.00	1.76	94.71	**
9.50	3.53	96.47	****
12.00		100.00	

MEAN ST.DEV. SKEWNESS KURTOSIS

5.42	1.39	0.30	0.26	KRUMBEIN+PETTICORN(1938) MOMENT MEASURES FOR SIZE RANGE 2.5 TO 9.5 PHI
5.50	1.62	0.26	1.39	FOLK GRAPHIC STATISTICAL PARAMETERS FOLK AND WARD,1957

PERCENTILES	MEDIAN	5.29	5TH	3.30	16TH	4.11	25TH	4.60
			75TH	6.31	84TH	7.09	95TH	9.08

PER CENT GRAVEL 0.0 SAND 14.45 SILT 77.05 ( 76.73) CLAY 8.50 ( 8.82)

GRAVEL + SAND 14.45 SILT/(SILT+CLAY) 89.69PCT GRAV+SAND/SILT+CLAY 0.17

LABELS SHEPARD -SILT FOLK(GMS)-SANDY MUD (SCS)-SANDY SILT

PI++ 132A 0 0.0 0 0.0 0

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 \*\*\* MULTIMOAL SAMPLE \*\*\*  
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WET WT	DRY WT	SALT	ORGANIC	MOISTURE	WEIGHT LOSS DUE TO HANDLING	0.0
1000.0000	7.9100	0.0	0.0	0.0 (GRAMS)	GRAVEL CORRECTION FACTOR	1.000
100.0000	100.0000	0.0	0.0	0.0 (PCT WET WT)	SIZES ELIMINATED (<0.01)	NONE
					TRASK SORTING COEFFICIENT	2.260
					USING PROBABILITY EXTRAP.	2.239
					MEAN CUBED DEVIATION	21.106
					USING PROBABILITY EXTRAP.	17.671

PERCENTAGE COMPOSITION		TABLE OF STATISTICAL DATA IN PHI UNITS					PERCENTILES		LINEAR EXTRAP.		PROBABILITY EXTRAP.	
		MEAN	STD DEV	SKWENESS	KURTOSIS		MM.	PHI UNITS	MM.	PHI UNITS		
GRAVEL	0.0	MOMENT 5.54481	2.39540	1.53590	5.14592	5.0	0.11736	3.09094	0.11315	3.14368		
SAND	28.55	P-MOMENT 5.53067	2.30231	1.44798	4.70631	10.0	0.09888	3.33618	0.09546	3.38894		
SILT	58.32	FOLK 5.31179	2.16554	0.38535	1.43714	16.0	0.08311	3.58885	0.08205	3.60741		
CLAY	12.72	P-FOLK 5.31566	2.16608	0.59231	1.44184	25.0	0.06818	3.87457	0.06731	3.89313		
MUD	71.05	INMAN 5.45978	1.87093	0.23731	1.20491	50.0	0.03091	5.01580	0.03091	5.01573		
S/M	0.41	P-INMAN 5.46562	1.85821	0.24211	1.20207	75.0	0.01335	6.22739	0.01342	6.21935		
		KPUMBEIN 1.74283	0.03518	0.20979		84.0	0.00621	7.33071	0.00624	7.32384		
		P-KPUM. 1.72312	0.04051	0.20947		90.0	0.00203	8.94569	0.00203	8.94160		
		FOLK (TRANSFORMED) 0.58968				95.0	0.00039	11.34142	0.00039	11.32750		
		P-FOLK (TRANSFORMED) 0.59047										

DATA FOR CONSTN OF BARGRAPHS AND CUM. CURVES

SIZE FRACTION	WT.(GMS)	WT.PCT.	WT.PCT.	MID PHI(LINEAR)	MID PHI(PROB.)	MODE				
MM	PHI	UNCOR	COR	COR	CUMUL.	PHI	MM	PHI	MM	
0.250000	2.000	0.070	0.070	0.885	0.885	1.751	0.29707	1.911	0.26599	1
0.177000	2.498	0.030	0.030	0.379	1.264	2.249	0.21036	2.268	0.20757	0
0.125000	3.000	0.150	0.150	1.896	3.161	2.749	0.14875	2.796	0.14396	0
0.088000	3.506	0.810	0.810	10.240	13.401	3.253	0.10488	3.316	0.10226	0
0.062500	4.000	1.230	1.230	15.550	28.951	3.753	0.07416	3.781	0.07276	1*
0.044000	4.506	0.895	0.895	11.314	40.265	4.253	0.05244	4.261	0.05216	0
0.031000	5.012	0.161	0.161	2.626	49.891	4.759	0.03693	4.761	0.03688	0
0.022000	5.506	1.006	1.006	12.714	62.606	5.259	0.02612	5.256	0.02617	1
0.015000	6.002	0.765	0.765	9.723	72.328	5.754	0.01853	5.747	0.01862	0
0.011000	6.506	0.473	0.473	5.983	78.311	6.254	0.01310	6.246	0.01317	0
0.007800	7.002	0.296	0.296	3.740	82.051	6.754	0.00926	6.747	0.00931	0
0.005500	7.506	0.237	0.237	2.992	85.042	7.254	0.00655	7.247	0.00658	0
0.003900	8.002	0.177	0.177	2.243	87.286	7.754	0.00463	7.747	0.00465	0
0.002700	8.503	0.118	0.118	1.496	88.782	8.268	0.00325	8.262	0.00326	0
0.001900	9.040	0.118	0.118	1.496	90.277	8.786	0.00227	8.780	0.00228	0
0.001360	9.501	0.118	0.118	1.496	91.773	9.270	0.00162	9.263	0.00163	1
0.000980	9.995	0.059	0.059	0.748	92.521	9.748	0.00116	9.744	0.00117	0
0.000690	10.501	0.059	0.059	0.748	93.269	10.248	0.00082	10.243	0.00083	1
0.000490	10.995	0.059	0.059	0.748	94.017	10.748	0.00058	10.742	0.00058	0
0.000340	11.522	0.118	0.118	1.496	95.513	11.259	0.00041	11.243	0.00041	1
0.000240	12.025	0.059	0.059	0.748	96.260	11.773	0.00029	11.764	0.00029	0

0.000061 14.000 0.296 0.296 3.740 100.000 13.012 0.00012 12.329 0.00019 0  
 TOTALS 7.910 7.910 100.0

P1+ 1328 0 0.0 0 0.0 0

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 \*\*\* MULTIMODAL SAMPLE \*\*\*  
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WET WT	DPY WT	SALT	ORGANIC	MOISTURE	WEIGHT LOSS DUE TO HANDLING	0.0
1000.0000	8.9200	0.0	0.0	0.0 (GRAMS)	GRAVEL CORRECTION FACTOR	1.000
99.9999	100.0000	0.0	0.0	0.0 (PCT WET WT)	SIZES ELIMINATED (CG.01%)	NONE
					TRASK SORTING COEFFICIENT	2.452
					USING PROBABILITY EXTRAP.	2.435
					MEAN CUBED DEVIATION	30.729
					USING PROBABILITY EXTRAP.	25.422

PERCENTAGE COMPOSITION		TABLE OF STATISTICAL DATA IN PHI UNITS				PERCENTILES		LINEAR EXTRAP.		PROBABILITY EXTRAP.	
		MEAN	STD DEV	SKEWNESS	KURTOSIS	MM.	PHI UNITS	MM.	PHI UNITS		
GRAVEL	0.0	MOMENT 5.32545	2.72786	1.51384	4.54831	5.0	0.15305	2.70790	0.14333	2.80257	
SAND	41.93	P-MOMENT 5.30363	2.60885	1.43171	4.18397	10.0	0.12545	2.99484	0.12524	2.99726	
SILT	43.69	FOLK 5.03235	2.52832	0.54917	1.49793	16.0	0.11102	3.17111	0.10809	3.20565	
CLAY	14.38	P-FOLK 5.04487	2.48586	0.56148	1.47352	25.0	0.09257	3.43168	0.09166	3.44754	
MUD	58.07	INMAN 5.36139	2.19028	0.45068	1.15930	50.0	0.04822	4.37427	0.04820	4.37486	
S/M	0.72	P-INMAN 5.37988	2.17023	0.46309	1.12994	75.0	0.01541	6.01967	0.01542	6.01887	
		KEUMEEIN 1.91703	0.35141	0.18956		84.0	0.00533	7.55167	0.00534	7.55011	
		P-KEUM. 1.90469	0.35635	0.18854		90.0	0.00111	9.82129	0.00111	9.81640	
		FOLK (TRANSFORMED)		0.59967		95.0	0.00022	12.16687	0.00024	12.04749	
		P-FOLK (TRANSFORMED)		0.59572							

DATA FOR CONSTN OF BARGRAPHS AND CUM. CURVES

Done

SIZE FRACTION	WT.(GMS)		WT.PCT.		MID PHI(LINEAR)		MID PHI(PROB.)		MODE	
	MM	PHI	UNCCR	COR	COR	CUMUL.	PHI	MM		
0.250000	2.000	0.080	0.080	0.497	0.697	1.751	0.29707	1.911	0.26596	1
0.177000	2.498	0.040	0.040	0.448	1.345	2.249	0.21036	2.271	0.20720	0
0.125000	3.000	0.780	0.780	8.744	10.090	2.749	0.14875	2.858	0.13987	0
0.087500	3.500	1.560	1.560	17.489	27.578	3.253	0.10488	3.292	0.10211	1*
0.062500	4.000	1.280	1.280	14.350	41.928	3.753	0.07416	3.763	0.07387	0
0.044000	4.506	0.974	0.974	10.920	52.848	4.253	0.05244	4.254	0.05240	0
0.031000	5.012	0.468	0.468	5.245	58.093	4.759	0.03693	4.758	0.03598	0
0.022000	5.506	0.961	0.961	10.776	68.869	5.259	0.02612	5.253	0.02623	1
0.015600	6.002	0.534	0.534	5.987	74.855	5.754	0.01853	5.748	0.01861	0
0.011000	6.506	0.374	0.374	4.191	79.047	6.254	0.01310	6.248	0.01316	0
0.007800	7.002	0.214	0.214	2.395	81.441	6.754	0.00926	6.750	0.00929	0
0.005500	7.500	0.214	0.214	2.395	83.836	7.254	0.00655	7.249	0.00658	1
0.003900	8.002	0.160	0.160	1.796	85.632	7.754	0.00463	7.749	0.00465	0
0.002700	8.533	0.107	0.107	1.197	86.829	8.268	0.00325	8.264	0.00325	0
0.001900	9.040	0.107	0.107	1.197	88.026	8.786	0.00227	8.782	0.00227	0
0.001300	9.501	0.107	0.107	1.197	89.224	9.270	0.00162	9.266	0.00162	0
0.000980	9.995	0.107	0.107	1.197	90.421	9.748	0.00116	9.743	0.00117	0
0.000690	10.501	0.107	0.107	1.197	91.618	10.240	0.00082	10.242	0.00083	0
0.000490	10.995	0.107	0.107	1.198	92.816	10.748	0.00058	10.741	0.00058	1
0.000340	11.522	0.107	0.107	1.197	94.013	11.259	0.00041	11.249	0.00041	0
0.000240	12.025	0.053	0.053	0.599	94.612	11.773	0.00029	11.768	0.00029	0

PI++ 133A C 0.0 0 0.0 0.

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 \*\*\* MULTIMODAL SAMPLE \*\*\*  
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WET WT	DRY WT	SALT	ORGANIC	MOISTURE	WEIGHT LOSS DUE TO HANDLING	0.0
1000.0000	8.0200	0.0	0.0	0.0 (GRAMS)	GRAVEL CORRECTION FACTOR	1.000
99.9999	100.0000	0.0	0.0	0.0 (PCT WET WT)	SIZES ELIMINATED (<0.01%)	NONE
					TRASK SORTING COEFFICIENT	2.218
					USING PROBABILITY EXTRAP.	2.210
					MEAN CUBED DEVIATION	23.169
					USING PROBABILITY EXTRAP.	19.762

PERCENTAGE COMPOSITION TABLE OF STATISTICAL DATA IN PHI UNITS PERCENTILES LINEAR EXTRAP. PROBABILITY EXTRAP.

	PERCENTAGE COMPOSITION	TABLE OF STATISTICAL DATA IN PHI UNITS	STATISTICAL DATA				PERCENTILES		LINEAR EXTRAP.		PROBABILITY EXTRAP.	
			MEAN	STD DEV	SKEWNESS	KURTOSIS	MM.	PHI UNITS	MM.	PHI UNITS		
GRAVEL	0.0	MOMENT	4.50676	2.26962	1.98171	7.19375	5.0	0.17334	2.52634	0.16949	2.56071	
SAND	57.36	P-MOMENT	4.50765	2.18476	1.89509	6.63331	10.0	0.15953	2.64812	0.15105	2.72686	
SILT	35.16	FCLK	4.17936	1.85558	0.54769	1.22782	16.0	0.14440	2.79185	0.13791	2.85816	
CLAY	7.48	P-FCLK	4.20043	1.83270	0.56641	1.22675	25.0	0.12433	3.00775	0.12423	3.00890	
MUD	42.64	INMAN	4.41614	1.62429	0.43733	1.11991	50.0	0.07664	3.70579	0.07666	3.70542	
S/M	1.35	P-INMAN	4.44794	1.58978	0.46706	1.15424	75.0	0.02527	5.30647	0.02543	5.29722	
		KFUMBEIN	1.70276	0.45132	0.25473	0.25473	84.0	0.01519	6.04043	0.01522	6.03772	
		P-KFUMBEIN	1.69505	0.44764	0.25849	0.25849	90.0	0.00699	7.16022	0.00703	7.15311	
		FCLK (TRANSFORMED)				0.55113	95.0	0.00146	9.41503	0.00147	9.41025	
		P-FCLK (TRANSFORMED)				0.55091						

DATA FOR CONSTN OF BARGRAPHS AND CUM. CURVES

SIZE FRACTION	WT.(GMS)		WT.PCT.		MID PHI(LINEAR)		MID PHI(PROB.)		MODE	
	MM	PHI	UNCOR	COR	PHI	MM	PHI	MM		
0.250000	2.000	0.100	0.100	1.247	1.247	1.751	0.29707	1.915	0.26925	0
0.177000	2.498	0.200	0.200	2.494	3.741	2.249	0.21036	2.304	0.20248	0
0.125000	3.000	1.680	1.680	20.948	24.688	2.749	0.14875	2.823	0.14129	1*
0.088000	3.506	1.630	1.630	20.324	45.012	3.253	0.10488	3.267	0.10387	0
0.062500	4.000	0.990	0.990	12.344	57.357	3.753	0.07416	3.753	0.07419	0
0.044000	4.566	0.482	0.482	6.011	63.367	4.253	0.05244	4.251	0.05254	0
0.031000	5.312	0.576	0.576	7.178	70.546	4.759	0.03693	4.753	0.03707	0
0.022000	5.906	0.599	0.599	7.473	78.019	5.259	0.02612	5.250	0.02625	1
0.015000	6.002	0.458	0.458	5.715	83.734	5.754	0.01853	5.743	0.01867	0
0.011000	6.506	0.282	0.282	3.517	87.251	6.254	0.01310	6.244	0.01319	0
0.007800	7.002	0.176	0.176	2.198	89.449	6.754	0.00926	6.746	0.00932	0
0.005500	7.506	0.141	0.141	1.759	91.208	7.254	0.00655	7.246	0.00659	0
0.002900	8.002	0.106	0.106	1.319	92.526	7.754	0.00463	7.747	0.00466	0
0.002700	8.533	0.071	0.071	0.880	93.406	8.268	0.00325	8.261	0.00326	0
0.001900	9.040	0.070	0.070	0.879	94.285	8.786	0.00227	8.779	0.00228	0
0.001380	9.561	0.070	0.070	0.879	95.164	9.270	0.00162	9.263	0.00163	1
0.000980	9.995	0.035	0.035	0.440	95.603	9.748	0.00116	9.743	0.00117	0
0.000690	10.501	0.035	0.035	0.440	96.044	10.248	0.00082	10.243	0.00083	1
0.000490	10.995	0.035	0.035	0.440	96.483	10.748	0.00058	10.742	0.00058	0
0.000340	11.522	0.035	0.035	0.440	96.923	11.259	0.00041	11.251	0.00041	1
0.000240	12.025	0.035	0.035	0.440	97.362	11.773	0.00029	11.765	0.00029	1

0.000061 14.000 0.212 0.212 2.638 100.000 13.012 0.00012 12.337 0.00019 0  
 TOTALS 8.020 8.020 100.0



PIT136

SIEVE, SH. PIP., SEDIGRAPH SAMPLE WT.= 4.3900

PHI PCT. CUMPCT.

3.00	2.51	***
3.50	2.51	*****
4.00	7.74	*****
4.50	14.33	*****
5.00	28.46	*****
5.50	43.52	*****
6.00	57.64	*****
6.50	67.05	***
7.00	70.82	***
7.50	73.64	***
8.00	76.47	**
8.50	78.35	**
9.00	80.23	***
9.50	83.06	*
10.00	84.00	****
10.50	87.76	**
11.00	89.64	**
11.50	91.53	*
12.00	92.47	***
12.50	95.29	*****
12.00	100.00	

MEAN ST.DEV. SKEWNESS KURTOSIS

6.33 2.23 0.58 0.46 KRUMBEIN+PETTIGRAPH (1938) MOMENT MEASURES  
FOR SIZE RANGE 3.5 TO 12.5 PHI

6.76 2.68 0.56 1.64 FOLK GRAPHIC STATISTICAL PARAMETERS  
FOLK AND WARD, 1957

PERCENTILES MEDIAN 5.73 5TH 3.74 16TH 4.56 25TH 4.88  
75TH 7.74 84TH 10.00 95TH 12.45

PER CENT GRAVEL 0.0 SAND 7.74 SILT 68.91 ( 68.72) CLAY 23.35 ( 23.53)

P1+ 137 0 0.0 0 0.0 0

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 \*\*\* MULTIMODAL SAMPLE \*\*\*  
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WET WT DRY WT SALT ORGANIC MOISTURE  
 1000.0000 5.0000 0.0 0.0 0.0  
 100.0000 100.0000 0.0 0.0 0.0  
 (GRAMS) (PCT WET WT)

WEIGHT LOSS DUE TO HANDLING 0.0  
 GRAVEL CORRECTION FACTOR 1.000  
 SIZES ELIMINATED (<0.01%) NONE  
 TRASK SORTING COEFFICIENT 1.848  
 USING PROBABILITY EXTRAP. 1.531  
 MEAN CUBED DEVIATION 5.657  
 USING PROBABILITY EXTRAP. 4.544

PERCENTAGE COMPOSITION

TABLE OF STATISTICAL DATA IN PHI UNITS

PERCENTILES

LINEAR EXTRAP.

PROBABILITY EXTRAP.

GRAVEL	SAND	SILT	CLAY	MUD	S/M	MOMENT	P-MOMENT	FOLK	P-FOLK	INMAR	P-INMAN	KPUMBEIN	P-KPUM.	FGLK (TRANSFORMED)	P-FGLK (TRANSFORMED)	MEAN	STD DEV	SKEWNESS	KURTOSIS	PERCENTILES		LINEAR EXTRAP.		PROBABILITY EXTRAP.	
																				MM.	PHI UNITS	MM.	PHI UNITS		
0.0	28.40	65.63	5.97	71.60	0.40	5.00902	5.00873	4.85852	4.85704	4.89110	4.88861	1.31246	1.29296	0.54916	0.54970	5.00902	1.58568	1.41879	5.96666	5.0	0.11826	3.07994	0.11411	3.13147	
																				10.0	0.10139	3.30202	0.09727	3.36187	
																				16.0	0.08500	3.55642	0.08438	3.56696	
																				25.0	0.06800	3.87836	0.06726	3.85416	
																				50.0	0.03606	4.79336	0.03605	4.75391	
																				75.0	0.01991	5.65018	0.02006	5.63965	
																				84.0	0.01336	6.22579	0.01351	6.21026	
																				90.0	0.00859	6.86262	0.00867	6.84944	
																				95.0	0.00307	8.34609	0.00310	8.33193	

DATA FOR CONSTN OF BARGRAPHS AND CUM. CURVES

SIZE FRACTION	MM	PHI	WT.(GMS)		WT.PCT. COR	WT.PCT. CUMUL.	MID PHI(LINEAR)		MID PHI(PROB.)		MODE
			UNCOR	COR			PHI	MM	PHI	MM	
0.250000	2.000	0.010	0.010	0.200	0.200	1.751	0.29707	1.883	0.27111	0	
0.177000	2.498	0.010	0.010	0.200	0.400	2.249	0.21036	2.287	0.20486	0	
0.125000	3.000	0.140	0.140	2.800	3.200	2.749	0.14875	2.846	0.13904	0	
0.088000	3.506	0.570	0.570	11.400	14.000	3.253	0.10488	3.320	0.10311	0	
0.062500	4.000	0.690	0.690	13.800	28.400	3.753	0.07416	3.777	0.07295	1	
0.044000	4.506	0.588	0.588	11.750	40.150	4.253	0.05244	4.261	0.05214	0	
0.031000	5.012	0.867	0.867	17.338	57.488	4.759	0.03693	4.760	0.03691	1	
0.022000	5.506	0.746	0.746	14.916	72.404	5.259	0.02612	5.249	0.02629	0	
0.015600	6.002	0.447	0.447	8.950	81.554	5.754	0.01853	5.741	0.01870	0	
0.011000	6.506	0.298	0.298	5.967	87.521	6.254	0.01310	6.238	0.01325	0	
0.007800	7.002	0.186	0.186	3.729	91.050	6.754	0.00926	6.739	0.00936	0	
0.005500	7.506	0.075	0.075	1.492	92.542	7.254	0.00655	7.246	0.00659	0	
0.003900	8.002	0.075	0.075	1.491	94.033	7.754	0.00463	7.744	0.00467	0	
0.002700	8.533	0.075	0.075	1.492	95.525	8.268	0.00325	8.252	0.00328	1	
0.001900	9.046	0.037	0.037	0.746	96.271	8.786	0.00227	8.777	0.00228	0	
0.001380	9.501	0.075	0.075	1.492	97.763	9.270	0.00152	9.246	0.00165	1	
0.000980	9.995	0.075	0.075	1.491	99.254	9.748	0.00116	9.692	0.00121	0	
0.000061	14.000	0.037	0.037	0.746	100.000	11.997	0.00024	10.733	0.00059	0	
TOTALS			5.000	5.000	100.0						
0.250000	0.030000										
0.177000	0.030000										

PI+ 138 0 0.0 0 0.0 0

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 \*\*\* MULTIMODAL SAMPLE \*\*\*  
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WET WT	DRY WT	SALT	ORGANIC	MOISTURE	WEIGHT LOSS DUE TO HANDLING	0.0
1000.0000	6.0300	0.0	0.0	0.0 (GRAMS)	GRAVEL CORRECTION FACTOR	1.000
100.0000	100.0000	0.0	0.0	0.0 (PCT WET WT)	SIZES ELIMINATED (KO.01%)	NONE
					TRASK SORTING COEFFICIENT	2.086
					USING PROBABILITY EXTRAP.	2.086
					MEAN CUBED DEVIATION	10.910
					USING PROBABILITY EXTRAP.	5.812

PERCENTAGE COMPOSITION	TABLE OF STATISTICAL DATA IN PHI UNITS					PERCENTILES		LINEAR EXTRAP.		PROBABILITY EXTRAP.	
		MPAN	STD DEV	SKEWNESS	KURTOSIS	MM.	PHI UNITS	MM.	PHI UNITS		
GRAVEL 0.0	MOMENT 5.15899	1.93139	1.81435	5.76153	5.0	0.12198	3.03522	0.11954	3.05965		
SAND 31.84	P-MOMENT 5.11450	1.73799	1.10719	3.98882	10.0	0.10573	3.24153	0.10133	3.30279		
SILT 60.34	FCLK 5.01066	1.68515	0.29443	1.10890	16.0	0.08906	3.48506	0.08870	3.49494		
CLAY 7.82	P-FCLK 5.00971	1.67555	0.29644	1.11578	25.0	0.07274	3.78103	0.07168	3.80250		
MUD 68.16	INMAN 5.11993	1.63084	0.20100	0.75991	50.0	0.03609	4.75213	0.03608	4.79245		
S/M 0.47	P-INMAN 5.11834	1.62340	0.20074	0.75600	75.0	0.01672	5.90255	0.01679	5.89648		
	KPUMKRN 1.57150	0.04966	0.24228		84.0	0.00929	6.75077	0.00934	6.74173		
	P-KPUM. 1.55124	0.05694	0.24308		90.0	0.00508	7.61985	0.00512	7.61032		
	FCLK (TRANSFORMED)		0.52582		95.0	0.00228	8.77547	0.00230	8.76103		
	P-FCLK (TRANSFORMED)		0.52736								

DATA FOR CONSTN OF BARGRAPHS AND CUM. CURVES

SIZE FRACTION	WT. (GMS)		WT. PCT.		MID PHI (LINEAR)		MID PHI (PROB.)		MODE	
	MM	PHI	UNCOR	COP	COR	CUMUL.	PHI	MM		
0.250000	2.000	0.030	0.030	0.498	0.498	1.751	0.29707	1.402	0.26757	1
0.177000	2.498	0.030	0.030	0.498	0.995	2.249	0.21036	2.286	0.20498	0
0.125000	3.000	0.190	0.190	3.151	4.146	2.749	0.14875	2.819	0.14169	0
0.088000	3.506	0.740	0.740	12.272	16.418	3.253	0.10488	3.313	0.10359	0
0.062500	4.000	0.930	0.930	15.423	31.841	3.753	0.07416	3.775	0.07303	1*
0.044000	4.506	0.625	0.625	10.370	42.211	4.253	0.05244	4.259	0.05223	0
0.031000	5.012	0.830	0.830	13.770	55.981	4.759	0.03693	4.759	0.03692	1
0.022000	5.506	0.771	0.771	12.779	68.760	5.259	0.02612	5.252	0.02624	0
0.015000	6.002	0.471	0.471	7.310	76.571	5.754	0.01853	5.745	0.01864	0
0.011000	6.506	0.342	0.342	5.680	82.250	6.254	0.01310	6.244	0.01315	0
0.007800	7.002	0.214	0.214	3.550	85.800	6.754	0.00926	6.745	0.00932	0
0.005500	7.506	0.214	0.214	3.550	89.350	7.254	0.00655	7.242	0.00661	1
0.003900	8.002	0.171	0.171	2.840	92.190	7.754	0.00463	7.740	0.00468	0
0.002700	8.533	0.128	0.128	2.130	94.320	8.268	0.00325	8.251	0.00328	0
0.001900	9.040	0.086	0.086	1.420	95.740	8.786	0.00227	8.772	0.00229	0
0.001380	9.501	0.043	0.043	0.710	96.450	9.270	0.00162	9.262	0.00163	0
0.001061	14.000	0.214	0.214	3.550	100.000	11.751	0.00029	10.197	0.00085	0
TOTALS		6.030	6.030	100.0						
0.250000	0.030000									
0.177000	0.010000									
0.125000	0.180000									



PI++ 139 0 0.0 0 0.0 0

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 \*\*\*\* MULTIMODAL SAMPLE \*\*\*\*  
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WET WT DRY WT SALT ORGANIC MOISTURE  
 1003.0000 5.3400 0.0 0.0 0.0 (GRAMS)  
 99.9999 100.0000 0.0 0.0 0.0 (PCT WET WT)

WEIGHT LOSS DUE TO HANDLING 0.0  
 GRAVEL CORRECTION FACTOR 1.000  
 SIZES ELIMINATED (<0.01%) NONE  
 TRASK SORTING COEFFICIENT 1.976  
 USING PROBABILITY EXTRAP. 1.956  
 MEAN CUBED DEVIATION 11.992  
 USING PROBABILITY EXTRAP. 7.663

PERCENTAGE COMPOSITION	TABLE OF STATISTICAL DATA IN PHI UNITS					PERCENTILES		LINEAR EXTRAP.		PROBABILITY EXTRAP.	
	GRAVEL	SAND	SILT	CLAY	MUD	S/M	MM.	PHI UNITS	MM.	PHI UNITS	
	0.0	32.21	60.57	7.22	67.79	0.48					
	MEAN	STD DEV	SKEWNESS	KURTOSIS							
	5.03403	1.90546	1.73337	6.56473							
	MOMENT	5.00610	1.75075	1.42754	5.00869		5.0	0.12217	3.03304	0.12009	3.05761
	P-MOMENT	4.81995	1.64918	0.33258	1.25922		10.0	0.10726	3.22081	0.10252	3.26595
	FOLK	4.82220	1.63724	0.33696	1.27286		16.0	0.09175	3.44614	0.09048	3.46624
	P-FOLK	4.91501	1.46887	0.19414	1.05508		25.0	0.07400	3.75632	0.07299	3.77334
	INMAN	4.91926	1.45302	0.20040	1.06859		50.0	0.04039	4.62983	0.04044	4.62808
	P-INMAN		1.45552	0.10896	0.23731		75.0	0.01895	5.72127	0.01908	5.71172
	KRUMBEIN		1.43383	0.11580	0.23798		84.0	0.01197	6.38366	0.01207	6.37226
	P-KRUMBEIN				0.23798		90.0	0.00608	7.36078	0.00612	7.35278
	FOLK (TRANSFORMED)				0.55737		95.0	0.00186	9.07033	0.00186	9.06663
	P-FOLK (TRANSFORMED)				0.55999						

DATA FOR CONSTN OF BARGRAPHS AND CUM. CURVES

SIZE FRACTION	WT.(GMS)		WT.PCT.		MID PHI(LINEAR)		MID PHI(PROB.)		MODE	
	MM	PHI	UNCOR	COR	CUMUL.	PHI	MM	PHI		
0.250000	2.000	0.030	0.030	0.562	0.562	1.751	0.29707	1.904	0.26720	1
0.177000	2.498	0.010	0.010	0.167	0.749	2.249	0.21036	2.265	0.20807	0
0.125000	3.000	0.180	0.180	3.371	4.120	2.749	0.14875	2.831	0.14054	0
0.088000	3.506	0.720	0.720	13.483	17.603	3.253	0.10488	3.316	0.10342	0
0.062500	4.000	0.780	0.780	14.607	32.210	3.753	0.07416	3.773	0.07515	1
0.044000	4.506	0.799	0.799	13.280	45.490	4.253	0.05244	4.259	0.05221	0
0.031000	5.012	0.985	0.985	18.451	63.941	4.759	0.03693	4.755	0.03702	1*
0.022000	5.506	0.424	0.424	7.934	71.675	5.259	0.02612	5.253	0.02621	0
0.015000	6.002	0.385	0.385	7.212	79.086	5.754	0.01853	5.744	0.01865	0
0.011000	6.506	0.347	0.347	6.491	85.577	6.254	0.01310	6.240	0.01323	0
0.007800	7.002	0.154	0.154	2.885	88.462	6.754	0.00926	6.745	0.00932	0
0.005500	7.506	0.115	0.115	2.163	90.625	7.254	0.00655	7.245	0.00659	0
0.003900	8.002	0.116	0.116	2.164	92.788	7.754	0.00463	7.742	0.00467	1
0.002700	8.533	0.038	0.038	0.721	93.509	8.268	0.00325	8.262	0.00326	0
0.001900	9.040	0.077	0.077	1.443	94.952	8.786	0.00227	8.774	0.00228	1
0.001300	9.501	0.039	0.039	0.721	95.673	9.270	0.00162	9.263	0.00163	0
0.000900	9.995	0.077	0.077	1.442	97.115	9.748	0.00116	9.728	0.00116	0
0.000061	14.000	0.154	0.154	2.885	100.000	11.997	0.00024	10.624	0.00063	0
TOTALS				5.340	5.340	100.0				
0.250000	0.030000									
0.177000	0.030000									

PL# 140 0 0.0 0 0.0 0

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 MULTIMODAL SAMPLE  
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WET WT	DRY WT	SALT	ORGANIC	MOISTURE	WEIGHT LOSS DUE TO HANDLING	0.0
1000.0000	6.0900	0.0	0.0	0.0 (GRAMS)	GRAVEL CORRECTION FACTOR	1.000
100.0000	100.0000	0.0	0.0	0.0 (PCT WET WT)	SIZES ELIMINATED (<0.075)	NONE
					TRASK SORTING COEFFICIENT	1.974
					USING PROBABILITY EXTRAP.	1.970
					MEAN CUBED DEVIATION	8.875
					USING PROBABILITY EXTRAP.	4.459

PERCENTAGE COMPOSITION	TABLE OF STATISTICAL DATA IN PHI UNITS					PERCENTILES	LINEAR EXTRAP.		PROBABILITY EXTRAP.	
		MEAN	STD DEV	SKEWNESS	KURTOSIS		MM.	PHI UNITS	MM.	PHI UNITS
GRAVEL 0.0	MOMENT	5.21568	1.75895	1.63083	6.96997	5.0	0.11604	3.10735	0.11181	3.16052
SAND 25.29	P-MOMENT	5.17539	1.57455	1.14219	4.78355	10.0	0.09520	3.39288	0.09289	3.42637
SILT 68.48	FOLK	5.01978	1.50134	0.16113	1.10958	16.0	0.07937	3.65528	0.07793	3.68165
CLAY 4.23	P-FULK	5.02576	1.48261	0.18980	1.04930	25.0	0.06296	3.98932	0.06288	3.99126
MUD 74.71	INMAN	5.04806	1.39277	0.06092	0.90723	50.0	0.03206	4.96321	0.03203	4.96450
S/M 0.34	P-INMAN	5.05643	1.37477	0.06687	0.90886	75.0	0.01616	5.95163	0.01620	5.94798
	KPUMBEIN		1.45356	0.00726	0.27644	84.0	0.01151	6.44083	0.01159	6.43120
	P-KPUM.		1.44942	0.00512	0.27920	90.0	0.00813	6.94211	0.00819	6.93253
	FOLK (TRANSFORMED)				0.52597	95.0	0.00292	8.42004	0.00294	8.40541
	P-FOLK (TRANSFORMED)				0.52365					

DATA FOR CONSTN OF BARGRAPHS AND CUM. CURVES

SIZE FRACTION	MM	PHI	WT.(GMS)		WT.PCT. COR	WT.PCT. CUMUL.	MID PHI(LINEAR)		MID PHI(PROB.)		MODE
			UNCOR	COR			PHI	MM	PHI	MM	
0.250000	2.000	2.000	0.030	0.030	0.493	0.493	1.751	0.29707	1.902	0.26760	0
0.177000	2.498	2.498	0.030	0.030	0.493	0.965	2.249	0.21036	2.296	0.20498	0
0.125000	3.000	3.000	0.130	0.130	2.135	3.120	2.749	0.14875	2.808	0.14263	0
0.088000	3.506	3.506	0.540	0.540	8.867	11.487	3.253	0.10488	3.315	0.10349	0
0.062500	4.000	4.000	0.810	0.810	13.300	25.287	3.753	0.07416	3.761	0.07272	1
0.044000	4.506	4.506	0.499	0.499	8.196	33.484	4.253	0.05244	4.261	0.05214	0
0.031000	5.012	5.012	1.112	1.112	18.264	51.748	4.759	0.03693	4.765	0.03579	1*
0.022000	5.506	5.506	0.948	0.948	15.566	67.314	5.259	0.02612	5.253	0.02623	0
0.015600	6.002	6.002	0.521	0.521	8.561	75.874	5.754	0.01853	5.745	0.01864	0
0.011000	6.506	6.506	0.569	0.569	9.339	85.213	6.254	0.01310	6.236	0.01327	1
0.007800	7.002	7.002	0.332	0.332	5.447	90.661	6.754	0.00926	6.734	0.00939	0
0.005500	7.506	7.506	0.095	0.095	1.557	92.218	7.254	0.00655	7.246	0.00659	0
0.003900	8.002	8.002	0.095	0.095	1.557	93.774	7.754	0.00463	7.744	0.00467	1
0.002700	8.533	8.533	0.095	0.095	1.557	95.331	8.268	0.00325	8.252	0.00328	1
0.001900	9.040	9.040	0.047	0.047	0.778	96.108	8.786	0.00227	8.777	0.00228	0
0.001300	9.501	9.501	0.047	0.047	0.778	96.887	9.270	0.00162	9.260	0.00163	0
0.000661	14.000	14.000	0.190	0.190	3.113	100.000	11.751	0.00029	10.204	0.00085	0
TOTALS			6.090	6.090	100.0						
0.250000	0.020000										
0.177000	0.030000										
0.125000	0.120000										



PI+ 142 0 0.0 0 0.0 0

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 \*\*\* MULTIMODAL SAMPLE \*\*\*  
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WET WT	DPY WT	SALT	ORGANIC	MOISTURE	WEIGHT LOSS DUE TO HANDLING	0.0
1000.0000	5.8700	0.0	0.0	0.0 (GRAMS)	GRAVEL CORRECTION FACTOR	1.000
99.9999	100.0000	0.0	0.0	0.0 (PCT WET WT)	SIZES ELIMINATED (<0.01%)	NONE
					TRASK SORTING COEFFICIENT	1.952
					USING PROBABILITY EXTRAP.	1.942
					MEAN CUBED DEVIATION	15.290
					USING PROBABILITY EXTRAP.	10.572

PERCENTAGE COMPOSITION	TABLE OF STATISTICAL DATA IN PHI UNITS				PERCENTILES		LINEAR EXTRAP.		PROBABILITY EXTRAP.	
		MEAN	STD DEV	SKEWNESS	KURTOSIS	MM.	PHI UNITS	MM.	PHI UNITS	
GRAVEL 0.0	MCMENT	4.99812	2.02941	1.82941	6.55402	5.0	0.12008	3.05789	0.11536	3.11572
SAND 38.33	P-MCMENT	4.97679	1.87859	1.59464	5.29855	10.0	0.10916	3.19549	0.10274	3.28295
SILT 92.76	FOLK	4.76062	1.74673	0.40570	1.37532	16.0	0.09735	3.36062	0.09375	3.41510
CLAY 8.91	P-FOLK	4.77681	1.72233	0.42320	1.37320	25.0	0.08169	3.61370	0.08096	3.62668
MUD 61.67	INMAN	4.89146	1.53084	0.25641	1.11538	50.0	0.04423	4.49894	0.04422	4.49905
S/M 0.62	P-INMAN	4.61549	1.50059	0.27765	1.13763	75.0	0.02144	5.54368	0.02147	5.54138
	KRUMHFN		1.42962	0.07975	0.22042	84.0	0.01166	6.42230	0.01171	6.41628
	P-KRUM.		1.41830	0.08498	0.22328	90.0	0.00525	7.57343	0.00526	7.57065
	FOLK (TRANSFORMED)				0.57900	95.0	0.00135	9.53450	0.00135	9.53116
	P-FOLK (TRANSFORMED)				0.57863					

DATA FOR CONSTN OF BARGRAPHS AND CUM. CURVES

SIZE FRACTION	PHI	WT.(GMS)	WT.PCT.	WT.PCT.	MID PHI(LINEAR)	MID PHI(PROB.)	MODE
MM	PHI	UNCOR	COR	COR	PHI	PHI	MM
0.250000	2.000	0.020	0.020	0.341	0.341	1.751	0.29707
0.177000	2.498	0.010	0.010	0.170	0.511	2.249	0.21036
0.125000	3.000	0.140	0.140	2.385	2.896	2.749	0.14875
0.088000	3.506	1.080	1.080	16.399	21.295	3.253	0.10488
0.062500	4.000	1.000	1.000	17.036	38.331	3.753	0.07416
0.044000	4.506	0.695	0.695	11.842	50.173	4.253	0.05244
0.031000	5.012	0.835	0.835	14.224	64.397	4.759	0.03693
0.022000	5.506	0.597	0.597	10.172	74.569	5.259	0.02612
0.015600	6.002	0.336	0.336	5.722	80.291	5.754	0.01853
0.011000	6.506	0.261	0.261	4.451	84.742	6.254	0.01310
0.007800	7.002	0.149	0.149	2.543	87.284	6.754	0.00926
0.005500	7.506	0.149	0.149	2.543	89.828	7.254	0.00655
0.003900	8.002	0.075	0.075	1.272	91.100	7.754	0.00463
0.002700	8.533	0.112	0.112	1.907	93.007	8.268	0.00325
0.001900	9.040	0.075	0.075	1.271	94.278	8.786	0.00227
0.001380	9.561	0.037	0.037	0.636	94.914	9.270	0.00162
0.000980	9.995	0.075	0.075	1.272	96.186	9.748	0.00116
0.000690	10.501	0.037	0.037	0.635	96.821	10.248	0.00082
0.000061	14.000	0.187	0.187	3.179	100.000	12.251	0.00021
TOTALS		5.870	5.870	100.0			
0.250000	0.020000						

PI++ 143 0 0.0 0 0.0 0

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 \*\*\* MULTIMODAL SAMPLE \*\*\*  
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WET WT	DRY WT	SALT	ORGANIC	MOISTURE	WEIGHT LOSS DUE TO HANDLING	0.0
1000.0000	6.0600	0.0	0.0	0.0 (GRAMS)	GRAVEL CORRECTION FACTOR	1.000
99.9999	100.0000	0.0	0.0	0.0 (PCT WET WT)	SIZES ELIMINATED (<0.01%)	NONE
					TRASK SORTING COEFFICIENT	2.395
					USING PROBABILITY EXTRAP.	2.377
					MEAN CUBED DEVIATION	13.554
					USING PROBABILITY EXTRAP.	10.155

PERCENTAGE COMPOSITION		TABLE OF STATISTICAL DATA IN PHI UNITS				PERCENTILES		LINEAR EXTRAP.		PROBABILITY EXTRAP.	
		MEAN	STD DEV	SKEWNESS	KURTOSIS	MM.	PHI UNITS	MM.	PHI UNITS		
GRAVEL	0.0	MOMENT 5.10492	2.16715	1.33174	4.55280	5.0	0.14618	2.77417	0.13693	2.86852	
SAND	40.59	P-MOMENT 5.09098	2.05574	1.16887	3.75398	10.0	0.12148	3.04118	0.11979	3.06146	
SILT	48.48	FCLK 4.97285	2.01769	0.35725	1.12432	16.0	0.10903	3.19721	0.10547	3.24513	
CLAY	10.92	P-FCLK 4.98754	1.98886	0.37466	1.11678	25.0	0.09270	3.43124	0.09151	3.44964	
MUD	59.41	INMAN 5.13790	1.94700	0.25514	0.78093	50.0	0.04003	4.64275	0.04004	4.64223	
S/M	0.68	P-INMAN 5.16020	1.91507	0.27047	0.77715	75.0	0.01616	5.95098	0.01620	5.94778	
		KPUMBEIN 1.86647	0.04836	0.24104		84.0	0.00740	7.07860	0.00742	7.07527	
		P-KPUM. 1.85033	0.05658	0.24029		90.0	0.00324	8.26602	0.00326	8.25920	
		FCLK (TRANSFORMED)		0.52926		95.0	0.00121	9.68665	0.00122	9.67526	
		P-FCLK (TRANSFORMED)		0.52758							

DATA FOR CONSTN OF BARGRAPHS AND CUM. CURVES

SIZE FRACTION	WT.(GMS)	WT.PCT.	WT.PCT.	MID PHI(LINEAR)	MID PHI(PROB.)	MODE				
MM	PHI	UNCOR	COR	COR	CUMUL.	PHI	MM	PHI	MM	
0.250000	2.000	0.020	0.020	6.330	0.330	1.751	0.29707	1.894	0.26898	0
0.177000	2.448	0.030	0.030	0.495	0.825	2.249	0.21036	2.298	0.20332	0
0.125000	3.000	0.460	0.460	7.591	8.416	2.749	0.14875	2.850	0.13571	0
0.088000	3.506	1.180	1.180	19.472	27.888	3.253	0.10488	3.299	0.10157	1*
0.062500	4.000	0.770	0.770	12.706	40.594	3.753	0.07416	3.762	0.07371	0
0.044000	4.506	0.400	0.400	6.607	47.201	4.253	0.05244	4.255	0.05138	0
0.031000	5.012	0.620	0.620	10.366	57.567	4.759	0.03693	4.758	0.03696	0
0.022000	5.506	0.661	0.661	10.912	68.479	5.259	0.02612	5.253	0.02522	1
0.015600	6.002	0.441	0.441	7.274	75.752	5.754	0.01853	5.746	0.01863	0
0.011000	6.506	0.257	0.257	4.243	79.996	6.254	0.01310	6.247	0.01316	0
0.007800	7.002	0.220	0.220	3.637	83.633	6.754	0.00926	6.747	0.00931	0
0.005500	7.506	0.147	0.147	2.425	86.058	7.254	0.00695	7.248	0.00698	0
0.003900	8.002	0.184	0.184	3.031	89.089	7.754	0.00463	7.744	0.00467	1
0.002700	8.533	0.110	0.110	1.818	90.908	8.268	0.00325	8.259	0.00326	0
0.001900	9.040	0.110	0.110	1.818	92.726	8.786	0.00227	8.776	0.00228	1
0.001300	9.561	0.110	0.110	1.818	94.545	9.270	0.00162	9.258	0.00163	1
0.000980	9.955	0.073	0.073	1.212	95.757	9.748	0.00116	9.736	0.00117	0
0.000690	10.501	0.110	0.110	1.818	97.575	10.248	0.00082	10.219	0.00084	0
0.000061	14.000	0.147	0.147	2.425	100.000	12.251	0.00021	11.059	0.00047	0
TOTALS		6.060	6.060	100.0						
0.250000	C.030000									

PI+ 144 0 0.0 0 0.0 0

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 \*\*\* MULTIMODAL SAMPLE \*\*\*  
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WET WT	DRY WT	SALT	ORGANIC	MOISTURE	WEIGHT LOSS DUE TO HANDLING	0.0
1000.0000	4.3400	0.0	0.0	0.0 (GRAMS)	GRAVEL CORRECTION FACTOR	1.000
100.0000	100.0000	0.0	0.0	0.0 (PCT WET WT)	SIZES ELIMINATED (<0.01%)	NONE
					TRASK SORTING COEFFICIENT	2.783
					USING PROBABILITY EXTRAP.	2.745
					MEAN CUBED DEVIATION	10.808
					USING PROBABILITY EXTRAP.	9.226

PERCENTAGE COMPOSITION TABLE OF STATISTICAL DATA IN PHI UNITS PERCENTILES LINEAR EXTRAP. PROBABILITY EXTRAP.

	PERCENTAGE COMPOSITION	MOMENT	STATISTICAL DATA IN PHI UNITS				PERCENTILES		LINEAR EXTRAP.		PROBABILITY EXTRAP.	
			MEAN	STD. DEV.	SKEWNESS	KURTOSIS	MM.	PHI UNITS	MM.	PHI UNITS		
GRAVEL	0.0		5.00420	2.17114	1.05601	3.44012	5.0	0.15634	2.67723	0.14589	2.77705	
SAND	47.70	P-MOMENT	5.00754	2.10821	0.98461	3.03967	10.0	0.13170	2.92471	0.12862	2.95883	
SILT	40.55	FOLK	4.89243	2.09724	0.52159	0.94091	16.0	0.11642	3.10292	0.11395	3.13347	
CLAY	11.76	P-FOLK	4.90008	2.07148	0.53860	0.93911	25.0	0.10093	3.30854	0.09862	3.34154	
MUD	52.30	INMAN	5.24207	2.13955	0.49026	0.58474	50.0	0.05467	4.19313	0.05467	4.19302	
S/M	0.91	P-INMAN	5.25361	2.12014	0.50024	0.57426	75.0	0.01303	6.26229	0.01309	6.25517	
		KRUMHOLZ		2.18796	0.59229	0.27229	84.0	0.00600	7.38163	0.00603	7.37376	
		P-KRUMHOLZ		2.15791	0.60555	0.27083	90.0	0.00307	8.34861	0.00309	8.33710	
		FOLK (TRANSFORMED)				0.48478	95.0	0.00142	9.45849	0.00143	9.45236	
		P-FOLK (TRANSFORMED)				0.48430						

DATA FOR CONSTN OF BARGRAPHS AND CUM. CURVES

SIZE FRACTION	WT. (GMS)		WT. PCT.		MID PHI (LINEAR)		MID PHI (PROB.)		MODE	
	MM	PHI	UNCOR	COR	COR	CUMUL.	PHI	MM		
0.250000	2.000	0.030	0.030	0.691	0.691	1.751	0.29707	1.907	0.26662	0
0.177000	2.498	0.030	0.030	0.691	1.382	2.249	0.21036	2.286	0.20993	0
0.125000	3.000	0.440	0.440	10.138	11.521	2.749	0.14875	2.841	0.13961	0
0.088000	3.506	0.960	0.960	22.120	33.641	3.253	0.10488	3.291	0.10217	1*
0.062500	4.000	0.610	0.610	14.055	47.696	3.753	0.07416	3.759	0.07389	0
0.044000	4.506	0.262	0.262	6.040	53.736	4.253	0.05244	4.253	0.05245	0
0.031000	5.012	0.224	0.224	9.168	58.904	4.759	0.03693	4.758	0.03697	0
0.022000	5.506	0.324	0.324	7.471	66.376	5.259	0.02612	5.255	0.02619	1
0.015600	6.002	0.255	0.255	5.871	72.247	5.754	0.01853	5.749	0.01859	0
0.011000	6.506	0.232	0.232	5.338	77.584	6.254	0.01310	6.247	0.01316	0
0.007800	7.002	0.139	0.139	3.202	80.786	6.754	0.00926	6.749	0.00930	0
0.005500	7.506	0.185	0.185	4.271	85.057	7.254	0.00635	7.244	0.00660	1
0.003900	8.002	0.139	0.139	3.202	88.258	7.754	0.00463	7.744	0.00466	0
0.002700	8.533	0.116	0.116	2.668	90.926	8.268	0.00325	8.255	0.00327	0
0.001900	9.040	0.093	0.093	2.136	93.062	8.786	0.00227	8.773	0.00229	0
0.001380	9.561	0.093	0.093	2.135	95.197	9.270	0.00162	9.254	0.00164	0
0.000980	9.995	0.093	0.093	2.135	97.332	9.748	0.00116	9.719	0.00119	0
0.000690	10.501	0.069	0.069	1.600	98.932	10.248	0.00082	10.200	0.00085	0
0.000061	14.000	0.046	0.046	1.068	100.000	12.251	0.00021	11.114	0.00045	0
TOTALS										
0.250000	0.010000	4.340	4.340	100.0						

P1+ 145 0 0.0 0 0.0 0

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 \*\*\* MULTIMODAL SAMPLE \*\*\*  
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WET WT	DRY WT	SALT	ORGANIC	MOISTURE	WEIGHT LOSS DUE TO HANDLING	0.0
1000.0000	5.5000	0.0	0.0	0.0 (GRAMS)	GRAVEL CORRECTION FACTOR	1.000
100.0000	100.0000	0.0	0.0	0.0 (PCT WET WT)	SIZES ELIMINATED (<0.01%)	NONE
					TRASK SORTING COEFFICIENT	2.316
					USING PROBABILITY EXTRAP.	2.309
					MEAN CUBED DEVIATION	17.740
					USING PROBABILITY EXTRAP.	13.725

PERCENTAGE COMPOSITION		TABLE OF STATISTICAL DATA IN PHI UNITS				PERCENTILES		LINEAR EXTRAP.		PROBABILITY EXTRAP.	
		MEAN	STD DEV	SKEWNESS	KURTOSIS		MM.	PHI UNITS	MM.	PHI UNITS	
GRAVEL	0.0	5.20623	2.28454	1.48787	4.78651	5.0	0.12394	3.01228	0.12293	3.02411	
SAND	40.73	5.19140	2.16681	1.34911	4.09239	10.0	0.11285	3.14747	0.10765	3.21559	
SILT	46.30	5.02288	2.06127	0.45702	1.21977	16.0	0.10085	3.30970	0.09693	3.36690	
CLAY	12.97	5.04026	2.04218	0.46790	1.21455	25.0	0.08507	3.55519	0.08470	3.56155	
MUD	59.27	5.24717	1.93747	0.34729	0.86066	50.0	0.04198	4.57430	0.04199	4.57370	
S/M	0.69	5.27354	1.90664	0.36705	0.88459	75.0	0.01587	5.97796	0.01588	5.97660	
		KRUMBEIN	1.79465	0.19228	0.21290	84.0	0.00687	7.18464	0.00690	7.18018	
		P-KRUM.	1.78892	0.19537	0.21510	90.0	0.00219	8.83751	0.00220	8.82935	
		FOLK (TRANSFORMED)			0.54950	95.0	0.00084	10.22301	0.00084	10.21057	
		P-FOLK (TRANSFORMED)			0.54946						

DATA FOR CONSTN OF BARGRAPHS AND CUM. CURVES

SIZE FRACTION	WT.(GMS)		WT.PCT.		MID PHI(LINEAR)		MID PHI(PK08.)		MODE	
	MM	PHI	UNCOR	COR	PHI	MM	PHI	MM		
0.250000	2.000	0.010	0.010	0.182	0.182	1.751	0.29707	1.881	0.27157	0
0.177000	2.498	0.010	0.010	0.182	0.364	2.249	0.21036	2.287	0.20485	0
0.125000	3.000	0.230	0.230	4.182	4.545	2.749	0.14875	2.860	0.13174	0
0.098000	3.506	1.030	1.030	18.727	23.273	3.253	0.10468	3.319	0.10317	1*
0.062500	4.000	0.960	0.960	17.455	40.727	3.753	0.07416	3.768	0.07342	0
0.044000	4.506	0.426	0.426	7.739	48.466	4.253	0.05244	4.255	0.05238	0
0.031000	5.012	0.627	0.627	11.401	59.867	4.759	0.03693	4.757	0.03698	1
0.027000	5.506	0.509	0.509	9.262	69.129	5.259	0.02612	5.253	0.02522	0
0.015600	6.002	0.340	0.340	6.174	75.303	5.754	0.01853	5.748	0.01861	0
0.011000	6.506	0.272	0.272	4.940	80.243	6.254	0.01310	6.246	0.01317	0
0.007800	7.002	0.170	0.170	3.087	83.330	6.754	0.00926	6.748	0.00931	0
0.005500	7.506	0.102	0.102	1.852	85.182	7.254	0.00655	7.249	0.00657	0
0.003900	8.002	0.102	0.102	1.853	87.035	7.754	0.00463	7.749	0.00465	1
0.002700	8.533	0.102	0.102	1.852	88.886	8.268	0.00325	8.260	0.00326	0
0.001900	9.040	0.102	0.102	1.853	90.739	8.766	0.00227	8.778	0.00228	0
0.001300	9.501	0.136	0.136	2.409	93.208	9.270	0.00162	9.257	0.00163	1
0.000900	9.995	0.068	0.068	1.235	94.444	9.748	0.00116	9.738	0.00117	0
0.000690	10.501	0.068	0.068	1.235	95.678	10.248	0.00082	10.235	0.00083	0
0.000490	10.995	0.068	0.068	1.235	96.913	10.748	0.00058	10.731	0.00059	0
0.000061	14.000	0.170	0.170	3.087	100.000	12.497	0.00017	11.465	0.00035	0
TOTALS		5.500	5.500	100.0						

PITT 146 0 0.0 0 0.0 0

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 \*\*\* MULTIMODAL SAMPLE \*\*\*  
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WET WT	DRY WT	SALT	ORGANIC	MOISTURE	WEIGHT LOSS DUE TO HANDLING	0.0
1000.0000	5.7550	0.0	0.0	0.0 (GRAMS)	GRAVEL CORRECTION FACTOR	1.000
100.0000	100.0000	0.0	0.0	0.0 (PCT WET WT)	SIZES ELIMINATED (<0.01%)	NONE
					TRASK SORTING COEFFICIENT	2.154
					USING PROBABILITY EXTRAP.	2.134
					MEAN CUBED DEVIATION	16.966
					USING PROBABILITY EXTRAP.	12.464

PERCENTAGE COMPOSITION		TABLE OF STATISTICAL DATA IN PHI UNITS				PERCENTILES	LINEAR EXTRAP.	PROBABILITY EXTRAP.		
		MEAN	STD DEV	SKEWNESS	KURTOSIS		MM.	PHI UNITS	MM.	PHI UNITS
GRAVEL	0.0	5.32753	2.20175	1.58452	5.37505	5.0	0.11674	3.09860	0.11054	3.17740
SAND	33.71	5.30545	2.06618	1.41304	4.52068	10.0	0.10306	3.27848	0.09757	3.35737
SILT	54.79	5.13246	1.98459	0.39571	1.32555	16.0	0.08874	3.49433	0.08841	3.49959
CLAY	11.50	5.13281	1.96800	0.40402	1.32390	25.0	0.07419	3.75254	0.07259	3.77617
MUD	66.29	5.29403	1.79969	0.26932	0.98904	50.0	0.03566	4.80533	0.03566	4.80969
S/M	0.51	5.29437	1.79478	0.27005	0.96850	75.0	0.01600	5.96607	0.01602	5.96359
			1.63965	0.04998	0.21011	84.0	0.00732	7.09372	0.00734	7.08915
			1.62031	0.06019	0.21083	90.0	0.00268	8.54607	0.00268	8.54498
					0.56949	95.0	0.00082	10.25792	0.00082	10.24344
					0.56469					

DATA FOR CONSTN OF BARGRAPHS AND CUM. CURVES

SIZE FRACTION		WT. (GMS)		WT. PCT.		MID PHI (LINEAR)		MID PHI (PROB.)		MODE
MM	PHI	UNCOR	COR	COR	CUMUL.	PHI	MM	PHI	MM	
0.250000	2.000	0.010	0.010	0.174	0.174	1.751	0.29707	1.879	0.27180	0
0.177000	2.498	0.010	0.010	0.174	0.348	2.249	0.21036	2.287	0.20885	0
0.125000	3.000	0.110	0.110	1.911	2.259	2.749	0.14875	2.840	0.13968	0
0.088000	3.506	0.810	0.810	14.075	16.334	3.253	0.10488	3.337	0.09596	0
0.062500	4.000	1.000	1.000	17.376	33.710	3.753	0.07416	3.777	0.07296	1*
0.044000	4.506	0.528	0.528	9.182	42.891	4.253	0.05244	4.258	0.05228	0
0.021000	5.012	0.682	0.682	11.853	54.745	4.759	0.03693	4.760	0.03692	0
0.027000	5.506	0.744	0.744	12.931	67.675	5.259	0.02612	5.253	0.02622	1
0.015000	6.002	0.455	0.455	7.902	75.577	5.754	0.01853	5.746	0.01863	0
0.011000	6.506	0.289	0.289	5.028	80.605	6.254	0.01310	6.246	0.01518	0
0.007500	7.002	0.165	0.165	2.874	83.479	6.754	0.00926	6.748	0.00930	0
0.005500	7.506	0.165	0.165	2.873	86.352	7.254	0.00655	7.246	0.00659	0
0.003900	8.002	0.124	0.124	2.155	88.507	7.754	0.00463	7.747	0.00466	0
0.002700	8.533	0.083	0.083	1.437	89.944	8.268	0.00325	8.261	0.00326	0
0.001900	9.040	0.124	0.124	2.155	92.098	8.786	0.00227	8.775	0.00228	1
0.001380	9.501	0.083	0.083	1.437	93.535	9.270	0.00162	9.262	0.00163	0
0.000900	9.995	0.041	0.041	0.719	94.254	9.748	0.00116	9.742	0.00117	0
0.000690	10.501	0.083	0.083	1.436	95.690	10.248	0.00082	10.234	0.00083	1
0.000490	10.995	0.041	0.041	0.719	96.408	10.748	0.00058	10.739	0.00059	0
0.000061	14.000	0.207	0.207	3.592	100.000	12.497	0.00017	11.459	0.00036	0
TOTALS		5.755	5.755	100.0						



PI\*\* 147 0 0.0 0 0.0 0

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 \*\*\* MULTIMODAL SAMPLE \*\*\*  
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WET WT	DRY WT	SALT	ORGANIC	MOISTURE	WEIGHT LOSS DUE TO HANDLING	0.0
1000.0000	5.6300	0.0	0.0	0.0 (GRAMS)	GRAVEL CORRECTION FACTOR	1.000
100.0000	100.0000	0.0	0.0	0.0 (PCT WET WT)	SIZES ELIMINATED (<0.01)	NONE
					TRASK SORTING COEFFICIENT	1.843
					USING PROBABILITY EXTRAP.	1.834
					MEAN CUBED DEVIATION	12.172
					USING PROBABILITY EXTRAP.	6.762

PERCENTAGE COMPOSITION		TABLE OF STATISTICAL DATA IN PHI UNITS				PERCENTILES		LINEAR EXTRAP.		PROBABILITY EXTRAP.	
		MEAN	STD DEV	SKEWNESS	KURTOSIS	MM.	PHI UNITS	MM.	PHI UNITS		
GRAVEL	0.0	5.46444	1.91212	1.74112	6.55292	5.0	0.10131	3.30311	0.09595	3.38157	
SAND	19.89	5.41673	1.70805	1.35702	4.87894	10.0	0.08238	3.60149	0.08068	3.63162	
SILT	71.75	5.24436	1.67551	0.28160	1.44044	16.0	0.06968	3.84316	0.06820	3.87411	
CLAY	8.36	5.25066	1.65326	0.29613	1.43409	25.0	0.05291	4.24027	0.05238	4.25474	
MUD	80.11	5.31488	1.47172	0.14376	1.10694	50.0	0.02909	5.10331	0.02912	5.10159	
S/M	0.25	5.32520	1.45109	0.15409	1.10978	75.0	0.01557	6.03477	0.01558	6.00457	
			1.30704	0.01921	0.21662	84.0	0.00906	6.78660	0.00912	6.77628	
			1.29617	0.02806	0.21998	90.0	0.00490	7.67434	0.00493	7.66591	
					0.59024	95.0	0.00138	9.50477	0.00138	9.50452	
					0.58917						

DATA FOR CONSTN OF SARGRAPHS AND CUM. CURVES

SIZE FRACTION	PHI	WT.(GMS)	WT.PCT.	WT.PCT.	MID PHI(LINEAR)	MID PHI(PRG.)	MODE
MM	PHI	UNCOR	COR	COR	CUMUL.	PHI	MM
0.250000	2.000	0.010	0.010	0.178	0.178	1.751	0.29707
0.177000	2.498	0.010	0.010	0.178	0.355	2.249	0.21036
0.125000	3.000	0.040	0.040	0.710	1.066	2.749	0.14875
0.088000	3.506	0.370	0.370	6.572	7.638	3.253	0.10498
0.062500	4.000	0.690	0.690	12.256	19.893	3.753	0.07416
0.044000	4.506	0.606	0.606	10.761	30.655	4.253	0.05244
0.031000	5.012	0.897	0.897	19.941	46.546	4.759	0.03693
0.022000	5.506	1.034	1.034	18.358	64.954	5.259	0.02612
0.015600	6.002	0.564	0.564	10.013	74.967	5.754	0.01853
0.011000	6.506	0.376	0.376	6.675	81.642	6.254	0.01310
0.007000	7.002	0.235	0.235	4.172	85.814	6.754	0.00926
0.005500	7.506	0.188	0.188	3.337	69.152	7.254	0.00655
0.003900	8.002	0.141	0.141	2.504	91.655	7.754	0.00463
0.002700	8.523	0.094	0.094	1.669	93.324	8.268	0.00325
0.001900	9.040	0.047	0.047	0.835	94.159	8.766	0.00227
0.001380	9.561	0.047	0.047	0.835	94.994	9.270	0.00162
0.000980	9.995	0.047	0.047	0.834	95.828	9.748	0.00116
0.000661	14.000	0.235	0.235	4.172	100.000	11.997	0.00024
TOTALS		5.630	5.630	100.0			
0.250000	0.010000						
0.177000	0.010000						

PI++ 148 0 0.0 0 0.0 0

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 \*\*\* MULTIMODAL SAMPLE \*\*\*  
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WET WT	DRY WT	SALT	ORGANIC	MOISTURE	WEIGHT LOSS DUE TO HANDLING	0.0
100.0000	5.4700	0.0	0.0	0.0	GRAVEL CORRECTION FACTOR	1.000
100.0000	100.0000	0.0	0.0	0.0	SIZES ELIMINATED (<0.01%)	NONE
					TRASK SORTING COEFFICIENT	1.655
					USING PROBABILITY EXTRAP.	1.645
					MEAN CUBED DEVIATION	10.783
					USING PROBABILITY EXTRAP.	4.900

PERCENTAGE COMPOSITION	TABLE OF STATISTICAL DATA IN PHI UNITS				PERCENTILES	LINEAR EXTRAP.		PROBABILITY EXTRAP.	
	MEAN	STD DEV	SKWNESS	KURTOSIS		MM.	PHI UNITS	MM.	PHI UNITS
GRAVEL 0.0	MOMENT 5.03805	1.70734	2.16667	8.70359	5.0	0.10674	3.22784	0.10045	3.31549
SAND 25.46	P-MOMENT 4.98277	1.45327	1.59656	5.93573	10.0	0.08678	3.52641	0.08626	3.53519
SILT 68.63	FCLK 4.75833	1.32911	0.24844	1.42264	16.0	0.07671	3.70445	0.07460	3.74468
CLAY 5.41	P-FOLK 4.80992	1.30334	0.26977	1.41143	25.0	0.06375	3.97150	0.06345	3.97816
MUD 74.04	INMAN 4.83283	1.12838	0.09172	1.23706	50.0	0.03770	4.72534	0.03772	4.72867
S/M 0.35	P-INMAN 4.85054	1.10586	0.11020	1.23930	75.0	0.02326	5.42588	0.02342	5.41628
	KRUMBEIN 1.07732	-0.03064	0.22499	0.22499	84.0	0.01605	5.96121	0.01610	5.95640
	P-KRUM. 1.06527	-0.03145	0.22406	0.22406	90.0	0.00924	6.75849	0.00933	6.74447
	FOLK (TRANSFORMED) 0.58723			0.58723	95.0	0.00323	8.27635	0.00324	8.26821
	P-FOLK (TRANSFORMED) 0.58531			0.58531					

DATA FOR CONSTN OF BARGRAPHS AND CUM. CURVES

SIZE FRACTION MM	PHI	WT.(GMS)		WT.PCT.		MID PHI(LINEAR)		MID PHI(PROB.)		MODE
		UNCOR	CCR	COR	CUMUL.	PHI	MM	PHI	MM	
0.250000	2.000	0.010	0.010	0.183	0.183	1.751	0.29707	1.881	0.27154	0
0.177000	2.498	0.010	0.010	0.183	0.366	2.249	0.21036	2.287	0.20485	0
0.125000	3.000	0.060	0.060	1.097	1.463	2.749	0.14875	2.820	0.14158	0
0.088000	3.506	0.430	0.430	7.861	9.324	3.253	0.10438	3.337	0.09594	0
0.062500	4.000	0.910	0.910	16.636	25.960	3.753	0.07416	3.752	0.07217	1
0.044000	4.506	0.821	0.821	15.003	40.963	4.253	0.05244	4.265	0.05203	0
0.031000	5.012	1.120	1.120	20.475	61.438	4.759	0.03693	4.758	0.03696	1*
0.022000	5.506	0.886	0.886	16.196	77.633	5.259	0.02512	5.244	0.02539	0
0.015600	6.002	0.380	0.380	6.942	84.575	5.754	0.01893	5.740	0.01871	0
0.011000	6.506	0.211	0.211	3.856	88.431	6.254	0.01310	6.242	0.01321	0
0.007800	7.002	0.165	0.169	3.085	91.516	6.754	0.00926	6.740	0.00935	0
0.005500	7.506	0.084	0.084	1.542	93.058	7.254	0.00655	7.245	0.00659	0
0.003900	8.002	0.084	0.084	1.543	94.601	7.754	0.00463	7.742	0.00467	1
0.002700	8.533	0.042	0.042	0.771	95.373	8.268	0.00325	8.259	0.00326	0
0.001900	9.040	0.042	0.042	0.771	96.143	8.786	0.00227	8.777	0.00228	0
0.000001	14.000	0.211	0.211	3.856	100.000	11.520	0.00034	9.803	0.00112	0
TOTALS		5.470	5.470	100.0						
0.177000	0.010000									
0.125000	0.120000									
0.088000	0.550000									
0.062500	0.470000									

PI++ 149 0 0.0 0 0.0 0

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 \*\*\* MULTIMODAL SAMPLE \*\*\*  
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WET WT	OPY WT	SALT	ORGANIC	MOISTURE	WEIGHT LOSS DUE TO HANDLING	0.0
1000.0000	4.9900	0.0	0.0	0.0 (GRAMS)	GRAVEL CORRECTION FACTOR	1.000
100.0000	100.0000	0.0	0.0	0.0 (PCT WET WT)	SIZES ELIMINATED (<0.01%)	NONE
					TRASK SORTING COEFFICIENT	2.035
					USING PROBABILITY EXTRAP.	2.024
					MEAN CUBED DEVIATION	12.142
					USING PROBABILITY EXTRAP.	8.304

PERCENTAGE COMPOSITION	TABLE OF STATISTICAL DATA IN PHI UNITS					PERCENTILES		LINEAR EXTRAP.		PROBABILITY EXTRAP.	
		MEAN	STD DEV	SKEWNESS	KURTOSIS	MM.	PHI UNITS	MM.	PHI UNITS		
GRAVEL 0.0	MOMENT 5.51209	2.04103	1.42804	5.19853	5.0	0.11582	3.11000	0.11047	3.17820		
SAND 23.05	P-MOMENT 5.48541	1.90448	1.20210	4.17091	10.0	0.09877	3.33470	0.09500	3.39589		
SILT 65.95	FOLK 5.28287	1.89196	0.26506	1.35783	16.0	0.08073	3.63069	0.07981	3.64729		
CLAY 11.00	P-FOLK 5.28646	1.87502	0.27454	1.35322	25.0	0.05716	4.12673	0.05687	4.13606		
MUD 76.95	INMAN 5.35579	1.72510	0.12682	0.96920	50.0	0.02842	5.13702	0.02844	5.13567		
S/M 0.30	P-INMAN 5.36186	1.71457	0.13192	0.95881	75.0	0.01380	6.17942	0.01388	6.17039		
	KRUMMEIN 1.51903	0.01705	0.20515		84.0	0.00739	7.03090	0.00741	7.07643		
	P-KRUM. 1.50691	0.01755	0.20612		90.0	0.00309	8.33778	0.00311	8.33078		
	FOLK (TRANSFORMED) 0.57508				95.0	0.00104	9.90414	0.00105	9.89524		
	P-FOLK (TRANSFORMED) 0.57505										

DATA FOR CONSTN OF BARGRAPHS AND CUM. CURVES

SIZE FRACTION	WT.(GMS)	WT.PCT.	WT.PCT.	MID PHI(LINEAR)	MID PHI(PROB.)	MODE
MM	PHI	UNCOR	COR	CUMUL.	PHI	MM
0.177000	2.458	0.010	0.010	0.200	0.200	2.249
0.125000	3.000	0.120	0.120	2.405	2.605	2.749
0.080000	3.506	0.550	0.550	11.022	13.627	3.253
0.062500	4.000	0.470	0.470	9.419	23.046	3.753
0.044000	4.506	0.383	0.383	7.684	30.730	4.253
0.031000	5.012	0.753	0.753	15.088	45.819	4.759
0.022000	5.506	0.823	0.823	16.490	62.309	5.259
0.015600	6.002	0.509	0.509	10.207	72.516	5.754
0.011000	6.506	0.353	0.353	7.068	79.584	6.254
0.007800	7.002	0.196	0.196	3.926	82.510	6.754
0.005500	7.506	0.157	0.157	3.141	86.651	7.254
0.003900	8.002	0.118	0.118	2.356	89.007	7.754
0.002700	8.523	0.078	0.078	1.570	90.577	8.268
0.001900	9.040	0.078	0.078	1.570	92.147	8.786
0.001300	9.501	0.078	0.078	1.571	93.718	9.270
0.000900	9.995	0.078	0.078	1.570	95.289	9.748
0.000690	10.501	0.078	0.078	1.570	96.859	10.248
0.000001	14.000	0.157	0.157	3.141	100.000	12.291
TOTALS		4.990	4.990	100.0		
0.250000	0.010000					
0.177000	0.320000					

P1+150 0 0.0 0 0.0 0

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 \*\*\*\* MULTIMODAL SAMPLE \*\*\*\*  
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WET WT	DRY WT	SALT	ORGANIC	MOISTURE	WEIGHT LOSS DUE TO HANDLING	0.0
1000.0000	5.4700	0.0	0.0	0.0 (GRAMS)	GRAVEL CORRECTION FACTOR	1.000
100.0000	100.0000	0.0	0.0	0.0 (PCT WET WT)	SIZES ELIMINATED (<0.01%)	NONE
					TRASK SORTING COEFFICIENT	2.370
					USING PROBABILITY EXTRAP.	2.346
					MEAN CUBED DEVIATION	14.377
					USING PROBABILITY EXTRAP.	10.943

PERCENTAGE COMPOSITION	TABLE OF STATISTICAL DATA IN PHI UNITS				PERCENTILES		LINEAR EXTRAP.		PROBABILITY EXTRAP.	
		MEAN	STD DEV	SKEWNESS	KURTOSIS	MM.	PHI UNITS	MM.	PHI UNITS	
GRAVEL 0.0	MOMENT 5.44971	2.18289	1.38225	4.77423	5.0	0.11760	3.08006	0.11246	3.15245	
SAND 30.40	P-MOMENT 5.43285	2.07281	1.22872	4.05169	10.0	0.10273	3.28311	0.09782	3.35368	
SILT 57.57	FOLK 5.26484	2.02850	0.34035	1.18109	16.0	0.08745	3.51538	0.08732	3.51752	
CLAY 11.53	P-FOLK 5.26258	2.01373	0.34578	1.18190	25.0	0.07139	3.80817	0.07057	3.82897	
MUD 69.10	INMAN 5.39857	1.88319	0.21302	0.90463	50.0	0.03131	4.99740	0.03130	4.99760	
S/M 0.45	P-INMAN 5.39508	1.87756	0.21170	0.88934	75.0	0.01271	6.29739	0.01279	6.28912	
	KRUMPEIN	1.84387	0.05538	0.23585	84.0	0.00643	7.28176	0.00647	7.27264	
	P-KRUM.	1.82233	0.06145	0.23632	90.0	0.00265	8.56014	0.00265	8.55871	
	FCLK (TRANSFORMED)			0.54151	95.0	0.00081	10.26163	0.00082	10.24714	
	P-FOLK (TRANSFORMED)			0.54168						

DATA FOR CONSTN OF BARGRAPHS AND CUM. CURVES

SIZE FRACTION	WT.(GMS)		WT.PCT.		MID PHI(LINEAR)		MID PHI(PROB.)		MODE	
	MM	PHI	UNCOR	COR	PHI	MM	PHI	MM		
0.250000	2.000	0.010	0.010	0.183	0.183	1.751	0.29707	1.881	0.27154	0
0.177000	2.498	0.020	0.020	0.366	0.348	2.249	0.21036	2.308	0.20196	0
0.125000	3.000	0.120	0.120	2.194	2.742	2.749	0.14875	2.828	0.14078	0
0.088000	3.506	0.710	0.710	12.980	15.722	3.253	0.10488	3.329	0.09953	0
0.062500	4.000	0.830	0.830	15.174	30.896	3.753	0.07416	3.776	0.07299	1*
0.044000	4.506	0.416	0.416	7.599	38.495	4.253	0.05244	4.258	0.05225	0
0.031000	5.012	0.648	0.648	11.837	50.332	4.759	0.03693	4.762	0.03686	0
0.022000	5.506	0.709	0.709	12.957	63.289	5.259	0.02612	5.255	0.02518	1
0.015600	6.002	0.433	0.433	7.918	71.207	5.754	0.01853	5.748	0.01860	0
0.011000	6.506	0.354	0.354	6.479	77.686	6.254	0.01310	6.246	0.01318	0
0.007800	7.002	0.236	0.236	4.319	82.005	6.754	0.00926	6.746	0.00931	0
0.005500	7.506	0.197	0.197	3.599	85.603	7.254	0.00655	7.245	0.00659	0
0.003900	8.002	0.157	0.157	2.879	86.483	7.754	0.00463	7.745	0.00466	0
0.002700	8.533	0.079	0.079	1.440	89.922	8.268	0.00325	8.261	0.00326	0
0.001900	9.040	0.079	0.079	1.440	91.362	8.786	0.00227	8.779	0.00228	1
0.001300	9.501	0.079	0.079	1.440	92.802	9.270	0.00162	9.262	0.00163	1
0.000920	9.995	0.079	0.079	1.440	94.241	9.748	0.00116	9.737	0.00117	1
0.000690	10.501	0.079	0.079	1.440	95.681	10.248	0.00082	10.234	0.00083	0
0.000490	10.995	0.079	0.079	1.440	97.121	10.748	0.00058	10.728	0.00059	0
0.000061	14.000	0.157	0.157	2.879	100.000	12.497	0.00017	11.467	0.00035	0
TOTALS		5.470	5.470	100.0						

P1\*\* 151 0 0.0 0 0.0 0

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 \*\*\* MULTIMODAL SAMPLE \*\*\*  
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WET WT	DRY WT	SALT	ORGANIC	MOISTURE	WEIGHT LOSS DUE TO HANDLING	0.0
1000.0000	5.7600	0.0	0.0	0.0 (GRAMS)	GRAVEL CORRECTION FACTOR	1.000
100.0000	100.0000	0.0	0.0	0.0 (PCT WET WT)	SIZES ELIMINATED (<0.01%)	NONE
					TRASK SORTING COEFFICIENT	1.778
					USING PROBABILITY EXTRAP.	1.764
					MEAN CUBED DEVIATION	11.121
					USING PROBABILITY EXTRAP.	5.477

PERCENTAGE COMPOSITION	TABLE OF STATISTICAL DATA IN PHI UNITS				PERCENTILES		LINEAR EXTRAP.		PROBABILITY EXTRAP.	
		MEAN	STD DEV	SKEWNESS	KURTOSIS	MM.	PHI UNITS	MM.	PHI UNITS	
GRAVEL 0.0	MOMENT 5.43441	1.86476	1.71505	6.50260	5.0	0.09753	3.35805	0.09429	3.40670	
SAND 17.36	P-MOMENT 5.37723	1.63602	1.25075	4.58288	10.0	0.07869	3.66775	0.07645	3.70936	
SILT 74.02	FOLK 5.23949	1.57604	0.31919	1.42436	16.0	0.06522	3.93655	0.06454	3.95364	
CLAY 8.62	P-FOLK 5.24065	1.56139	0.32708	1.43004	25.0	0.05094	4.25507	0.05030	4.31334	
MUD 82.64	INMAN 5.34212	1.40357	0.21937	1.05549	50.0	0.03052	5.03422	0.03053	5.03359	
S/M 0.21	P-INMAN 5.34418	1.39054	0.22336	1.05545	75.0	0.01612	5.95532	0.01616	5.95160	
	KPUMBEIN 1.22981	0.09098	0.21103		84.0	0.00932	6.74570	0.00939	6.73472	
	P-KPUM. 1.21353	0.09888	0.21074		90.0	0.00515	7.60135	0.00517	7.55637	
	FOLK (TRANSFORMED) 0.58752		0.58752		95.0	0.00179	9.12611	0.00179	9.12307	
	P-FOLK (TRANSFORMED) 0.58848		0.58848							

DATA FOR CONSTN OF BARGRAPHS AND CUM. CURVES

SIZE FRACTION	WT.(GMS)		WT.PCT.		MID PHI(LINEAR)		MID PHI(PROB.)		MODE	
	MM	PHI	UNCOR	CCR	PHI	MM	PHI	MM		
0.250000	2.000	0.030	0.030	0.521	0.521	1.751	0.29707	1.903	0.26743	1
0.177000	2.496	0.020	0.020	0.347	0.868	2.249	0.21036	2.277	0.20034	0
0.125000	3.000	0.040	0.040	0.694	1.563	2.749	0.14875	2.781	0.14553	0
0.090000	3.506	0.280	0.280	4.861	6.424	3.253	0.10458	3.321	0.10305	0
0.062500	4.000	0.630	0.630	10.938	17.361	3.753	0.07416	3.795	0.07202	0
0.044000	4.506	0.755	0.755	13.108	30.469	4.253	0.05244	4.273	0.05174	0
0.031000	5.012	1.080	1.080	18.743	49.212	4.759	0.03693	4.767	0.03673	1*
0.022000	5.506	0.592	0.592	17.216	66.428	5.259	0.02612	5.255	0.02621	0
0.015600	6.002	0.545	0.545	9.469	75.897	5.754	0.01853	5.745	0.01865	0
0.011000	6.506	0.347	0.347	0.026	81.923	6.254	0.01310	6.244	0.01320	0
0.007800	7.002	0.248	0.248	4.304	86.227	6.754	0.00926	6.743	0.00933	0
0.005500	7.506	0.198	0.198	3.444	89.670	7.254	0.00655	7.242	0.00661	0
0.003900	8.002	0.099	0.099	1.721	91.392	7.754	0.00463	7.746	0.00466	0
0.002700	8.533	0.099	0.099	1.722	93.114	8.268	0.00325	8.256	0.00327	1
0.001900	9.040	0.099	0.099	1.721	94.835	8.786	0.00227	8.772	0.00229	0
0.001300	9.501	0.050	0.050	0.861	95.696	9.270	0.00162	9.262	0.00163	0
0.00061	14.000	0.248	0.248	4.304	100.000	11.751	0.00029	10.188	0.00086	0
TOTALS		5.760	5.760	100.0						

P1\*\* 152 0 0.0 0 0.0 0

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 \*\*\* MULTINODAL SAMPLE \*\*\*  
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WET WT	DPY WT	SALT	ORGANIC	MOISTURE	WEIGHT LOSS DUE TO HANDLING	0.0
1000.0000	5.5700	0.0	0.0	0.0 (GRAMS)	GRAVEL CORRECTION FACTOR	1.000
100.0000	100.0000	0.0	0.0	0.0 (PCT WET WT)	SIZES ELIMINATED (<0.01)	NONE
					TRASK SORTING COEFFICIENT	1.968
					USING PROBABILITY EXTRAP.	1.958
					MEAN CURED DEVIATION	11.302
					USING PROBABILITY EXTRAP.	7.097

PERCENTAGE COMPOSITION	TABLE OF STATISTICAL DATA IN PHI UNITS					PERCENTILES		LINEAR EXTRAP.		PROBABILITY EXTRAP.	
		MEAN	STD DEV	SKEWNESS	KURTOSIS	MM.	PHI UNITS	MM.	PHI UNITS		
GRAVEL 0.0	MOMENT 5.26645	1.94584	1.53409	5.76524	5.0	0.12524	2.99720	0.12509	2.99896		
SAND 26.21	P-MOMENT 5.23540	1.78898	1.23956	4.37945	10.0	0.10571	3.24181	0.10206	3.29244		
SILT 64.56	FOLK 5.02978	1.74802	0.24740	1.34007	16.0	0.08645	3.53201	0.08618	3.53652		
CLAY 9.23	P-FOLK 5.63944	1.74338	0.24638	1.34723	25.0	0.06495	3.94445	0.06465	3.95118		
MUD 73.79	INMAN 5.09250	1.56050	0.10136	1.04055	50.0	0.03270	4.93434	0.03268	4.93548		
S/M 0.36	P-INMAN 5.09142	1.55490	0.10029	1.05001	75.0	0.01677	5.89788	0.01685	5.89053		
	KRUMBEIN	1.44699	-0.01317	0.21657	84.0	0.00994	6.65300	0.00998	6.64633		
	P-KRUM.	1.43656	-0.01463	0.21779	90.0	0.00464	7.75168	0.00466	7.74470		
	FOLK (TRANSFORMED)			0.57266	95.0	0.00150	9.38446	0.00151	9.37410		
	P-FOLK (TRANSFORMED)			0.57397							

DATA FOR CONSTN OF BARGRAPHS AND CUM. CURVES

SIZE FRACTION	WT.(GMS)	WT.PCT.	WT.PCT.	MID PHI(LINEAR)	MID PHI(PROB.)	MODE				
MM	PHI	UNCOR	COR	COR	CUMUL.	PHI	MM	PHI	MM	
0.177000	2.498	0.010	0.010	0.180	0.180	2.249	0.21036	2.378	0.19233	0
0.125000	3.090	0.270	0.270	4.847	5.027	2.749	0.14875	2.881	0.13572	0
0.088000	3.506	0.580	0.580	10.413	15.440	3.253	0.10488	3.303	0.10131	0
0.062500	4.000	0.600	0.600	10.772	26.212	3.753	0.07416	3.772	0.07518	0
0.044000	4.506	0.601	0.601	10.789	37.001	4.253	0.05244	4.262	0.05210	0
0.031000	5.012	0.855	0.855	15.345	52.346	4.759	0.03693	4.762	0.03685	0
0.022000	5.506	0.856	0.856	15.373	67.718	5.259	0.02612	5.253	0.02623	1
0.015600	6.002	0.514	0.514	9.224	76.942	5.754	0.01853	5.744	0.01866	0
0.011000	6.506	0.342	0.342	6.149	83.091	6.254	0.01310	6.243	0.01321	0
0.007800	7.002	0.171	0.171	3.075	86.165	6.754	0.00926	6.746	0.00932	0
0.005500	7.506	0.171	0.171	3.075	89.240	7.254	0.00655	7.243	0.00660	0
0.003900	8.002	0.086	0.086	1.537	90.777	7.754	0.00463	7.747	0.00465	0
0.002700	8.533	0.086	0.086	1.538	92.314	8.268	0.00325	8.258	0.00327	1
0.001900	9.040	0.086	0.086	1.537	93.851	8.786	0.00227	8.775	0.00228	0
0.001380	9.501	0.086	0.086	1.538	95.389	9.270	0.00162	9.257	0.00163	1
0.000980	9.955	0.086	0.086	1.537	96.925	9.748	0.00116	9.728	0.00118	0
0.000061	14.000	0.171	0.171	3.075	100.000	11.997	0.00024	10.621	0.00063	0
TOTALS		5.570	5.570	100.0						

P1++ 153 0 0.0 0 0.0 0

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 \*\*\*\* MULTIMODAL SAMPLE \*\*\*\*  
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WET WT	DRY WT	SALT	ORGANIC	MOISTURE	WEIGHT LOSS DUE TO HANDLING	0.0
1000.0000	6.1000	0.0	0.0	0.0 (GRAMS)	GRAVEL CORRECTION FACTOR	1.000
99.9999	100.0000	0.0	0.0	0.0 (PCT WET WT)	SIZES ELIMINATED (<0.01%)	NONE
					TRASK SORTING COEFFICIENT	2.015
					USING PROBABILITY EXTRAP.	1.993
					MEAN CUBED DEVIATION	11.024
					USING PROBABILITY EXTRAP.	5.956

PERCENTAGE COMPOSITION				TABLE OF STATISTICAL DATA IN PHI UNITS				PERCENTILES		LINEAR EXTRAP.		PROBABILITY EXTRAP.	
		MEAN	STD DEV	SKEWNESS	KURTOSIS			MM.	PHI UNITS	MM.	PHI UNITS		
GRAVEL	0.0	5.13866	1.90420	1.59666	6.06504	5.0	0.11735	3.09113	0.11232	3.15430			
SAND	32.30	5.09649	1.70939	1.19241	4.24382	10.0	0.10174	3.29704	0.09717	3.36330			
SILT	60.02	4.57766	1.64163	0.29789	1.16576	16.0	0.05641	3.53266	0.08600	3.53945			
CLAY	7.69	4.97790	1.62580	0.30509	1.16774	25.0	0.07225	3.79077	0.07106	3.81488			
MUD	67.70	5.07290	1.54024	0.18551	0.86725	50.0	0.03622	4.78717	0.03621	4.78738			
S/M	0.48	5.07317	1.53372	0.18633	0.84812	75.0	0.01779	5.81295	0.01789	5.80450			
			1.49791	0.01469	0.24210	84.0	0.01022	6.61314	0.01026	6.60688			
			1.47379	0.02231	0.24226	90.0	0.00563	7.47341	0.00564	7.46976			
					0.53827	95.0	0.00218	8.64313	0.00221	8.82329			
					0.53869								

DATA FOR CONSTN OF BARGRAPHS AND CUM. CURVES

SIZE FRACTION	MM	PHI	WT.(GMS)		WT.PCT.		MID PHI(LINEAR)		MID PHI(PROB.)		MODE
			UNCOR	COR	COR	CUMUL.	PHI	MM	PHI	MM	
0.250000	2.000	0.040	0.040	0.656	0.656	1.751	0.29707	1.906	0.26076	1	
0.177000	2.498	0.020	0.020	0.328	0.984	2.249	0.21036	2.271	0.20717	0	
0.125000	3.000	0.110	0.110	1.803	2.787	2.749	0.14875	2.803	0.14333	0	
0.088000	3.506	0.750	0.750	12.295	15.082	3.253	0.10488	3.327	0.09966	0	
0.062500	4.000	1.050	1.050	17.213	32.295	3.753	0.07416	3.779	0.07285	1*	
0.044000	4.506	0.673	0.673	11.036	43.331	4.253	0.05244	4.259	0.05123	0	
0.031000	5.012	0.732	0.732	11.998	55.329	4.759	0.03693	4.759	0.03692	0	
0.022000	5.506	0.937	0.937	15.356	70.684	5.259	0.02612	5.250	0.02527	1	
0.015000	6.002	0.426	0.426	6.980	77.665	5.754	0.01853	5.746	0.01864	0	
0.011000	6.506	0.341	0.341	5.584	83.248	6.254	0.01310	6.243	0.01320	0	
0.007800	7.002	0.213	0.213	3.490	86.739	6.754	0.00926	6.745	0.00933	0	
0.005500	7.506	0.213	0.213	3.469	90.228	7.254	0.00655	7.241	0.00661	0	
0.003900	8.002	0.128	0.128	2.094	92.322	7.754	0.00463	7.743	0.00467	0	
0.002700	8.533	0.085	0.085	1.396	93.718	8.268	0.00325	8.257	0.00327	0	
0.001900	9.040	0.128	0.128	2.094	95.812	8.786	0.00227	8.766	0.00230	1	
0.001360	9.501	0.043	0.043	0.698	96.510	9.270	0.00162	9.262	0.00165	0	
0.00061	14.000	0.213	0.213	3.490	100.000	11.751	0.00029	10.198	0.00085	0	
TOTALS		6.100	6.100	100.0							

PI+ 154 0 0.0 0 0.0 0

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 MULTIMODAL SAMPLE  
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WET WT DRY WT SALT ORGANIC MOISTURE  
 1000.0000 5.7400 0.0 0.0 0.0 (GRAMS)  
 100.0000 100.0000 0.0 0.0 0.0 (PCT WET WT)

WEIGHT LOSS DUE TO HANDLING 0.0  
 GRAVEL CORRECTION FACTOR 1.000  
 SIZES ELIMINATED (<0.01%) NONE  
 TRASK SORTING COEFFICIENT 3.030  
 USING PROBABILITY EXTRAP. 2.952  
 MEAN CUBED DEVIATION 43.722  
 USING PROBABILITY EXTRAP. 34.586

PERCENTAGE COMPOSITION		TABLE OF STATISTICAL DATA IN PHI UNITS					PERCENTILES		LINEAR EXTRAP.		PROBABILITY EXTRAP.	
		MEAN	STD DEV	SKEWNESS	KURTOSIS			MM.	PHI UNITS	MM.	PHI UNITS	
GRAVEL	0.0	5.57607	3.21677	1.31351	3.49902	5.0		0.15790	2.66293	0.14778	2.75849	
SAND	47.74	5.52139	3.03305	1.23952	3.25897	10.0		0.13370	2.90297	0.12987	2.94480	
SILT	33.25	5.44258	3.05257	0.64995	1.33420	16.0		0.11763	3.08760	0.11541	3.11516	
CLAY	19.01	5.45127	2.93594	0.65216	1.25567	25.0		0.10254	3.23577	0.10010	3.32048	
MUD	52.26	6.03773	2.95013	0.60521	0.76459	50.0		0.05247	4.25228	0.05247	4.25228	
S/M	0.91	6.05078	2.93562	0.61265	0.65037	75.0		0.01117	6.48396	0.01118	6.48307	
			2.36503	0.63259	0.17330	84.0		0.00197	8.98786	0.00197	8.98640	
			2.34266	0.64950	0.17352	90.0		0.00022	12.13009	0.00023	12.05611	
					0.57159	95.0		0.00012	13.07446	0.00018	12.44619	
					0.55667							

DATA FOR CONSTN OF BARGRAPHS AND CUM. CURVES

SIZE FRACTION		WT.(GMS)		WT.PCT.		MID PHI(LINEAR)		MID PHI(PROB.)		MODE
MM	PHI	UNCOR	COR	COR	CUMUL.	PHI	MM	PHI	MM	
0.250000	2.000	0.050	0.050	0.871	0.871	1.751	0.29707	1.910	0.26003	1
0.177000	2.498	0.040	0.040	0.697	1.568	2.249	0.21036	2.280	0.20984	0
0.125000	3.000	0.600	0.600	10.453	12.021	2.749	0.14875	2.837	0.13993	0
0.098000	3.506	1.320	1.320	22.997	35.017	3.253	0.10488	3.290	0.10223	1
0.062500	4.000	0.730	0.730	12.718	47.735	3.753	0.07416	3.758	0.07494	0
0.044000	4.506	0.261	0.261	4.545	52.281	4.253	0.05244	4.253	0.05244	0
0.031000	5.012	0.345	0.345	6.013	58.294	4.754	0.03693	4.758	0.03697	0
0.022600	5.506	0.545	0.545	9.503	67.796	5.259	0.02612	5.254	0.02621	1
0.019600	6.002	0.182	0.182	3.168	70.964	5.754	0.01853	5.751	0.01856	0
0.011000	6.506	0.242	0.242	4.223	75.187	6.254	0.01310	6.249	0.01315	1
0.007800	7.002	0.121	0.121	2.112	77.299	6.754	0.00926	6.751	0.00928	0
0.005500	7.506	0.121	0.121	2.112	79.411	7.254	0.00655	7.251	0.00657	1
0.003900	8.002	0.091	0.091	1.584	80.995	7.754	0.00463	7.751	0.00464	0
0.002700	8.533	0.091	0.091	1.584	82.578	8.268	0.00325	8.264	0.00325	1
0.001900	9.040	0.091	0.091	1.584	84.162	8.786	0.00227	8.782	0.00227	1
0.001380	9.501	0.061	0.061	1.056	85.218	9.270	0.00162	9.268	0.00162	0
0.000980	9.995	0.061	0.061	1.056	86.274	9.748	0.00116	9.745	0.00117	0
0.000690	10.501	0.061	0.061	1.057	87.330	10.248	0.00082	10.244	0.00082	1
0.000490	10.995	0.061	0.061	1.056	88.386	10.748	0.00058	10.744	0.00058	0
0.000340	11.522	0.030	0.030	0.528	88.914	11.259	0.00041	11.256	0.00041	0
0.000240	12.025	0.030	0.030	0.528	89.442	11.773	0.00029	11.771	0.00029	1

0.000061 14.000 0.606 0.606 10.558 99.900 13.012 0.00012 12.319 0.00020 0  
 TOTALS 5.740 5.740 100.0



PI\*\* 155 0 0.0 0 0.0 0

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 MULTIMODAL SAMPLE  
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WET WT	DRY WT	SALT	ORGANIC	MOISTURE	WEIGHT LOSS DUE TO HANDLING	0.0
100.0000	5.6400	0.0	0.0	0.0 (GRAMS)	GRAVEL CORRECTION FACTOR	1.000
100.0000	100.0000	0.0	0.0	0.0 (PCT WET WT)	SIZES ELIMINATED (<0.01%)	NONE
					TRASK SORTING COEFFICIENT	2.027
					USING PROBABILITY EXTRAP.	2.020
					MEAN CUBED DEVIATION	23.820
					USING PROBABILITY EXTRAP.	19.565

PERCENTAGE COMPOSITION	TABLE OF STATISTICAL DATA IN PHI UNITS					PERCENTILES	LINEAR EXTRAP.		PROBABILITY EXTRAP.	
	MEAN	STD DEV	SKEWNESS	KURTOSIS	MM.		PHI UNITS	MM.	PHI UNITS	
GRAVEL 0.0	5.46484	2.42218	1.07616	5.53946	5.0	0.13401	2.89962	0.13001	2.94332	
SAND 26.60	5.44548	2.31465	1.57774	5.06670	10.0	0.10988	3.18592	0.10646	3.23163	
SILT 69.79	5.16888	2.25461	0.40149	1.75939	16.0	0.09044	3.46682	0.08980	3.47716	
CLAY 12.61	5.17060	2.24275	0.40552	1.75839	25.0	0.06610	3.91920	0.06573	3.92724	
MUD 73.40	5.32406	1.85723	0.25066	1.35608	50.0	0.03447	4.85853	0.03442	4.86048	
S/M 3.36	5.32566	1.84849	0.25165	1.35384	75.0	0.01609	5.95781	0.01611	5.95548	
	FRUMBEIN	1.51008	0.07998	0.17788	84.0	0.00689	7.18129	0.00692	7.17415	
	P-KRUM.	1.50240	0.08088	0.17855	90.0	0.00207	8.91634	0.00208	8.91136	
	FOLK (TRANSFORMED)			0.63760	95.0	0.00031	11.65119	0.00031	11.64542	
	P-FOLK (TRANSFORMED)			0.63747						

DATA FOR CONSTN OF BARGRAPHS AND CUM. CURVES

SIZE FRACTION MM	PHI	WT.(GMS) UNCOR	WT.(GMS) COR	WT.PCT. COR	WT.PCT. CUMUL.	MID PHI(LINEAR) PHI	MID PHI(Prob.) MM	MODE		
0.177000	2.498	0.050	0.050	0.887	0.887	2.249	0.21030	2.409	0.18933	0
0.125000	3.000	0.290	0.290	5.142	6.028	2.749	0.14875	2.838	0.13990	0
0.082000	3.506	0.610	0.610	10.816	16.844	3.253	0.10488	3.298	0.10165	1
0.062500	4.000	0.550	0.550	9.752	26.596	3.753	0.07416	3.769	0.07533	0
0.044000	4.506	0.508	0.508	9.011	35.606	4.253	0.05244	4.261	0.05215	0
0.031000	5.012	1.165	1.165	20.648	56.254	4.759	0.03693	4.762	0.03684	1*
0.022000	5.506	0.753	0.753	13.346	69.600	5.259	0.02612	5.252	0.02525	0
0.015000	6.002	0.335	0.335	5.932	75.532	5.754	0.01853	5.748	0.01661	0
0.011000	6.506	0.251	0.251	4.449	79.981	6.254	0.01310	6.247	0.01117	0
0.007800	7.002	0.167	0.167	2.966	82.947	6.754	0.00926	6.748	0.00930	0
0.005500	7.506	0.167	0.167	2.965	85.912	7.254	0.00655	7.246	0.00559	0
0.003900	8.002	0.084	0.084	1.483	87.395	7.754	0.00463	7.750	0.00465	0
0.002700	8.533	0.084	0.084	1.483	88.879	8.268	0.00325	8.262	0.00326	0
0.001900	9.040	0.084	0.084	1.482	90.361	8.786	0.00227	8.780	0.00228	0
0.001380	9.561	0.084	0.084	1.483	91.844	9.270	0.00162	9.263	0.00163	1
0.000980	9.995	0.042	0.042	0.741	92.585	9.748	0.00116	9.744	0.00117	0
0.000690	10.501	0.042	0.042	0.742	93.327	10.248	0.00082	10.243	0.00083	1
0.000490	10.955	0.042	0.042	0.741	94.068	10.748	0.00058	10.742	0.00058	0
0.000340	11.522	0.042	0.042	0.741	94.809	11.259	0.00041	11.252	0.00041	0
0.000240	12.025	0.042	0.042	0.742	95.551	11.773	0.00029	11.766	0.00029	0
0.000061	14.000	0.251	0.251	4.449	100.000	13.012	0.00012	12.326	0.00019	0

TOTALS 5.640 5.640 100.0

P1\*\* 156 0 0.0 0 0.0 0

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 \*\*\* MULTIMODAL SAMPLE \*\*\*  
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WET WT	DRY WT	SALT	ORGANIC	MOISTURE	WEIGHT LOSS DUE TO HANDLING	0.0
1000.0000	6.2200	0.0	0.0	0.0 (GRAMS)	GRAVEL CORRECTION FACTOR	1.000
100.0000	100.0000	0.0	0.0	0.0 (PCT WET WT)	SIZES ELIMINATED (<0.018)	NGNE
					TRASK SORTING COEFFICIENT	2.187
					USING PROBABILITY EXTRAP.	2.183
					MEAN CUBED DEVIATION	13.772
					USING PROBABILITY EXTRAP.	11.320

PERCENTAGE COMPOSITION TABLE OF STATISTICAL DATA IN PHI UNITS PERCENTILES LINEAR EXTRAP. PROBABILITY EXTRAP.

		MEAN	STD DEV	SKEWNESS	KURTOSIS		MM.	PHI UNITS	MM.	PHI UNITS
GRAVEL	0.0	4.87330	2.08486	1.51969	5.41443	5.0	0.15388	2.70015	0.14726	2.76359
SAND	45.02	4.66579	2.00543	1.40357	4.72923	10.0	0.12259	3.02803	0.12136	3.04264
SILT	46.47	4.67855	1.88953	0.44497	1.24212	16.0	0.11084	3.17339	0.10730	3.22020
CLAY	8.51	4.69289	1.86666	0.46103	1.24821	25.0	0.09530	3.36143	0.09355	3.41809
MUD	54.98	4.67820	1.70480	0.35132	1.30758	50.0	0.05150	4.27526	0.05150	4.27537
S/M	0.82	4.69964	1.67944	0.36933	1.01788	75.0	0.01992	5.64996	0.02000	5.64551
			1.67298	0.24144	0.24302	84.0	0.01043	6.56300	0.01046	6.57908
			1.64846	0.25143	0.24071	90.0	0.00489	7.67474	0.00493	7.66531
					0.55399	95.0	0.00134	9.54521	0.00134	9.54139
					0.55520					

DATA FOR CONSTN OF BARGRAPHS AND CUM. CURVES

SIZE FRACTION	WT.(GNS)	WT.PCT.	WT.PCT.	MID PHI(LINEAR)	MID PHI(Prob.)	MODE
MM	PHI	UNCOR	COR	CUMUL.	PHI	MM
0.250000	2.000	0.090	0.090	1.447	1.447	1
0.177000	2.49E	0.060	0.060	0.965	2.412	0
0.125000	3.000	0.400	0.400	6.431	8.842	0
0.082000	3.506	1.300	1.300	20.900	29.743	1
0.062500	4.000	0.950	0.950	15.273	45.016	0
0.044000	4.506	0.562	0.562	9.036	54.052	0
0.031000	5.012	0.531	0.531	8.536	62.588	0
0.022000	5.506	0.670	0.670	10.770	73.359	1
0.015000	6.002	0.353	0.353	5.668	79.027	0
0.011000	6.506	0.282	0.282	4.535	83.562	0
0.007800	7.002	0.176	0.176	2.834	86.396	0
0.005500	7.506	0.176	0.176	2.834	89.230	1
0.003900	8.002	0.141	0.141	2.268	91.498	0
0.002700	8.503	0.070	0.070	1.133	92.631	0
0.001500	9.004	0.106	0.106	1.700	94.331	1
0.001380	9.501	0.035	0.035	0.568	94.899	0
0.000980	9.995	0.070	0.070	1.133	96.032	1
0.000690	10.501	0.070	0.070	1.133	97.166	0
0.000490	10.995	0.071	0.071	1.134	98.300	0
0.000061	14.000	0.106	0.106	1.700	100.000	0
TOTALS		6.220	6.220	100.0		

PI+ 157 0 0.0 0 0.0 0

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 MULTIMODAL SAMPLE  
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WET WT	DRY WT	SALT	ORGANIC	MOISTURE	WEIGHT LOSS DUE TO HANDLING	0.0
1000.0000	6.1400	0.0	0.0	0.0 (GRAMS)	GRAVEL CORRECTION FACTOR	1.000
100.0000	100.0000	0.0	0.0	0.0 (PCT WET WT)	SIZES ELIMINATED (<0.01%)	NONE
					TRASK SORTING COEFFICIENT	2.126
					USING PROBABILITY EXTRAP.	2.108
					MEAN CUBED DEVIATION	8.923
					USING PROBABILITY EXTRAP.	6.388

PERCENTAGE COMPOSITION		TABLE OF STATISTICAL DATA IN PHI UNITS					PERCENTILES		LINEAR EXTRAP.		PROBABILITY EXTRAP.	
		MEAN	STD DEV	SKEWNESS	KURTOSIS		MM.	PHI UNITS	MM.	PHI UNITS		
GRAVEL	0.0	4.34413	1.80627	1.51416	5.84721	5.0	0.17600	2.50637	0.17511	2.51367		
SAND	56.03	4.33869	1.70746	1.28327	4.42558	10.0	0.15882	2.65490	0.15190	2.71883		
SILT	39.03	4.18926	1.61348	0.47229	1.03073	16.0	0.14041	2.83226	0.13575	2.88096		
CLAY	4.94	4.26466	1.59920	0.48400	1.04055	25.0	0.11842	3.07803	0.11745	3.08952		
MUD	43.97	4.40098	1.56872	0.40489	0.74416	50.0	0.07351	3.76582	0.07351	3.76592		
S/M	1.27	4.42403	1.54307	0.42649	0.77003	75.0	0.02621	5.25388	0.02644	5.24133		
			1.61174	0.40014	0.26690	84.0	0.01596	5.96970	0.01599	5.96711		
			1.59372	0.39965	0.26897	90.0	0.00942	6.73067	0.00950	6.71846		
					0.50757	95.0	0.00396	7.97856	0.00357	7.97626		
					0.50944							

DATA FOR CONSTN OF BARGRAPHS AND CUM. CURVES

SIZE FRACTION	WT.(GMS)		WT.PCT.		MID PHI(LINEAR)		MID PHI(PROB.)		MODE	
	MM	PHI	UNCOR	COR	PHI	MM	PHI	MM		
0.250000	2.000	0.120	0.120	1.954	1.954	1.751	0.29707	1.919	0.26446	0
0.177000	2.498	0.170	0.170	2.769	4.723	2.249	0.21036	2.293	0.20403	0
0.125000	3.000	1.040	1.040	16.938	21.661	2.749	0.14875	2.812	0.14244	0
0.080000	3.506	1.330	1.330	21.661	43.323	3.253	0.10488	3.271	0.10358	1
0.062500	4.000	0.780	0.780	12.704	56.026	3.753	0.07416	3.753	0.07415	0
0.044000	4.506	0.450	0.450	7.336	63.362	4.253	0.05244	4.250	0.05255	0
0.031000	5.012	0.431	0.431	7.024	70.385	4.759	0.03693	4.754	0.03707	0
0.022000	5.506	0.579	0.579	9.423	79.808	5.259	0.02612	5.246	0.02534	1
0.015600	6.002	0.276	0.276	4.467	84.295	5.754	0.01853	5.745	0.01865	0
0.011000	6.506	0.275	0.275	4.487	88.782	6.254	0.01310	6.240	0.01323	0
0.007800	7.002	0.165	0.165	2.653	91.475	6.754	0.00926	6.742	0.00934	0
0.005500	7.506	0.138	0.138	2.243	93.718	7.254	0.00655	7.240	0.00662	0
0.003900	8.002	0.083	0.083	1.346	95.064	7.754	0.00463	7.743	0.00467	0
0.002700	8.533	0.083	0.083	1.346	96.410	8.268	0.00325	8.251	0.00328	1
0.001900	9.040	0.083	0.083	1.346	97.757	8.786	0.00227	8.762	0.00230	0
0.001380	9.501	0.055	0.055	0.897	98.654	9.270	0.00162	9.246	0.00165	0
0.000661	14.000	0.083	0.083	1.346	100.000	11.751	0.00029	10.266	0.00081	0
TOTALS		6.140	6.140	100.0						
0.250000	0.030000									
0.177000	0.030000									
0.125000	0.400000									

P1+ 158 0 C.0 0 0.0 0

WET WT	DRY WT	SALT	ORGANIC	MOISTURE		WEIGHT LOSS DUE TO HANDLING	0.0
1000.0000	6.1500	0.0	0.0	0.0	(GRAMS)	GRAVEL CORRECTION FACTOR	1.000
100.0000	100.0000	0.0	0.0	0.0	(PCT WET WT)	SIZES ELIMINATED (<0.01%)	NONE
						TRASK SORTING COEFFICIENT	1.750
						USING PROBABILITY EXTRAP.	1.738
						MEAN CUBED DEVIATION	10.778
						USING PROBABILITY EXTRAP.	5.998

PERCENTAGE COMPOSITION		TABLE OF STATISTICAL DATA IN PHI UNITS				PERCENTILES		LINEAR EXTRAP.		PROBABILITY EXTRAP.	
		MEAN	STD DEV	SKEWNESS	KURTOSIS		MM.	PHI UNITS	MM.	PHI UNITS	
GRAVEL	0.0	4.46896	1.69660	2.20701	9.01030	5.0	0.14273	2.80867	0.13531	2.86562	
SAND	51.22	4.44097	1.50717	1.75197	6.31393	10.0	0.12017	3.05686	0.11758	3.08828	
SILT	43.64	4.22197	1.37490	0.44155	1.32762	16.0	0.10940	3.19225	0.10531	3.24729	
CLAY	5.14	4.24047	1.34652	0.46822	1.33162	25.0	0.09504	3.35534	0.09314	3.42450	
MUD	48.78	4.34709	1.15484	0.52504	1.27882	50.0	0.06374	3.97172	0.06368	3.97290	
S/M	1.05	4.37426	1.12697	0.35614	1.29874	75.0	0.03082	5.02014	0.03084	5.01915	
			1.20355	0.23602	0.25387	84.0	0.02207	5.50193	0.02208	5.50123	
			1.18122	0.24892	0.25258	90.0	0.01308	6.25685	0.01318	6.24500	
					0.57038	95.0	0.00372	8.07201	0.00373	8.06685	
					0.57111						

DATA FOR CONSTN OF BARGRAPHS AND CUM. CURVES

SIZE FRACTION	WT.(GMS)	WT.PCT.	WT.PCT.	MID PHI(LINEAR)	MID PHI(Prob.)	MODE
MM	PHI	UNCOR	COR	PHI	MM	
0.250000	2.000	0.030	0.030	0.488	0.488	0
0.177000	2.498	0.030	0.030	0.488	0.976	0
0.125000	3.000	0.400	0.400	6.504	7.480	0
0.088000	3.506	1.380	1.380	22.439	29.919	0
0.062500	4.000	1.310	1.310	21.301	51.220	1*
0.044000	4.506	0.784	0.784	12.743	63.963	0
0.031000	5.012	0.669	0.669	10.877	74.840	0
0.022000	5.506	0.568	0.568	9.242	84.082	0
0.015600	6.002	0.284	0.284	4.621	88.703	0
0.011000	6.506	0.158	0.158	2.567	91.271	0
0.007800	7.002	0.126	0.126	2.054	93.224	0
0.005500	7.506	0.063	0.063	1.028	94.552	0
0.003900	8.002	0.032	0.032	0.513	94.865	0
0.002700	8.533	0.063	0.063	1.027	95.892	0
0.001900	9.040	0.095	0.095	1.541	97.433	0
0.00061	14.000	0.158	0.158	2.567	100.000	0
TOTALS		6.150	6.150	100.0	11.520	0.00034
0.250000	0.030000					5.827
0.177000	0.030000					0.00110
0.125000	1.730000					
0.088000	2.170000					

PI# 159 0 0.0 0 0.0 0

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 \*\*\* MULTIMODAL SAMPLE \*\*\*  
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WET WT	DPY WT	SALT	ORGANIC	MOISTURE	WEIGHT LOSS DUE TO HANDLING	0.0
1000.0000	6.5100	0.0	0.0	0.0 (GRAMS)	GRAVEL CORRECTION FACTOR	1.000
100.0000	100.0000	0.0	0.0	0.0 (PCT WET WT)	SIZES ELIMINATED (<0.01%)	NONE
					TRASK SORTING COEFFICIENT	1.504
					USING PROBABILITY EXTRAP.	1.487
					MEAN CUBED DEVIATION	8.791
					USING PROBABILITY EXTRAP.	5.486

PERCENTAGE COMPOSITION		TABLE OF STATISTICAL DATA IN PHI UNITS				PERCENTILES		LINEAR EXTRAP.		PROBABILITY EXTRAP.	
		MEAN	STD DEV	SKWNESS	KURTOSIS	MM.	PHI UNITS	MM.	PHI UNITS		
GRAVEL	0.0	3.81337	1.47543	2.73693	12.71195	5.0	0.16780	2.57518	0.15376	2.70128	
SAND	73.27	3.81987	1.33264	2.31810	9.15342	10.0	0.15717	2.66960	0.14310	2.80493	
SILT	24.45	3.86023	1.14048	0.54370	1.42959	16.0	0.14530	2.78290	0.13520	2.86684	
CLAY	2.28	3.09246	1.09073	0.60231	1.42148	25.0	0.12915	2.55285	0.12691	2.97813	
MUD	26.73	3.81943	1.03653	0.46077	0.98095	50.0	0.09863	3.34183	0.09829	3.34686	
S/M	2.74	3.86527	0.97843	0.52984	1.02679	75.0	0.05711	4.13014	0.05740	4.12276	
		KPUMBEIN	0.87207	0.19966	0.21223	84.0	0.03453	4.85596	0.03485	4.84369	
		P-KFUM.	0.84787	0.20358	0.21767	90.0	0.02298	5.44320	0.02313	5.43426	
		FOLK (TRANSFORMED)			0.58841	95.0	0.00974	6.68180	0.00981	6.67133	
		P-FOLK (TRANSFORMED)			0.58703						

DATA FOR CONSTN OF BARGRAPHS AND CUM. CURVES

SIZE FRACTION	WT.(GMS)	WT.PCT.	WT.PCT.	MID PHI(LINEAR)	MID PHI(PROB.)	MODE				
MM	PHI	UNCOR	COR	COR	CUMUL.	PHI	MM	PHI	MM	
0.250000	2.000	0.030	0.030	0.461	0.461	1.751	0.25707	1.901	0.26781	1
0.177000	2.498	0.030	0.030	0.461	0.922	2.249	0.21036	2.287	0.20497	0
0.125000	3.000	1.730	1.730	26.575	27.496	2.749	0.14875	2.865	0.13726	0
0.088000	3.506	2.170	2.170	33.333	60.830	3.253	0.10488	3.262	0.10427	1
0.062500	4.000	0.810	0.810	12.442	73.272	3.753	0.07416	3.744	0.07465	0
0.044000	4.506	0.438	0.438	6.723	79.995	4.253	0.05244	4.243	0.05201	0
0.031000	5.012	0.377	0.377	5.788	85.783	4.759	0.03693	4.745	0.03729	0
0.022000	5.566	0.315	0.315	4.834	90.617	5.259	0.02612	5.241	0.02545	0
0.015600	6.002	0.167	0.167	2.559	93.176	5.754	0.01853	5.739	0.01870	0
0.011000	6.566	0.093	0.093	1.422	94.598	6.254	0.01310	6.243	0.01320	0
0.007800	7.002	0.074	0.074	1.137	95.735	6.754	0.00926	6.743	0.00934	0
0.005500	7.566	0.074	0.074	1.137	96.872	7.254	0.00659	7.238	0.00662	1
0.003900	8.002	0.055	0.055	0.853	97.725	7.754	0.00463	7.738	0.00468	0
0.002700	8.533	0.037	0.037	0.569	98.294	8.268	0.00325	8.251	0.00328	0
0.001900	9.040	0.019	0.019	0.284	98.578	8.786	0.00227	8.776	0.00228	0
0.000001	14.000	0.093	0.093	1.422	100.000	11.520	0.00034	9.877	0.00106	0
TOTALS		6.510	6.510	100.0						
0.250000	0.010000									
0.177000	0.020000									
0.125000	0.040000									
0.088000	0.220000									

P1+ 160 0 0.0 0 0.0 0

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 MULTIMODAL SAMPLE  
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WET WT	DPY WT	SALT	ORGANIC	MOISTURE	WEIGHT LOSS DUE TO HANDLING	0.0
1000.0000	4.6900	0.0	0.0	0.0 (GRAMS)	GRAVEL CORRECTION FACTOR	1.000
100.0000	100.0000	0.0	0.0	0.0 (PCT WET WT)	SIZES ELIMINATED (<0.01)	NONE
					TRASK SORTING COEFFICIENT	1.921
					USING PROBABILITY EXTRAP.	1.913
					MEAN CURED DEVIATION	5.198
					USING PROBABILITY EXTRAP.	3.117

PERCENTAGE COMPOSITION		TABLE OF STATISTICAL DATA IN PHI UNITS					PERCENTILES		LINEAR EXTRAP.		PROBABILITY EXTRAP.	
		MEAN	STD DEV	SKEWNESS	KURTOSIS			MM.	PHI UNITS	MM.	PHI UNITS	
GRAVEL	0.0	5.64269	1.09771	1.06232	4.65365	5.0	0.09615	3.37860	0.09329	3.42204		
SAND	14.50	5.62261	1.59289	0.77105	3.36558	10.0	0.07521	3.73291	0.07326	3.77091		
SILT	75.02	5.54653	1.62107	0.26070	1.20444	16.0	0.05840	4.05775	0.05794	4.10928		
CLAY	10.48	5.54612	1.60540	0.26483	1.19893	25.0	0.04167	4.58494	0.04138	4.59495		
MUD	85.50	5.66181	1.56405	0.22111	0.77029	50.0	0.02510	5.31598	0.02509	5.31678		
S/M	0.17	5.66079	1.55151	0.22172	0.76462	75.0	0.01129	6.46924	0.01131	6.46674		
		KRUMPEIN	1.39578	0.21111	0.21705	84.0	0.00668	7.22586	0.00674	7.21230		
		P-KRUM.	1.38649	0.21408	0.21794	90.0	0.00371	8.07359	0.00373	8.06507		
		FOLK (TRANSFORMED)			0.54637	95.0	0.00207	8.91625	0.00210	8.89765		
		P-FOLK (TRANSFORMED)			0.54523							

DATA FOR CONSTN OF BARGRAPHS AND CUM. CURVES

SIZE FRACTION	WT.(GMS)	WT.PCT.	WT.PCT.	MID PHI(LINEAR)	MID PHI(Prob.)	MODE
MM	PHI	UNCOR	COR	PHI	MM	MM
0.250000	2.000	0.010	0.010	0.213	0.213	1.751
0.177000	2.498	0.020	0.020	0.426	0.640	2.249
0.125000	3.000	0.040	0.040	0.853	1.493	2.749
0.080000	3.506	0.220	0.220	4.891	6.183	3.253
0.062500	4.000	0.390	0.390	8.316	14.499	3.753
0.044000	4.506	0.365	0.365	7.774	22.273	4.253
0.031000	5.012	0.822	0.822	17.528	39.801	4.759
0.022000	5.506	0.777	0.777	16.577	56.377	5.259
0.015600	6.002	0.536	0.536	11.426	67.804	5.754
0.011000	6.500	0.364	0.364	7.768	75.571	6.254
0.007800	7.002	0.286	0.286	6.107	81.678	6.754
0.005500	7.506	0.245	0.245	5.255	86.913	7.254
0.003900	8.002	0.123	0.123	2.618	89.531	7.754
0.002700	8.533	0.164	0.164	3.489	93.020	8.268
0.001900	9.040	0.123	0.123	2.617	95.638	8.786
0.001360	9.501	0.123	0.123	2.617	98.255	9.270
0.000661	14.000	0.082	0.082	1.745	100.000	11.751
TOTALS		4.690	4.690	100.0		
0.250000	0.340000					
0.177000	0.020000					
0.125000	0.660900					

P1\*\* 161 0 0.0 0 0.0 0

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 \*\*\* MULTIMODAL SAMPLE \*\*\*  
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WET WT	DRY WT	SALT	ORGANIC	MOISTURE	WEIGHT LOSS DUE TO HANDLING	0.0
1000.0000	4.5300	0.0	0.0	0.0 (GRAMS)	GRAVEL CORRECTION FACTOR	1.000
100.0000	100.0000	0.0	0.0	0.0 (PCT WET WT)	SIZES ELIMINATED (<0.01%)	NONE
					TRASK SORTING COEFFICIENT	1.981
					USING PROBABILITY EXTRAP.	1.984
					MEAN CUBED DEVIATION	7.409
					USING PROBABILITY EXTRAP.	3.205

PERCENTAGE COMPOSITION		TABLE OF STATISTICAL DATA IN PHI UNITS				PERCENTILES		LINEAR EXTRAP.		PROBABILITY EXTRAP.	
		MEAN	STD DEV	SKWENESS	KURTOSIS	MM.	PHI UNITS	MM.	PHI UNITS		
GRAVEL	0.0	5.44229	1.79035	1.29109	5.47933	5.0	0.10826	3.20739	0.10400	3.26445	
SAND	19.43	5.35263	1.59692	0.76686	3.53277	10.0	0.08371	3.57841	0.08248	3.59975	
SILT	72.25	5.29670	1.57300	0.22001	1.10615	16.0	0.06950	3.84676	0.06821	3.87382	
CLAY	8.32	5.20254	1.55546	0.23168	1.10833	25.0	0.05157	4.27729	0.05107	4.29128	
MUD	80.57	5.37980	1.53304	0.16262	0.73601	50.0	0.02855	5.13049	0.02857	5.12910	
S/M	0.24	5.58926	1.51544	0.17168	0.73715	75.0	0.01314	6.24941	0.01325	6.23818	
		KRUMHEIN	1.46083	0.13286	0.23640	84.0	0.00830	6.91284	0.00835	6.90470	
		P-KRUM.	1.44215	0.13563	0.23544	90.0	0.00465	7.74952	0.00470	7.73436	
		FGLK (TRANSFORMED)			0.52520	95.0	0.00270	8.53015	0.00271	8.52953	
		P-FGLK (TRANSFORMED)			0.52569						

DATA FOR CONSTN OF BARGRAPHS AND CUM. CURVES

SIZE FRACTION	WT. (GMS)		WT. PCT.		MID PHI (LINEAR)		MID PHI (PROB.)		MODE	
	MM	PHI	UNCOR	COR	COR	CUMUL.	PHI	MM		
0.250000	2.000	0.040	0.040	0.883	0.883	1.751	0.29707	1.911	0.26000	1
0.177000	2.498	0.020	0.020	0.442	1.325	2.249	0.21036	2.271	0.20720	0
0.125000	3.000	0.060	0.060	1.325	2.649	2.749	0.14875	2.785	0.14305	0
0.088000	3.506	0.260	0.260	5.740	8.389	3.293	0.10488	3.309	0.10393	0
0.062500	4.000	0.500	0.500	11.038	19.426	3.753	0.07416	3.788	0.07240	1
0.044000	4.506	0.461	0.461	10.178	29.604	4.253	0.05244	4.267	0.05192	0
0.031000	5.012	0.743	0.743	16.403	46.007	4.759	0.03693	4.768	0.03671	0
0.022000	5.506	0.753	0.753	16.614	62.620	5.259	0.02612	5.256	0.02517	1*
0.015600	6.002	0.376	0.376	8.307	70.927	5.754	0.01853	5.748	0.01861	0
0.011000	6.506	0.376	0.376	8.307	79.234	6.254	0.01310	6.243	0.01320	1
0.007000	7.002	0.263	0.263	5.815	85.049	6.754	0.00926	6.742	0.00935	0
0.005500	7.506	0.150	0.150	3.322	88.371	7.254	0.00655	7.243	0.00660	0
0.003900	8.002	0.150	0.150	3.322	91.693	7.754	0.00463	7.739	0.00468	0
0.002700	8.533	0.151	0.151	3.323	95.017	8.268	0.00325	8.242	0.00330	1
0.001900	9.040	0.075	0.075	1.661	96.678	8.786	0.00227	8.766	0.00230	0
0.000001	14.000	0.150	0.150	3.322	100.000	11.520	0.00354	9.811	0.00311	0
TOTALS		4.530	4.530	100.0						
0.250000	0.040000									
0.177000	0.040000									
0.125000	1.470000									
0.088000	2.360000									





P1\*\* 163 0 0.0 0 0.0 0

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 MULTIMODAL SAMPLE  
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WET WT DRY WT SALT ORGANIC MOISTURE  
 1000.0000 6.5600 0.0 0.0 0.0 (GRAMS)  
 99.9999 100.0000 0.0 0.0 0.0 (PCT WET WT)

WEIGHT LOSS DUE TO HANDLING 0.0  
 GRAVEL CORRECTION FACTOR 1.000  
 SIZES ELIMINATED (<0.01%) NONE  
 TRASK SORTING COEFFICIENT 2.016  
 USING PROBABILITY EXTRAP. 2.015  
 MEAN CUBED DEVIATION 12.881  
 USING PROBABILITY EXTRAP. 9.079

PERCENTAGE COMPOSITION TABLE OF STATISTICAL DATA IN PHI UNITS PERCENTILES LINEAR EXTRAP. PROBABILITY EXTRAP.

PERCENTAGE COMPOSITION		TABLE OF STATISTICAL DATA IN PHI UNITS				PERCENTILES		LINEAR EXTRAP.		PROBABILITY EXTRAP.	
		MEAN	STD DEV	SKEWNESS	KURTOSIS	MM.	PHI UNITS	MM.	PHI UNITS		
GRAVEL	0.0	4.23774	1.87659	1.94917	7.45318	5.0	0.17006	2.55591	0.16208	2.62520	
SAND	63.11	4.23330	1.75045	1.69277	5.79397	10.0	0.15727	2.66865	0.14692	2.76693	
SILT	31.84	4.02134	1.56895	0.59923	1.10744	16.0	0.14320	2.83393	0.13594	2.87892	
CLAY	5.05	4.04235	1.53020	0.62432	1.09428	25.0	0.12449	3.00594	0.12440	3.00695	
MUD	36.89	4.28479	1.48086	0.53372	0.84631	50.0	0.08873	3.49442	0.08363	3.45527	
SYM	1.71	4.31589	1.43697	0.57108	0.87788	75.0	0.03061	5.02962	0.03064	5.02824	
			1.49902	0.52336	0.25676	84.0	0.01838	5.76565	0.01854	5.75287	
			1.49725	0.52233	0.26351	90.0	0.01024	6.60951	0.01029	6.60226	
					0.52251	95.0	0.00384	8.02416	0.00385	8.02212	

DATA FOR CONSTN OF BARGRAPHS AND CUM. CURVES

SIZE FRACTION	WT.(GMS)	WT.PCT.	WT.PCT.	MID PHI(LINEAR)	MID PHI(PROB.)	PCDE
MM	PHI	UNCOR	COR	PHI	MM	MM
0.250000	2.000	0.050	0.050	0.762	0.762	1.751
0.177000	2.498	0.110	0.110	1.677	2.439	2.249
0.125000	3.000	1.460	1.460	22.256	24.695	2.749
0.088000	3.506	1.700	1.700	25.915	50.610	3.253
0.062500	4.000	0.820	0.820	12.500	63.110	3.753
0.044000	4.506	0.254	0.254	3.869	66.979	4.253
0.021000	5.012	0.510	0.510	7.780	74.759	4.759
0.022000	5.500	0.433	0.433	6.601	81.361	5.259
0.015600	6.002	0.331	0.331	5.048	86.409	5.754
0.011000	6.506	0.204	0.204	3.107	89.515	6.254
0.007800	7.002	0.153	0.153	2.330	91.845	6.754
0.005500	7.506	0.127	0.127	1.941	93.787	7.254
0.003900	8.002	0.076	0.076	1.165	94.952	7.754
0.002700	8.533	0.076	0.076	1.165	96.117	8.254
0.001900	9.040	0.051	0.051	0.777	96.893	8.786
0.001300	9.501	0.051	0.051	0.777	97.670	9.270
0.000900	9.995	0.025	0.025	0.389	98.059	9.748
0.000061	14.000	0.127	0.127	1.941	100.000	11.997
TOTALS		6.560	6.560	100.0		
0.250000	0.030000					
0.177000	0.030000					

PI\*\* 164 0 0.0 0 0.0 0

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 \*\*\*\* MULTIMODAL SAMPLE \*\*\*\*  
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WET WT	DRY WT	SALT	ORGANIC	MOISTURE	WEIGHT LOSS DUE TO HANDLING	0.0
1000.0000	6.2730	0.0	0.0	0.0 (GRAMS)	GRAVEL CORRECTION FACTOR	1.000
100.0000	100.0000	0.0	0.0	0.0 (PCT WET WT)	SIZES ELIMINATED (<0.01%)	NONE
					TRASK SORTING COEFFICIENT	1.875
					USING PROBABILITY EXTRAP.	1.859
					MEAN CUBED DEVIATION	12.299
					USING PROBABILITY EXTRAP.	7.157

PERCENTAGE COMPOSITION		TABLE OF STATISTICAL DATA IN PHI UNITS					PERCENTILES		LINEAR EXTRAP.		PROBABILITY EXTRAP.	
		MEAN	STD DEV	SKWNESS	KURTOSIS		MM.	PHI UNITS	MM.	PHI UNITS		
GRAVEL	0.0	4.70128	1.84726	1.95120	7.98669	5.0	0.14486	2.78728	0.13656	2.87236		
SAND	42.74	4.66852	1.66081	1.56224	5.51932	10.0	0.12033	3.05495	0.11818	3.08099		
SILT	51.22	4.47437	1.53345	0.33852	1.28100	16.0	0.10749	3.21776	0.10390	3.26667		
CLAY	6.03	4.48833	1.50556	0.35934	1.27743	25.0	0.09075	3.46198	0.09002	3.47361		
MUD	57.26	4.56740	1.34964	0.20679	1.09941	50.0	0.05118	4.28831	0.05117	4.28861		
S/M	0.75	4.58820	1.32153	0.22670	1.10954	75.0	0.02583	5.27503	0.02605	5.26243		
			1.34300	0.08019	0.24174	84.0	0.01655	5.91705	0.01663	5.90972		
			1.32505	0.07941	0.24085	90.0	0.00894	6.80492	0.00901	6.79456		
					0.56159	95.0	0.00285	8.45420	0.00286	8.44799		
					0.56091							

DATA FOR CONSTN OF BARGRAPHS AND CUM. CURVES

SIZE FRACTION	WT. (GMS)		WT. PCT.		MID PHI (LINEAR)		MID PHI (PROB.)		MODE	
	MM	PHI	UNCOR	CCP	CCR	CUMUL.	PHI	MM		
0.250000	2.000	0.030	0.030	0.478	0.478	1.751	0.29707	1.901	0.26765	0
0.177000	2.498	0.030	0.030	0.478	0.957	2.249	0.21036	2.286	0.20497	0
0.125000	3.000	0.440	0.440	7.018	7.974	2.749	0.14875	2.843	0.13934	0
0.088000	3.506	1.170	1.170	18.660	26.635	3.253	0.10488	3.300	0.10150	1*
0.062500	4.000	1.010	1.010	16.108	42.743	3.753	0.07416	3.764	0.07361	0
0.044000	4.506	0.799	0.799	12.744	55.487	4.253	0.05244	4.254	0.05242	0
0.031000	5.012	0.902	0.902	14.378	69.865	4.759	0.03643	4.751	0.03714	1
0.022000	5.506	0.605	0.605	9.643	79.508	5.259	0.02612	5.246	0.02534	0
0.015600	6.002	0.340	0.340	5.424	84.932	5.754	0.01853	5.742	0.01868	0
0.011000	6.506	0.227	0.227	3.616	88.549	6.254	0.01310	6.242	0.01321	0
0.007800	7.002	0.151	0.151	2.411	90.959	6.754	0.00926	6.744	0.00933	0
0.005500	7.506	0.113	0.113	1.809	92.768	7.254	0.00655	7.244	0.00660	0
0.003900	8.002	0.076	0.076	1.205	93.973	7.754	0.00463	7.746	0.00466	0
0.002700	8.533	0.076	0.076	1.206	95.179	8.268	0.00325	8.256	0.00327	1
0.001900	9.040	0.038	0.038	0.602	95.781	8.766	0.00227	8.779	0.00228	0
0.001380	9.501	0.076	0.076	1.206	96.986	9.270	0.00162	9.255	0.00164	0
0.00061	14.000	0.189	0.189	3.014	100.000	11.751	0.00029	10.206	0.00085	0
TOTALS		6.270	6.270	100.0						
0.250000	0.060000									
0.177000	0.130000									
0.125000	1.120000									

PI+ 165 0 0.0 0 0.0 0

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 \*\*\* MULTIMODAL SAMPLE \*\*\*  
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WET WT	OPY WT	SALT	ORGANIC	MOISTURE	WEIGHT LOSS DUE TO HANDLING	0.0
1000.0000	5.8500	0.0	0.0	0.0 (GRAMS)	GRAVEL CORRECTION FACTOR	1.000
100.0000	100.0000	0.0	0.0	0.0 (PCT WET WT)	SIZES ELIMINATED (<0.01%)	NONE
					TRASK SORTING COEFFICIENT	1.907
					USING PROBABILITY EXTRAP.	1.898
					MEAN CUBED DEVIATION	8.782
					USING PROBABILITY EXTRAP.	5.639

PERCENTAGE COMPOSITION		TABLE OF STATISTICAL DATA IN PHI UNITS				PERCENTILES		LINEAR EXTRAP.		PROBABILITY EXTRAP.	
		MEAN	STD DEV	SKEWNESS	KURTOSIS	MM.	PHI UNITS	MM.	PHI UNITS		
GRAVEL	0.0	4.14152	1.66488	1.90298	7.73452	5.0	0.17145	2.54409	0.16599	2.59086	
SAND	62.91	4.13388	1.53808	1.54970	5.39615	10.0	0.15657	2.67515	0.14776	2.75864	
SILT	33.65	3.97067	1.40557	0.51545	1.06776	16.0	0.14040	2.83241	0.13479	2.89123	
CLAY	3.45	3.98474	1.38173	0.33937	1.06271	25.0	0.12065	3.05112	0.11991	3.05991	
MUD	37.09	4.17270	1.34028	0.45221	0.81076	50.0	0.08440	3.56661	0.08445	3.56568	
S/M	1.70	4.20177	1.31053	0.48536	0.82928	75.0	0.03317	4.91417	0.03328	4.90898	
			1.38003	0.41604	0.26095	84.0	0.02190	5.51293	0.02191	5.51230	
			1.26969	0.41876	0.26626	90.0	0.01319	6.24487	0.01332	6.23089	
					0.51638	95.0	0.00593	7.39794	0.00598	7.38552	
					0.51520						

DATA FOR CONSTN OF BARGRAPHS AND CUM. CURVES

SIZE FRACTION	WT.(GMS)	WT.PCT.	WT.PCT.	MID PHI(LINEAR)	MID PHI(Prob.)	MODE
MM	PHI	UNCOR	COR	PHI	MM	PHI
0.250000	2.000	0.060	0.060	1.026	1.026	1.751
0.177000	2.498	0.130	0.130	2.222	3.248	2.249
0.125000	3.000	1.120	1.120	19.145	22.393	2.749
0.088000	3.506	1.510	1.510	25.812	48.205	3.253
0.062500	4.000	0.860	0.860	14.701	62.906	3.753
0.044000	4.506	0.391	0.391	6.690	69.596	4.253
0.031000	5.012	0.392	0.392	6.695	76.251	4.759
0.022000	5.506	0.447	0.447	7.648	83.938	5.259
0.015600	6.002	0.268	0.268	4.589	88.527	5.754
0.011000	6.506	0.179	0.179	3.060	91.587	6.254
0.007800	7.002	0.112	0.112	1.912	93.499	6.754
0.005500	7.506	0.112	0.112	1.912	95.411	7.254
0.002900	8.002	0.067	0.067	1.147	96.558	7.754
0.002700	8.533	0.067	0.067	1.147	97.705	8.268
0.001900	9.040	0.045	0.045	0.765	98.470	8.786
0.00061	14.000	0.089	0.089	1.530	100.000	11.520
TOTALS		5.850	5.850	100.0		
0.250000	0.030000					
0.177000	0.070000					
0.125000	0.900000					
0.088000	1.470000					

PI++ 166 0 0.0 0 0.0 0

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 \*\*\* MULTIMODAL SAMPLE \*\*\*  
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WET WT	DRY WT	SALT	ORGANIC	MOISTURE	WEIGHT LOSS DUE TO HANDLING	0.0
1000.0000	6.7700	0.0	0.0	0.0 (GRAMS)	GRAVEL CORRECTION FACTOR	1.000
99.9999	100.0000	0.0	0.0	0.0 (PCT WET WT)	SIZES ELIMINATED (<0.01*)	NCNE
					TRASK SORTING COEFFICIENT	2.442
					USING PROBABILITY EXTRAP.	2.411
					MEAN CURVED DEVIATION	25.499
					USING PROBABILITY EXTRAP.	21.496

PERCENTAGE COMPOSITION TABLE OF STATISTICAL DATA IN PHI UNITS PERCENTILES LINEAR EXTRAP. PROBABILITY EXTRAP.

		MEAN	STD DEV	SKEWNESS	KURTOSIS		MM.	PHI UNITS	MM.	PHI UNITS
GRAVEL	0.0	4.98936	2.50767	1.61701	5.22733	5.0	0.16141	2.63115	0.15029	2.73415
SAND	49.78	4.78315	2.41172	1.53244	4.77880	10.0	0.14162	2.81989	0.13439	2.89550
SILT	38.43	4.67698	2.19946	0.57616	1.27119	16.0	0.12254	3.02864	0.12180	3.03745
CLAY	11.80	4.67654	2.18082	0.58851	1.27215	25.0	0.10595	3.23852	0.10376	3.26865
MUD	50.22	5.00629	1.97764	0.49955	1.02013	50.0	0.06171	4.01835	0.06171	4.01829
S/M	0.99	5.01017	1.97272	0.50280	0.99812	75.0	0.01777	5.81459	0.01784	5.80838
			1.90820	0.50820	0.22069	84.0	0.00790	6.98393	0.00791	6.98289
			1.88128	0.52022	0.22057	90.0	0.00248	8.65824	0.00248	8.65269
					0.55970	95.0	0.00063	10.62136	0.00064	10.61759
					0.55989					

DATA FOR CONSTN OF BARGRAPHS AND CUM. CURVES

SIZE FRACTION	WT.(GMS)		WT.PCT.		MID PHI(LINEAR)		MID PHI(PROB.)		MODE	
MM	PHI	UNCOR	COR	COR	CUMUL.	PHI	MM	PHI	MM	
0.250000	2.000	0.030	0.030	0.443	0.443	1.751	0.29707	1.900	0.26794	0
0.177000	2.458	0.070	0.070	1.034	1.477	2.249	0.21036	2.311	0.20147	0
0.125000	3.000	0.900	0.900	13.294	14.771	2.749	0.14875	2.844	0.13924	0
0.088000	3.506	1.470	1.470	21.713	36.484	3.253	0.10488	3.283	0.10275	1
0.062500	4.000	0.900	0.900	13.294	49.778	3.753	0.07416	3.757	0.07398	0
0.044000	4.506	0.413	0.413	6.107	55.886	4.253	0.05244	4.252	0.05247	0
0.031000	5.012	0.419	0.419	6.192	62.078	4.759	0.03693	4.757	0.03699	0
0.022000	5.506	0.659	0.659	9.737	71.815	5.259	0.02612	5.252	0.02525	1
0.015600	6.002	0.347	0.347	5.125	76.939	5.754	0.01853	5.748	0.01861	0
0.011000	6.506	0.278	0.278	4.100	81.039	6.254	0.01310	6.247	0.01317	0
0.007800	7.002	0.208	0.208	3.075	84.114	6.754	0.00926	6.747	0.00931	0
0.005500	7.506	0.139	0.139	2.049	86.163	7.254	0.00655	7.248	0.00658	0
0.003900	8.002	0.139	0.139	2.050	88.213	7.754	0.00463	7.747	0.00465	1
0.002700	8.533	0.104	0.104	1.537	89.750	8.268	0.00325	8.261	0.00326	0
0.001900	9.040	0.069	0.069	1.025	90.775	8.786	0.00227	8.781	0.00227	1
0.001380	9.501	0.104	0.104	1.538	92.313	9.270	0.00162	9.263	0.00163	1
0.000980	9.995	0.104	0.104	1.537	93.850	9.748	0.00116	9.737	0.00117	0
0.000690	10.501	0.069	0.069	1.025	94.875	10.248	0.00082	10.239	0.00083	0
0.000490	10.995	0.035	0.035	0.513	95.388	10.748	0.00058	10.743	0.00058	0
0.000340	11.522	0.035	0.035	0.513	95.900	11.259	0.00041	11.252	0.00041	0
0.000240	12.025	0.035	0.035	0.513	96.413	11.773	0.00029	11.767	0.00029	1

0.000061 14.000 0.243 0.243 3.587 100.000 13.012 0.00012 12.330 0.00019 0  
 TOTALS 6.770 6.770 100.0

PI++ 167 0 0.0 0 0.0 0

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 \*\*\* MULTIMODAL SAMPLE \*\*\*  
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WET WT	DPY WT	SALT	ORGANIC	MOISTURE	WEIGHT LOSS DUE TO HANDLING	0.0
1000.0000	6.1100	0.0	0.0	0.0 (GRAMS)	GRAVEL CORRECTION FACTOR	1.000
100.0000	100.0000	0.0	0.0	0.0 (PCT WET WT)	SIZES ELIMINATED (<0.01%)	NONE
					TRASK SORTING COEFFICIENT	1.710
					USING PROBABILITY EXTRAP.	1.689
					MEAN CUBED DEVIATION	8.819
					USING PROBABILITY EXTRAP.	6.608

PERCENTAGE COMPOSITION		TABLE OF STATISTICAL DATA IN PHI UNITS					PERCENTILES		LINEAR EXTRAP.		PROBABILITY EXTRAP.	
		MEAN	STD DEV	SKEWNESS	KURTOSIS		MM.	PHI UNITS	MM.	PHI UNITS		
GRAVEL	0.0	4.86212	1.68540	1.84179	7.19225	5.0	0.11875	3.07402	0.11441	3.12776		
SAND	32.24	4.85513	1.59327	1.63340	5.80864	10.0	0.10368	3.26983	0.09884	3.35971		
SILT	60.84	4.64672	1.46327	0.33542	1.49699	16.0	0.09809	3.50480	0.08806	3.50540		
CLAY	6.92	4.64483	1.45134	0.34101	1.51448	25.0	0.07283	3.77954	0.07170	3.80179		
MUD	67.76	4.71817	1.21337	0.17665	1.32964	50.0	0.04408	4.50383	0.04407	4.50391		
S/M	0.48	4.71529	1.20989	0.17471	1.30857	75.0	0.02491	5.32710	0.02515	5.31349		
			1.14649	0.04939	0.21168	84.0	0.01638	5.93155	0.01646	5.92517		
			1.11978	0.05373	0.21099	90.0	0.00822	6.92575	0.00825	6.92102		
					0.59952	95.0	0.00236	8.72747	0.00238	8.71399		
					0.60230							

DATA FOR CONSTN OF BARGRAPHS AND CUM. CURVES

SIZE FRACTION	WT.(GMS)		WT.PCT.		MID PHI(LINEAR)		MID PHI(PROB.)		MODE	
	MM	PHI	UNCOR	COR	COR	CUMUL.	PHI	MM		
0.250000	2.000	0.020	0.020	0.327	0.327	1.751	0.29707	1.894	0.26901	0
0.177000	2.498	0.020	0.020	0.327	0.655	2.249	0.21036	2.287	0.20492	0
0.125000	3.000	0.150	0.150	2.455	3.110	2.749	0.14875	2.826	0.14103	0
0.088000	3.506	0.790	0.790	12.930	16.039	3.253	0.10488	3.324	0.09583	0
0.062500	4.000	0.990	0.990	16.203	32.242	3.753	0.07416	3.776	0.07297	0
0.044000	4.506	1.090	1.090	17.846	50.088	4.253	0.05244	4.260	0.05220	1*
0.031000	5.012	1.064	1.064	17.416	67.504	4.759	0.03693	4.753	0.03710	0
0.222000	5.506	0.718	0.718	11.754	79.258	5.259	0.02612	5.245	0.02637	0
0.015600	6.002	0.338	0.338	5.531	84.789	5.754	0.01893	5.742	0.01868	0
0.011000	6.506	0.211	0.211	3.457	88.246	6.254	0.01310	6.243	0.01320	0
0.007800	7.002	0.127	0.127	2.074	90.320	6.754	0.00926	6.746	0.00932	0
0.005500	7.506	0.085	0.085	1.383	91.703	7.254	0.00655	7.247	0.00658	0
0.003500	8.002	0.085	0.085	1.383	93.086	7.754	0.00463	7.746	0.00466	1
0.002700	8.533	0.085	0.085	1.383	94.469	8.268	0.00325	8.256	0.00327	1
0.001900	9.040	0.085	0.085	1.383	95.852	8.786	0.00227	8.772	0.00229	1
0.001380	9.501	0.084	0.084	1.382	97.234	9.270	0.00162	9.251	0.00164	0
0.000980	9.995	0.084	0.084	1.383	98.617	9.748	0.00116	9.712	0.00119	0
0.000061	14.000	0.084	0.084	1.383	100.000	11.997	0.00024	10.674	0.00061	0
TOTALS			6.110	6.110	100.0					
0.250000	0.050000									
0.177000	0.040000									

3888

PITT168

SIEVE, SH. PIP., SEDIGRAPH SAMPLE WT.= 5.3700

PHI PCT. CUMPT.

3.50	2.61	2.61	***
4.00	3.98	6.58	****
4.50	16.88	25.47	*****
5.00	24.84	50.31	*****
5.50	16.89	67.21	*****
6.00	9.94	77.14	*****
6.50	5.96	83.11	**
7.00	1.99	85.09	**
7.50	1.99	87.08	**
8.00	1.99	89.07	*
8.50	0.99	90.06	**
9.00	1.99	92.05	*
9.50	0.99	93.04	*
10.00	0.99	94.04	*
10.50	0.99	95.03	*****
11.00	4.97	100.00	
12.00			

MEAN ST.DEV. SKEWNESS KURTOSIS

5.79	1.34	0.81	2.83	KRUMBEIN+PETT IJOHN(1938) MOMENT MEASURES FOR SIZE RANGE 4.0 TO 11.0 PHI
5.82	1.63	0.52	1.74	FOLK GRAPHIC STATISTICAL PARAMETERS FOLK AND WARD,1957

PERCENTILES	MEDIAN	5.49	5TH	4.30	16TH	4.75	25TH	4.99
			75TH	6.39	84TH	7.22	95TH	10.98

PER CENT GRAVEL 0.0 SAND 2.61 SILT 84.34 ( 84.47) CLAY 13.05 ( 12.92)

GRAVEL + SAND 2.61 SILT/(SILT+CLAY) 86.73PCT GRAV+SAND/SILT+CLAY 0.03

LABELS SHEPAD -SILT FOLK(GMS)-MUD (SCS)-SILT

PITT169

SIEVE, SH. PIP., SEDIGRAPH SAMPLE WT.= 3.6900

PHI PCT. CUMPT.

2.50	0.81		*
3.00	1.35	0.81	*
3.50	2.44	2.17	**
4.00	1.91	4.60	**
4.50	6.51		*****
5.00	14.31	20.82	*****
5.50	19.08	39.90	*****
6.00	10.49	50.39	*****
6.50	9.54	59.93	*****
7.00	7.63	67.56	*****
7.50	5.72	73.29	*****
8.00	3.82	77.10	****
8.50	2.86	79.97	****
9.00	3.82	83.78	****
9.50	3.82	87.60	****
10.00	2.86	90.46	***
10.50	2.86	93.32	***
11.00	0.95	94.28	*
11.50	1.91	96.18	**
12.00	3.82	100.00	****

MEAN ST.DEV. SKEWNESS KURTOSIS

6.40	1.85	0.40	-0.02	KRUMBEIN+PETTICHOHN(1938) MOMENT MEASURES FOR SIZE RANGE 3.0 TO 11.5 PHI
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6.61	2.12	0.46	1.40	FOLK GRAPHIC STATISTICAL PARAMETERS FOLK AND WARD,1957
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PERCENTILES	MEDIAN	5.98	5TH	4.10	16TH	4.83	25TH	5.11
			75TH	7.72	84TH	9.03	95TH	11.19

PER CENT GRAVEL 0.0 SAND 4.60 SILT 72.40 ( 72.50) CLAY 23.00 ( 22.90)

PITT170

SIEVE, SH. PIP., SEDIGRAPH SAMPLE WT.= 3.3000

PHI PCT. CUMPCT.

2.50	3.03	***
3.00	6.06	3.03
3.50	9.09	*****
4.00	18.18	*****
4.50	27.46	*****
5.00	43.49	*****
5.50	61.20	*****
6.00	71.32	*****
6.50	82.29	****
7.00	86.50	****
7.50	91.57	***
8.00	94.10	**
8.50	95.78	**
9.00	97.47	***
12.00	100.00	

MEAN ST.DEV. SKEWNESS KURTOSIS

5.24 1.33 0.20 -0.10 KRUMBEIN+PETTICHOHN(1938) MOMENT MEASURES  
FOR SIZE RANGE 3.0 TO 9.0 PHI

5.26 1.48 0.14 1.20 FOLK GRAPHIC STATISTICAL PARAMETERS  
FOLK AND WARD,1957

PERCENTILES MEDIAN 5.18 5TH 3.16 16TH 3.88 25TH 4.37  
75TH 6.17 84TH 6.70 95TH 8.27

PER CENT GRAVEL 0.0 SAND 18.18 SILT 76.52 ( 75.91) CLAY 5.30 ( 5.90)

GRAVEL + SAND 18.18 SILT/(SILT+CLAY) 92.78PCT GRAV+SAND/SILT+CLAY 0.22

LABELS SHEPARD -SILT FOLK(GMS)-SANDY MUD (SCS)-SANDY SILT



PIT1171

SIEVE, SH. PIP., SEDIGRAPH SAMPLE WT.= 5.1600

PHI PCT. CUMPCT.

3.50	2.13	**
4.00	1.98	**
4.50	4.11	*****
5.00	19.93	*****
5.50	47.61	*****
6.00	65.40	*****
6.50	76.27	*****
7.00	81.22	****
7.50	85.17	****
8.00	89.13	*****
8.50	94.07	****
9.00	98.02	**
12.00	100.00	

MEAN ST.DEV. SKEWNESS KURTOSIS

5.87 1.17 0.47 0.23 KRUMBEIN+PETTIJOHN(1938) MOMENT MEASURES FOR SIZE RANGE 4.0 TO 9.0 PHI

5.93 1.24 0.47 1.08 FOLK GRAPHIC STATISTICAL PARAMETERS FOLK AND WARD, 1957

PERCENTILES MEDIAN 5.57 5TH 4.53 10TH 4.88 25TH 5.09  
75TH 6.44 84TH 7.35 95TH 8.62

PER CENT GRAVEL 0.0 SAND 2.13 SILT 87.21 ( 86.99) CLAY 10.66 ( 10.87)

GRAVEL + SAND 2.13 SILT/(SILT+CLAY) 88.89PCT GRAV+SAND/SILT+CLAY 0.02

LABELS SHEPARD -SILT FOLK(GMS)-MUD (SCS)-SILT

PI++ 172 0 0.0 0 0.0 0

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 \*\*\*\* MULTIMODAL SAMPLE \*\*\*\*  
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WET WT 1000.0000 DRY WT 6.2000 SALT 0.0 ORGANIC 0.0 MOISTURE 0.0 (GRAMS)  
 100.0000 100.0000 0.0 0.0 0.0 (PCT WET WT)  
 WEIGHT LOSS DUE TO HANDLING 0.0  
 GRAVEL CORRECTION FACTOR 1.000  
 SIZES ELIMINATED (<0.01%) NONE  
 TRASK SORTING COEFFICIENT 1.769  
 USING PROBABILITY EXTRAP. 1.742  
 MEAN CUBED DEVIATION 10.025  
 USING PROBABILITY EXTRAP. 6.001

PERCENTAGE COMPOSITION	TABLE OF STATISTICAL DATA IN PHI UNITS				PERCENTILES		LINEAR EXTRAP.		PROBABILITY EXTRAP.	
	MEAN-MOMENT	STD DEV	SKWNESS	KURTOSIS	MM.	PHI UNITS	MM.	PHI UNITS		
GRAVEL 0.0	4.24545	1.67467	2.13458	8.68077	5.0	0.15915	2.65150	0.14634	2.75503	
SAND 61.45	4.23052	1.51648	1.72089	5.99570	10.0	0.13702	2.86755	0.13166	2.92597	
SILT 34.93	4.07644	1.33846	0.51821	1.19969	10.0	0.12076	3.04980	0.11915	3.06908	
CLAY 3.62	4.08157	1.31259	0.54101	1.20514	25.0	0.10863	3.23253	0.10580	3.24062	
MUD 38.55	4.26705	1.21725	0.46978	0.97858	50.0	0.07720	3.69521	0.07726	3.69419	
S/M 1.59	4.27525	1.20617	0.48174	0.95210	75.0	0.03472	4.84806	0.03486	4.84206	
		1.21892	0.33008	0.23808	84.0	0.02234	5.48431	0.02238	5.48142	
		1.18625	0.34714	0.23656	90.0	0.01249	6.32338	0.01260	6.30995	
				0.54939	95.0	0.00565	7.46837	0.00567	7.46215	
				0.54651						

DATA FOR CONSTN OF BARGRAPHS AND CUM. CURVES

SIZE FRACTION	MM	PHI	WT.(GMS)		WT.PCT. COR	WT.PCT. CUMUL.	MID PHI(LINEAR)		MID PHI(PROB.)		MODE
			UNCOR	COR			PHI	MM	PHI	MM	
0.250000	2.000	2.000	0.050	0.050	0.806	0.806	1.751	0.29707	1.909	0.26622	1
0.177000	2.498	2.498	0.040	0.040	0.645	1.452	2.249	0.21036	2.280	0.20583	0
0.125000	3.000	3.000	0.720	0.720	11.613	13.065	2.749	0.14875	2.842	0.13946	0
0.088000	3.506	3.506	1.850	1.850	29.839	42.903	3.253	0.10488	3.289	0.10227	1
0.062500	4.000	4.000	1.150	1.150	18.548	61.452	3.753	0.07416	3.752	0.07225	0
0.044000	4.506	4.506	0.618	0.618	9.973	71.425	4.253	0.05244	4.246	0.05271	0
0.031000	5.012	5.012	0.328	0.328	5.285	76.710	4.759	0.03693	4.752	0.03710	0
0.022000	5.506	5.506	0.473	0.473	7.629	84.340	5.259	0.02612	5.244	0.02539	1
0.015600	6.002	6.002	0.224	0.224	3.614	87.953	5.754	0.01853	5.743	0.01867	0
0.011000	6.506	6.506	0.199	0.199	3.213	91.166	6.254	0.01310	6.240	0.01323	0
0.007800	7.002	7.002	0.100	0.100	1.606	92.772	6.754	0.00926	6.745	0.00932	0
0.005500	7.500	7.500	0.149	0.149	2.410	95.181	7.254	0.00655	7.234	0.00664	1
0.003400	8.002	8.002	0.075	0.075	1.205	96.386	7.754	0.00463	7.740	0.00468	0
0.002700	8.533	8.533	0.050	0.050	0.803	97.189	8.268	0.00325	8.254	0.00328	0
0.001900	9.040	9.040	0.050	0.050	0.802	97.992	8.786	0.00227	8.768	0.00229	0
0.00061	14.000	14.000	0.124	0.124	2.008	100.000	11.520	0.00034	9.646	0.00109	0
TOTALS			6.200	6.200	100.0						
0.250000	0.040000										
0.177000	0.040000										
0.125000	0.530000										
0.088000	1.080000										

P1++ 173 0 0.0 0 0.0 0

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 \*\*\* MULTIMODAL SAMPLE \*\*\*  
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WET WT	DRY WT	SALT	ORGANIC	MOISTURE	WEIGHT LOSS DUE TO HANDLING	0.0
1000.0000	6.6100	0.0	0.0	0.0 (GRAMS)	GRAVEL CORRECTION FACTOR	1.000
100.0000	100.0000	0.0	0.0	0.0 (PCT WET WT)	SIZES ELIMINATED (0.01%)	NONE
					TRASK SORTING COEFFICIENT	1.946
					USING PROBABILITY EXTRAP.	1.936
					MEAN CUBED DEVIATION	13.436
					USING PROBABILITY EXTRAP.	8.226

PERCENTAGE COMPOSITION	TABLE OF STATISTICAL DATA IN PHI UNITS				PERCENTILES		LINEAR EXTRAP.		PROBABILITY EXTRAP.	
	MEAN	STD DEV	SKEWNESS	KURTOSIS	MM.	PHI UNITS	MM.	PHI UNITS		
GRAVEL 0.0	4.80247	1.92296	1.88955	7.41921	5.0	0.15017	2.73535	0.14084	2.82763	
SAND 39.64	4.77049	1.74700	1.54282	5.64280	10.0	0.12295	3.02390	0.12207	3.03419	
SILT 53.94	4.55618	1.59466	0.26698	1.26038	16.0	0.10808	3.20984	0.10503	3.25114	
CLAY 6.43	4.56994	1.56951	0.28601	1.24847	25.0	0.08908	3.48676	0.08882	3.49293	
MUD 60.36	4.60957	1.39973	0.11444	1.10956	50.0	0.04577	4.44539	0.04575	4.44996	
S/M 0.66	4.62993	1.37879	0.13083	1.10647	75.0	0.02353	5.40508	0.02369	5.39977	
KRUMBEIN	1.42247	-0.00047		0.25119	84.0	0.01552	6.00931	0.01553	6.00872	
P-KRUM.	1.41248	-0.00301		0.25091	90.0	0.00869	6.84631	0.00876	6.85409	
FOLK (TRANSFORMED)				0.55760	95.0	0.00250	8.64101	0.00251	8.63659	
P-FOLK (TRANSFORMED)				0.55525						

DATA FOR CONSTN OF BARGRAPHS AND CUM. CURVES

SIZE FRACTION	MM	PHI	WT.(GMS)		WT.PCT.		MID PHILINEAR)		MID PHI(PROB.)		MODE
			UNCOR	COR	COR	CUMUL.	PHI	MM	PHI	MM	
0.250000	2.000	2.000	0.340	0.040	0.605	0.605	1.751	0.29707	1.905	0.26698	0
0.177000	2.498	0.040	0.040	0.040	0.605	1.210	2.249	0.21036	2.286	0.20901	0
0.125000	3.000	0.530	0.530	8.618	9.228	2.745	0.14875	2.839	0.13974	0	
0.087000	3.506	1.080	1.080	16.339	25.567	3.253	0.10488	3.293	0.10200	1	
0.062500	4.000	0.930	0.930	14.070	39.637	3.753	0.07416	3.764	0.07360	0	
0.044000	4.506	0.772	0.772	11.676	51.313	4.253	0.05244	4.255	0.05236	0	
0.031000	5.012	0.884	0.884	13.368	64.682	4.759	0.03693	4.755	0.03705	1	
0.022000	5.506	0.849	0.849	12.843	77.524	5.259	0.02612	5.246	0.02535	0	
0.015600	6.002	0.424	0.424	6.422	83.946	5.754	0.01853	5.742	0.01869	0	
0.011000	6.506	0.255	0.255	3.852	87.799	6.254	0.01310	6.243	0.01521	0	
0.007800	7.002	0.212	0.212	3.211	91.010	6.754	0.00926	6.741	0.00935	0	
0.005500	7.506	0.085	0.085	1.284	92.294	7.254	0.00655	7.247	0.00558	0	
0.003900	8.002	0.085	0.085	1.284	93.579	7.754	0.00463	7.746	0.00466	0	
0.002700	8.503	0.085	0.085	1.284	94.863	8.268	0.00325	8.256	0.00327	1	
0.001900	9.040	0.042	0.042	0.641	95.505	8.786	0.00227	8.780	0.00228	0	
0.001300	9.501	0.042	0.042	0.642	96.147	9.270	0.00162	9.263	0.00163	1	
0.000980	9.995	0.042	0.042	0.642	96.789	9.748	0.00116	9.739	0.00117	0	
0.000661	14.000	0.212	0.212	3.211	100.000	11.997	0.00024	10.619	0.00064	0	
TOTALS			6.610	6.610	100.0						
0.250000	0.030000										
0.177000	0.040000										

PITT174

SIEVE, SH. PIP., SEDIGRAPH SAMPLE WT.= 4.6800

PHI PCT. CUMPCT.

3.00	1.92		**
3.50	1.92	1.92	****
4.00	4.06	5.98	*****
4.50	4.75		*****
5.00	5.70	10.73	*****
5.50	14.25	16.43	*****
6.00	4.75	30.67	*****
6.50	21.84	35.42	*****
7.00	8.55	57.26	*****
7.50	6.65	65.61	*****
8.00	3.80	72.46	****
8.50	3.80	76.26	****
9.00	2.85	80.06	***
9.50	2.85	82.91	***
10.00	2.85	85.76	***
10.50	2.35	88.60	**
11.00	1.90	91.45	**
11.50	1.90	93.35	**
12.00	4.75	95.25	*****
12.00		100.00	

MEAN ST.DEV. SKEWNESS KURTOSIS

6.55 1.84 0.34 0.02 KRUMBEIN+PETTIJOHN(1938) MOMENT MEASURES FOR SIZE RANGE 3.5 TO 11.5 PHI

6.83 2.20 0.35 1.52 FOLK GRAPHIC STATISTICAL PARAMETERS FOLK AND WARD,1957

PERCENTILES MEDIAN 6.33 5TH 3.88 16TH 4.96 25TH 5.30  
75TH 7.83 84TH 9.19 95TH 11.43

PER CENT GRAVEL 0.0 SAND 5.98 SILT 70.51 ( 70.28) CLAY 23.50 ( 23.74)

GRAVEL + SAND 5.98 SILT/(SILT+CLAY) 74.75PCT GRAV+SAND/SILT+CLAY 0.06



P1++ 176 0 0.0 0 0.0 0

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 \*\*\* MULTIMODAL SAMPLE \*\*\*  
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WET WT DRY WT SALT ORGANIC MOISTURE  
 1000.0000 7.3200 0.0 0.0 0.0 (GRAMS)  
 99.9999 100.0000 0.0 0.0 0.0 (PCT WET WT)

WEIGHT LOSS DUE TO HANDLING 0.0  
 GRAVEL CORRECTION FACTOR 1.000  
 SIZES ELIMINATED (<0.075) NONE  
 TRASK SORTING COEFFICIENT 1.866  
 USING PROBABILITY EXTRAP. 1.846  
 MEAN CUBED DEVIATION 10.177  
 USING PROBABILITY EXTRAP. 5.902

PERCENTAGE COMPOSITION	TABLE OF STATISTICAL DATA IN PHI UNITS					PERCENTILES		LINEAR EXTRAP.		PROBABILITY EXTRAP.	
	MEAN	STD DEV	SKEWNESS	KURTOSIS		MM.	PHI UNITS	MM.	PHI UNITS		
GRAVEL 0.0	MOMENT 4.99725	1.78832	1.77948	6.98255	5.0	0.11697	3.09581	0.11153	3.16451		
SAND 32.65	P-MOMENT 4.96645	1.61852	1.39202	5.30257	10.0	0.10188	3.29508	0.09710	3.38442		
SILT 60.40	FOLK 4.77966	1.51455	0.30092	1.28297	15.0	0.08679	3.52624	0.08648	3.53142		
CLAY 6.95	P-FOLK 4.77785	1.49833	0.30926	1.28760	25.0	0.07268	3.73231	0.07147	3.80658		
MUD 67.35	INMAN 4.84641	1.32017	0.15167	1.13589	50.0	0.03994	4.64618	0.03946	4.64531		
S/M 0.48	P-INMAN 4.84412	1.31270	0.15145	1.11666	75.0	0.02087	5.58240	0.02097	5.57527		
	KRUMBEIN 1.33340	0.03618		0.23638	84.0	0.01392	6.16658	0.01402	6.15682		
	P-KRUM. 1.31021	0.04567		0.23698	90.0	0.00728	7.10263	0.00731	7.09628		
	FOLK (TRANSFORMED) 0.56217			0.56217	95.0	0.00235	8.73529	0.00237	8.72159		
	P-FOLK (TRANSFORMED) 0.56286			0.56286							

DATA FOR CONSTN OF BARGRAPHS AND CUM. CURVES

SIZE FRACTION MM	PHI	WT.(GMS) UNCOR	WT.(GMS) COR	WT.PCT. COR	WT.PCT. CUMUL.	MID PHI(LINEAR) PHI	MID PHI(LINEAR) MM	MID PHI(PROB.) PHI	MID PHI(PROB.) MM	MODE	
0.250000	2.000	0.030	0.030	0.410	0.410	1.751	0.29707	1.899	0.26320	0	
0.177000	2.498	0.040	0.040	0.546	0.546	0.956	2.249	0.21036	2.294	0.20384	0
0.125000	3.000	0.120	0.120	1.639	2.596	2.749	0.14875	2.801	0.14352	0	
0.082000	3.506	0.920	0.930	12.705	15.301	3.253	0.10488	3.330	0.09944	0	
0.062500	4.000	1.270	1.270	17.350	32.650	3.753	0.07416	3.779	0.07287	1*	
0.044000	4.506	0.997	0.997	13.626	46.277	4.253	0.05244	4.259	0.05222	0	
0.031000	5.012	0.985	0.985	13.452	59.729	4.759	0.03693	4.757	0.03697	0	
0.022000	5.506	1.016	1.016	13.887	73.615	5.259	0.02612	5.249	0.02630	1	
0.015600	6.002	0.661	0.661	9.927	82.642	5.754	0.01853	5.739	0.01872	0	
0.011000	6.506	0.305	0.305	4.166	86.808	6.254	0.01310	6.243	0.01320	0	
0.007800	7.002	0.203	0.203	2.777	89.585	6.754	0.00926	6.744	0.00933	0	
0.005500	7.506	0.152	0.152	2.083	91.668	7.254	0.00655	7.244	0.00660	0	
0.003900	8.002	0.102	0.102	1.389	93.057	7.754	0.00463	7.746	0.00466	0	
0.002700	8.503	0.102	0.102	1.389	94.445	8.254	0.00325	8.256	0.00327	0	
0.001900	9.000	0.102	0.102	1.389	95.834	8.754	0.00227	8.772	0.00229	1	
0.001300	9.501	0.102	0.102	1.389	97.223	9.270	0.00162	9.251	0.00164	1	
0.000661	14.000	0.203	0.203	2.777	100.000	11.751	0.00029	10.210	0.00084	0	
TOTALS		7.320	7.320	100.0							
0.250000	0.020000										
0.177000	0.010000										
0.125000	0.060000										

PI\*\* 177 0 0.0 0 0.0 0

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 \*\*\* MULTIMODAL SAMPLE \*\*\*  
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WET WT	DRY WT	SALT	ORGANIC	MOISTURE	WEIGHT LOSS DUE TO HANDLING	0.0
1000.0000	7.4100	0.0	0.0	0.0 (GRAMS)	GRAVEL CORRECTION FACTOR	1.000
100.0000	100.0000	0.0	0.0	0.0 (PCT WET WT)	SIZES ELIMINATED (<0.012)	NONE
					TRASK SORTING COEFFICIENT	1.728
					USING PROBABILITY EXTRAP.	1.719
					MEAN CUBED DEVIATION	8.771
					USING PROBABILITY EXTRAP.	4.094

PERCENTAGE COMPOSITION		TABLE OF STATISTICAL DATA IN PHI UNITS				PERCENTILES		LINEAR EXTRAP.		PROBABILITY EXTRAP.	
		MEAN	STD DEV	SKEWNESS	KURTOSIS	MM.	PHI UNITS	MM.	PHI UNITS	MM.	PHI UNITS
GRAVEL	0.0	5.12973	1.65875	1.92175	7.92382	5.0	0.10417	3.26301	0.05811	3.34945	
SAND	23.48	5.08011	1.44530	1.55623	5.14613	10.0	0.08504	3.55570	0.08390	3.57519	
SILT	70.93	4.95122	1.38019	0.26585	1.28004	10.0	0.07415	3.75343	0.07211	3.74356	
CLAY	5.59	4.96038	1.35111	0.26323	1.26615	25.0	0.05000	4.05884	0.05975	4.00488	
MUD	76.52	5.01921	1.26579	0.16114	0.94825	50.0	0.03552	4.81524	0.03548	4.81666	
S/M	0.31	5.03225	1.23869	0.17404	0.94951	75.0	0.02010	5.63659	0.02022	5.62817	
			1.16900	0.03267	0.23260	84.0	0.01282	6.28500	0.01295	6.27093	
			1.15800	0.02986	0.23219	90.0	0.00810	6.94812	0.00814	6.94160	
					0.56157	95.0	0.00341	8.16514	0.00345	8.17912	
					0.55872						

DATA FOR CONSTN OF BARGRAPHS AND CUM. CURVES

SIZE FRACTION	WT.(GMS)	WT.PCT.	WT.PCT.	MID PHI(LINEAR)	MID PHI(PROB.)	MODE				
MM	PHI	UNCOR	COR	COR	CUMUL.	PHI	MM	PHI	MM	
0.250000	2.000	0.020	0.020	0.270	0.270	1.751	0.29707	1.890	0.26978	1
0.177000	2.498	0.010	0.010	0.135	0.405	2.249	0.21036	2.272	0.20710	0
0.125000	3.000	0.060	0.060	0.810	1.215	2.749	0.14875	2.807	0.14288	0
0.088000	3.506	0.540	0.540	7.287	8.502	3.253	0.10488	3.341	0.09806	0
0.762500	4.000	1.110	1.110	14.980	23.482	3.753	0.07416	3.793	0.07213	1
0.044000	4.506	0.968	0.968	13.061	36.542	4.253	0.05244	4.266	0.05198	0
0.031000	5.012	1.631	1.631	22.010	58.553	4.759	0.03693	4.761	0.03588	1*
0.027000	5.506	1.063	1.063	14.348	72.900	5.259	0.02612	5.249	0.02630	0
0.015600	6.002	0.591	0.591	7.970	80.870	5.754	0.01853	5.742	0.01868	0
0.011000	6.506	0.413	0.413	5.580	80.450	6.254	0.01310	6.240	0.01323	0
0.007800	7.002	0.295	0.295	3.985	90.435	6.754	0.00926	6.739	0.00936	0
0.005500	7.506	0.177	0.177	2.391	92.827	7.254	0.00655	7.241	0.00661	0
0.003900	8.002	0.118	0.118	1.594	94.420	7.754	0.00463	7.742	0.00467	0
0.002700	8.533	0.118	0.118	1.594	96.015	8.268	0.00325	8.250	0.00329	1
0.001900	9.040	0.059	0.059	0.797	90.812	8.786	0.00227	8.775	0.00228	0
0.003061	14.000	0.236	0.236	3.188	100.000	11.520	0.00034	9.813	0.00111	0
TOTALS		7.410	7.410	100.0						
0.250000	0.070000									
0.177000	0.030000									
0.125000	0.290000									
0.088000	0.810000									

PITT178

SIEVE, SH. PIP., SEDIGRAPH SAMPLE WT.= 4.6300

PHI PCT. CUMPT.

3.50	2.16	**
4.00	2.16	**
	1.96	**
4.50	4.12	*****
	8.21	*****
5.00	12.92	*****
	18.59	*****
5.50	31.51	*****
	17.61	*****
6.00	49.12	*****
	12.72	*****
6.50	61.84	*****
	7.83	*****
7.00	69.67	*****
	5.87	*****
7.50	75.54	****
	3.91	****
8.00	79.45	**
	1.96	**
8.50	81.41	**
	1.96	**
9.00	83.37	***
	2.94	***
9.50	86.30	***
	2.94	***
10.00	89.24	**
	1.96	**
10.50	91.19	**
	1.96	**
11.00	93.15	**
	1.96	**
11.50	95.11	****
	4.89	****
12.00	100.00	

MEAN ST.DEV. SKEWNESS KURTOSIS

6.46 1.71 0.57 0.65

KRUMREIN+PETTICORN(1938) MOMENT MEASURES  
FOR SIZE RANGE 4.0 TO 11.5 PHI

6.74 2.06 0.55 1.52

FOLK GRAPHIC STATISTICAL PARAMETERS  
FOLK AND WARD, 1957

PERCENTILES MEDIAN 6.03 5TH 4.55 16TH 5.08 25TH 5.32  
75TH 7.45 84TH 9.11 95TH 11.47

PER CENT GRAVEL 0.0 SAND 2.16 SILT 77.30 ( 77.29) CLAY 20.54 ( 20.55)

GRAVEL + SAND 2.16 SILT/(SILT+CLAY) 79.00PCT GRAV+SAND/SILT+CLAY 0.02



PITT179

SIEVE, SH. PIP., SEDIGRAPH SAMPLE WT.= 4.8930

PHI PCT. CUMPT.

2.00	1.02	*
2.50	1.64	**
3.00	2.66	***
3.50	5.52	*****
4.00	11.04	*****
4.50	17.27	*****
5.00	36.84	*****
5.50	54.63	*****
6.00	67.09	*****
6.50	75.09	*****
7.00	81.32	****
7.50	85.77	**
8.00	87.55	**
8.50	89.33	**
9.00	91.10	**
9.50	92.88	***
10.00	95.55	**
10.50	97.33	***
12.00	100.00	

MEAN ST.DEV. SKEWNESS KURTOSIS

5.65 1.63 0.45 0.85 KRUMBEIN+PETT(JOHN(1938) MOMENT MEASURES FOR SIZE RANGE 2.5 TO 10.5 PHI

5.69 1.71 0.36 1.53 FOLK GRAPHIC STATISTICAL PARAMETERS FOLK AND WARD,1957

PERCENTILES MEDIAN 5.37 5TH 3.41 16TH 4.40 25TH 4.70  
75TH 6.49 84TH 7.30 95TH 9.90

PER CENT GRAVEL 0.0 SAND 11.04 SILT 76.69 ( 76.50) CLAY 12.27 ( 12.45)

GRAVEL + SAND 11.04 SILT/(SILT+CLAY) 86.00PCT GRAV+SAND/SILT+CLAY 0.12

LABELS SHEPARD -SILT FOLK(GMS)-SANDY MUD (SCS)-SANDY SILT

400

\*\*\*\*\*  
 \*\*\*\* MULTIMODAL SAMPLE \*\*\*\*\*  
 \*\*\*\*\*

PI# 180 0 0.0 0 0.0 0

WEIGHT LOSS DUE TO HANDLING 0.0  
 GRAVEL CORRECTION FACTOR 1.000  
 SIZES ELIMINATED (KO-01%) NONE  
 TRASK SORTING COEFFICIENT 2.434  
 USING PROBABILITY EXTRAP. 2.417  
 MEAN CUBED DEVIATION 11.139  
 USING PROBABILITY EXTRAP. 7.508

WET WT 1000.0000 0.0 0.0 0.0 0.0 (GRAMS)  
 99.9999 100.0000 0.0 0.0 (PCT WET WT)

ORGANIC MOISTURE  
 0.0 0.0 0.0 0.0

SALT  
 0.0 0.0 0.0 0.0

DPY WT 5.4700  
 100.0000

TABLE OF STATISTICAL DATA IN PHI UNITS

PERCENTAGE COMPOSITION	MEAN	STD DEV	SKWENESS	KURTOSIS	MM.	PHI UNITS	MM.	PHI UNITS
GRAVEL 0.0	5.21162	2.07127	1.25358	4.91588	0.14375	2.79839	0.13808	2.85640
SAND 34.00	5.18768	1.94761	1.01628	3.83622	0.11678	3.09813	0.11382	3.15511
SILT 57.22	5.07272	1.89660	0.24446	1.01803	0.10130	3.20330	0.09840	3.34521
CLAY 8.77	5.08026	1.87532	0.25827	1.01488	0.08088	3.63182	0.08008	3.68246
MUD 66.00	5.16457	1.86167	0.14865	0.71152	0.03377	4.88222	0.03376	4.88863
S/M 0.52	5.18507	1.83986	0.16112	0.71361	0.01362	6.15769	0.01371	6.18884
P-KPUM.	1.90079	0.02663	0.27304		0.00767	7.02064	0.00763	7.02493
P-FOLK (TRANSFORMED)	1.88621	0.02702	0.27093		0.00434	7.84945	0.00438	7.83436
P-FOLK (TRANSFORMED)	0.50447				0.00173	9.17247	0.00175	9.16200
	0.50369							

PERCENTILES LINEAR EXTRAP.

PROBABILITY EXTRAP.

DATA FOR CONSTN OF BARGRAPHS AND CUM. CURVES

SIZE FRACTION MM	PHI	UNCOR	WT.(GMS)	COR	WT.PCT.	COR	WT.PCT.	MID PHI (LINEAR)	PHI	MID PHI (PROB.)	MODE
0.250000	2.000	0.070	0.070	1.280	1.751	0.29707	1.915	0.26520	1		
0.175000	2.498	0.030	0.030	0.548	1.828	2.249	2.268	0.20761	0		
0.125000	3.000	0.290	0.290	9.302	2.749	0.14875	2.814	0.14220	0		
0.087500	3.500	0.810	0.810	14.308	3.253	0.10488	3.300	0.13155	1		
0.062500	4.000	0.660	0.660	12.066	3.753	0.07416	3.766	0.07349	0		
0.044000	4.500	0.505	0.505	9.227	4.253	0.05244	4.258	0.05228	0		
0.021000	5.012	0.480	0.480	8.956	4.759	0.03693	4.760	0.03661	0		
0.022500	5.506	0.626	0.626	11.448	5.259	0.02612	5.255	0.02618	0		
0.015000	6.002	0.479	0.479	72.589	5.754	0.01833	5.747	0.01862	0		
0.011000	6.506	0.268	0.268	6.734	6.254	0.01310	6.245	0.01319	0		
0.007600	7.002	0.258	0.258	4.714	6.754	0.00926	6.744	0.00933	0		
0.005500	7.506	0.184	0.184	3.367	7.254	0.00655	7.244	0.00660	0		
0.003900	8.002	0.221	0.221	4.060	7.754	0.00463	7.737	0.00469	1		
0.002700	8.533	0.111	0.111	2.021	8.266	0.00325	8.254	0.00327	0		
0.001500	9.074	0.074	0.074	1.346	8.786	0.00227	8.775	0.00228	0		
0.001300	9.501	0.074	0.074	1.347	9.250	0.00162	9.257	0.00163	1		
0.000690	10.501	0.074	0.074	1.346	97.306	10.001	0.00098	9.960	0.00100	0	
0.000061	14.000	0.147	0.147	2.694	100.000	12.251	0.00021	11.054	0.00047	0	
TOTALS	5.470	5.470	100.0								

EXECUTION TERMINATED

APPENDIX 4

BEDLOAD CALCULATIONS

A simplified form of Einsteins (1950) equation was used (Graf, 1971).

Method

$$\Phi = f(\Psi)$$

use  $d = d_{35}$

$$\Psi = \frac{\rho_s - \rho}{\rho} \frac{d}{s R_h}, \quad R_h \approx R_h'$$

Knowing  $\Psi$ , go to Figure and determine  $\Phi$

$$\Phi = \frac{g_s}{\gamma_s} \sqrt{\frac{\rho}{\rho_s - \rho} \frac{1}{g d^3}}$$

$$\therefore g_s = \frac{\Phi \gamma_s}{\sqrt{\frac{\rho}{\rho_s - \rho} \frac{1}{g d^3}}}$$

$$G_s = B g_s \quad (\text{in kilograms per hour})$$

$\Psi$  intensity of shear of particles

$\Phi$  intensity of bedload transport

$\rho_s$  density of grain

$\rho$  density of water

$d$  grain diameter

$s$  slope

$R_h$  hydraulic radius

$g_s$  bedload rate (unit time and width)

$G_s$  bedload rate per unit time

$B$  width

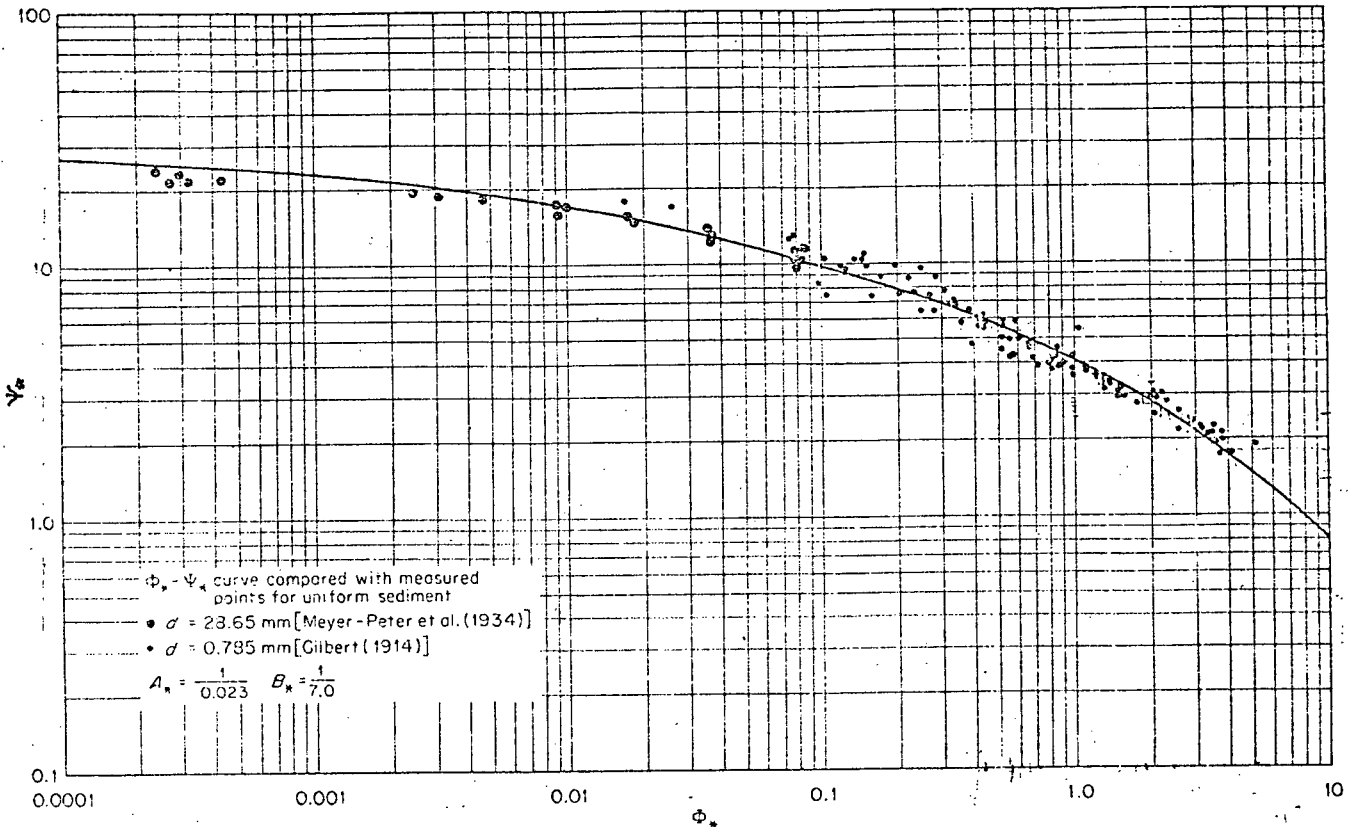


Fig. 7.13 Plot of Einstein's functions;  $\Phi_*$  vs.  $\Psi_*$ . [After EINSTEIN (1950).]

Graf, W. H., 1971, Hydraulics of sediment transport: McGraw Hill, Inc., New York.

An example: Pitt-Fraser confluence; Freshet flood.

$$\begin{aligned} B &= 601 \text{ m} \\ s &= .000018 \\ \rho_s &= 2.65 \\ \rho &= 1.00 \\ R_h &= 5.06 \text{ m} \\ d_{35} &= .0003 \text{ m} \end{aligned}$$

$$\begin{aligned} \psi &= \frac{2.65 - 1}{1} \times \frac{.0003}{.000018 \times 5.06} \\ &= \frac{.0003}{.0000919} = 3.3 \quad (\text{from fig. } \phi = 1.6) \end{aligned}$$

$$\begin{aligned} g_s &= \frac{1.6 (2650)}{2.65-1} \times \frac{1}{9.8(.0003)^3} \\ &= \frac{4240}{4785.91} \\ &= .088593 \end{aligned}$$

$$\begin{aligned} G_s &= .088593 (601) \\ &= 53.24 \text{ kg/sec} \\ &= 191,664 \text{ kg/hr} \end{aligned}$$

Summary of calculations of three cross sections of the river. (1) near Fraser-Pitt confluence (2) mid-river (3) near lake entrance. Values are in kg/hr.

+ movement in flood direction

- movement in ebb direction

	(1) Near Pitt- Fraser con- fluence	(2) Mid-river	(3) Near Lake entrance	
Winter Flood	+407,320	+239,680	+320,250	
Winter Ebb	-251,156	-164,352	-202,825	Average
	+156,164	+75,328	+117,425	+116,305
Freshet Flood	+191,664	+68,480	+117,425	
Freshet Ebb	-149,750	-49,990	-90,737	Average
	+41,914	+18,490	+26,688	+26,688

Calculations for net sediment movement were based on values determined at (1) near Fraser Pitt confluence.

WINTER TRANSPORT(8 months)

Flood = 44% of total time, 5856 hours  
Ebb = 56% of total time, 5856 hours

For time under flood, 55% is above critical velocity  
For time under ebb, 60% is above critical velocity

Thus, FLOOD = (44%)(55%)(5856)=1417 hours/year  
EBB = (56%)(60%)(5856)=1968 hours/year

FLOOD  
 $G_s = 407,319 \text{ kg/hr}$

total flood transport = 407,319kg/hr X 1417 hours  
total flood=+577,717,023 kg.

EBB

$G_s = 251,156 \text{ kg/hr}$

total ebb transport = 251,156 kg/hr X 1968 hours  
total ebb=-494,275,008 kg.

FRESHET TRANSPORT (4 months)

Flood =44% of total time, 2904 hours  
Ebb =56% of total time, 2904 hours

For time under flood, 55% is above critical velocity  
For time under ebb, 60% is above critical velocity

Thus, FLOOD = (44%)(55%)(2904)=702 hours  
EBB = (56%)(60%)(2904)=976 hours

FLOOD

$G_s = 191,664 \text{ kg/hr}$

total flood transport = 191,664 kg/hr X 702 hours  
total flood =+134,548,699 kg.

EBB

$G_s = 149,751 \text{ kg/hr}$

total ebb transport = 149,751 kg/hr X 976 hours  
total ebb =-146,156,976 kg.

Winter flood - Winter Ebb = +82,896 tonnes  
Freshet flood-freshet Ebb = -11,608 tonnes  
71,288 tonnes

Net transport + 71, 288 tonnes

Publications:

- Ashley, G.M., 1971. Rhythmic sedimentation: glacial Lake Hitchcock, Massachusetts-Connecticut: Geol. Soc. Amer., Abst./Programs, v.3, no.1, p.2 and v.3, no.7, p.495.
- \_\_\_\_\_, 1972. Rhythmic sedimentation in glacial Lake Hitchcock, Massachusetts-Connecticut: Univ. of Mass. Publications Series, no.10, 148 p.
- \_\_\_\_\_, (with Boothroyd, J.C.), 1972. Bedforms and sedimentary structures of braided outwash streams, northeastern Gulf of Alaska: Geol. Soc. Amer., Abst/Programs, v.4, no.1, p.3.
- \_\_\_\_\_, (with Boothroyd, J.C.), 1972. Continental sedimentation in a tectonically active geosynclinal basin: the glacial outwash shoreline, northeastern Gulf of Alaska: Abst/Programs, A.A.P.G.-S.E.P.M. (National Meeting).
- \_\_\_\_\_, (with Gustavson, T.C. and Boothroyd, J.C.), 1972. Depositional sequences in glaciolacustrine deltas: Geol. Soc. Amer., Abst/Programs, v.4, no.1, p.18.
- \_\_\_\_\_, (with Hartshorn, J.H.), 1972. Glacial environment and processes, southeastern Alaska: Coastal Research Center Technical Report Series, no.4, Dept. of Geol., Univ. of Mass., Amherst, 69 p.
- \_\_\_\_\_, (with Southard, J.B. and Boothroyd, J.C.), 1972. Flume simulation of ripple-draft sequences: Geol. Soc. Amer., Abst/Programs, v.4, no.7, p. 672 (manuscript in preparation).
- \_\_\_\_\_, 1973. Impregnation of fine-grained sediments with a polyester resin: a modification of Altemuller's method: Jour. Sed. Petrology, v.43, p.298-301.
- \_\_\_\_\_, (with Boothroyd, J.C.). Flow processes, bar morphology, and sedimentary structures on braided outwash fans, northeastern Gulf of Alaska.
- \_\_\_\_\_, (with Gustavson, T.C. and Boothroyd, J.C.). Depositional sequences in glaciolacustrine deltas.
- \_\_\_\_\_, and Duncan, I.J., 1977, The Hawksbury Sandstone: a critical review of proposed environmental models: Jour. Geol. Soc. Australia(March issue).
- \_\_\_\_\_, 1977, Sedimentology of the Pitt system, British Columbia: Geol. Assoc. Canada Annual Meeting Abstr., v. 2.
- \_\_\_\_\_, 197?, Polymodal sediments and their interpretation: Journal of Geology, (accepted for publication with minor revisions)